

1.1 Electrochemical cell as a tool of chemical analysis

Electroanalytical Chemistry

A science on applications of physicochemical processes taking place in an electrochemical cell for chemical analysis of matter.

Electrochemical Cell

Two electronic conductors in contact with an electrolyte solution.

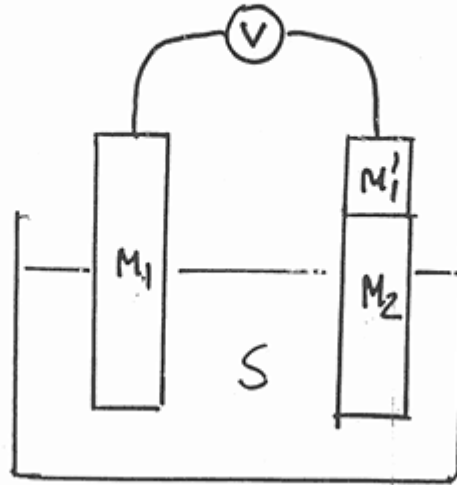
Electrode

The system electronic conductor in contact with ionic conductor.

Interface

The boundry between ionic and electronic conductor

Potential Difference between two metals in a cell without liquid junction



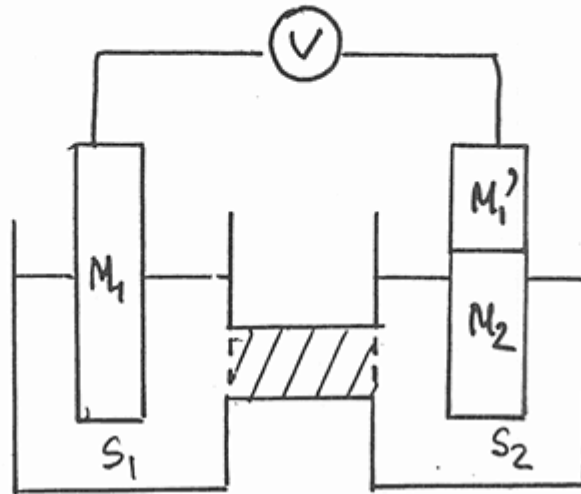
$$V = \text{potential } M'_1 - \text{potential } M_1$$

(right electrode) (left electrode)

$$V = PD_{M'_1/M_2} + PD_{M_2/S} + PD_{S/M_1}$$

In the most simple case the potential difference of the cell is equal to a sum of potential differences across three interfaces.

Potential difference between two metals in a cell with liquid junction



$$V = PD_{M'_1/M_2} + PD_{M_2/S_2} + PD_{S_2/S_1} + PD_{S_1/M_1}$$

The potential difference of the above cell is equal to the sum of potential differences of four phase boundaries.

In this bioelectroanalytical experiment the two electrodes are separated by large number of interfaces

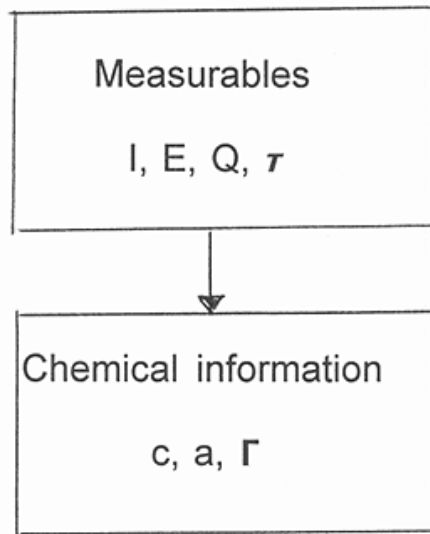


FIG. 5. The arrangement of electrodes for cyclic voltammetry in kidney cortex of a rat.

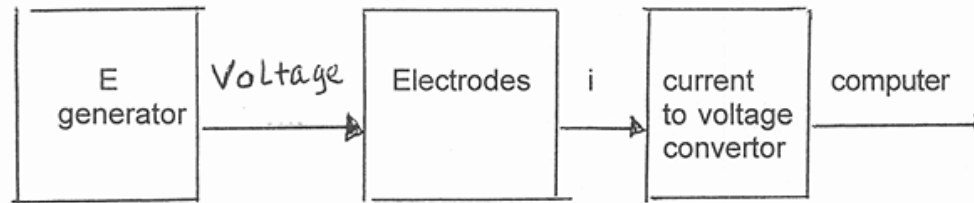
The principle of electroanalytical experiment consists of keeping the potential difference at all but one interface constant

Electrode with variable PD - indicator electrode

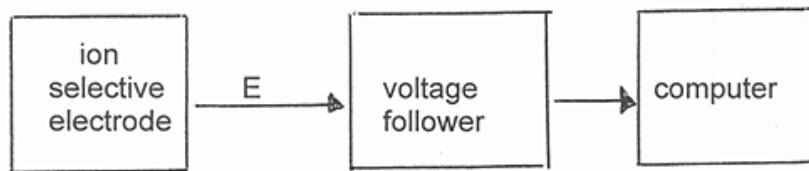
Electrode with constant PD - reference electrode



Polarography



Potentiometry

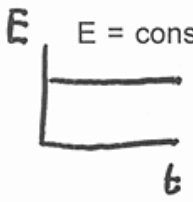
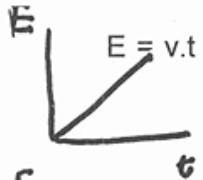

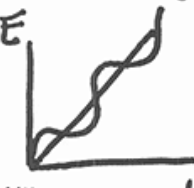
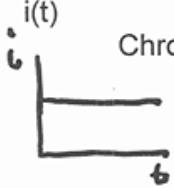
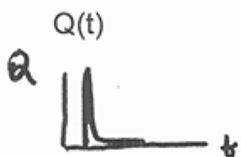


1.2 Classification of Electroanalytical techniques

1. Potentiometry - consists of measuring the potential difference of the electrochemical cell at zero current flow. Potentiometry includes analytical applications of the ion selective electrodes
2. Voltammetric techniques - consist of introducing a controlled perturbation and following the response of the cell to this perturbation

<u>Perturbation</u>	<u>Response</u>	<u>Technique</u>
$E(t)$	$i(t)$	voltammetry
$i = \text{const}$	$Q = i \cdot t$	coulometry

Voltammetric techniques

	perturbation	response	detection limit	
I)	$E(t)$	$I(t), Q(t)$	mole dm^{-3}	
	Amperometric			
1.	 <p>$E = \text{const}$</p>	polarography	$10^{-2}-10^{-5}$	
2.	 <p>$E = v \cdot t$</p>	cyclic voltummetry	$10^{-2}-10^{-5}$	
3.		pulse polarography	$10^{-2}-10^{-7}$	
4.		a.c. polarography	$10^{-2}-10^{-7}$	
II	5.	 <p style="text-align: center;">Chronopotentiometry</p>	$E(t)$ chronopotentiometry	$10^{-2}-10^{-5}$
III	6.		$E(t)$ coulostatic	$10^{-4}-10^{-7}$

I came to Karlsruhe in November 1908....I was then 22. Haber proposed to me to explore the glass electrode, the interest for this topic having been suggested to him by the earlier work of Cremer. They tried already in Karlsruhe some experiments before I came, but without success. I have been handed over the respective apparatus, consisting of a piece of broken glass -cylinder about 3 mm thick, with a tin-foil stucked around. I saw at once that such an element could never work, being short-circuited all over the moist glass surface. Although I didn't know at this stage that glass-balloons have been used by Cremer (and previously by Giese), I blew the thin bulb which remains until today the classical form of the glass electrode. I also installed a quadrant electrometer with the use of which I was well acquainted. With this arrangement I got at once positive results especially as I discovered at the very beginning the aid of steaming and soaking the glass, quite independently, of course. I applied steaming at first as a method of cleaning, being in this case reluctant to use either chromic acid or organic liquids. I also learned in the first days the need of avoiding drying out of the glass-bulb and the superiority of soft over hard glass. Finally, I chose the kind of diagram for plotting the bilogarithmic curve as the most adequate way of presentation. When Haber went to see me in the laboratory after two days, I was able to show him a very good curve in HCl-KOH, with an efficiency of about 0.5V. He would not believe first that it was possible to get these results in such a short time and I had to let him look at the reading telescope that he could plot the points by himself. The experiment proceeded smoothly, so he gave himself an outbreak of enthusiasm, leaped, embraced and praised me in his cheerful manner.

A letter from Klemensiewicz to
Malcolm Dole

Historical background of Electroanalytical Chemistry

Potentiometry

1910 - pH glass electrode

1920 - cation glass membrane electrode

1930 - pH meter marketed (Beckman)

1950 - blood gas analysers developed

1960 - Membrane Technology
Nonglass ISE
Gas sensors (GSE)
Enzyme electrodes

1970 - Bioelectrochemical sensors
Indirect ISE's
Enzyme; Tissue
Bacterial; Organelle

1980 - Bioselective sensors
Chem Fet
Bio Fet
Immunoasseys
Multiple enzymes

Voltammetric Technique

1905 - Kucera-mercury drop experiments

1920 - Heyrovsky - polarography

1930 - Ilkovic equation polarograph marketed

1950 - Polarography-major analytical technique (1955-Heyrovsky-Nobel Prize!)

1960 - Stripping voltammetry
AC polarography;
pulse polarography;
differential pulse polarography

1970 - Ultra microelectrodes in vivo voltammetry

1980 - Sensors for liquid chromatography; flow injection analysis; amperometric-sensors

Applications of electroanalytical techniques

1. environment control
2. industrial analysis
3. pharmacy and pharmacology
4. biology and clinical chemistry
5. surface analysis
6. energy conversion

2. Introduction to potentiometry

2.1. Galvani potential and electrochemical potential

Zero energy – charged particle in vacuum at infinite separation from a charged phase

Basic concepts

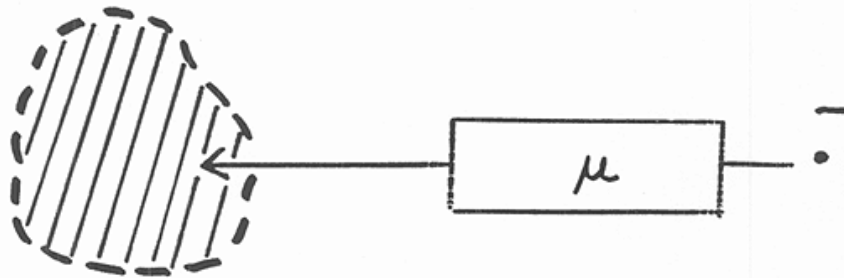
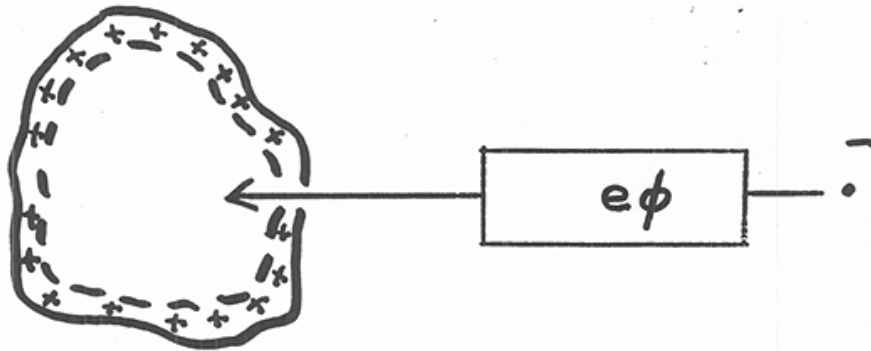
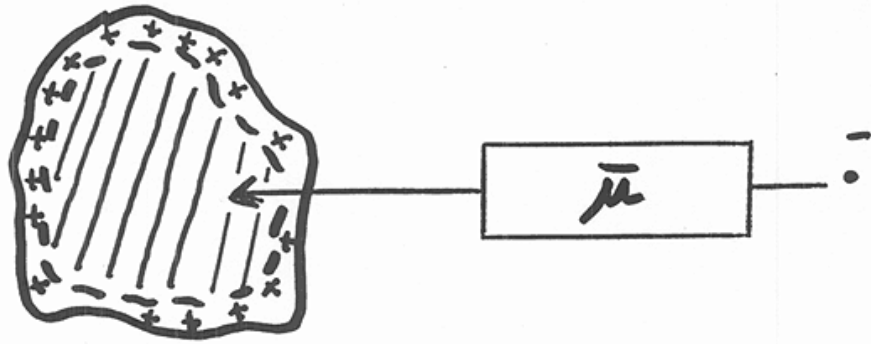
1. Electrochemical potential - $\bar{\mu}$

work done when a charged particle is transferred from infinite separation in vacuum to the interior of a charged phase

2. Chemical potential - μ

work done when a charged particle is transferred from infinite separation in vacuum to the interior of a phase stripped from the charged surface layer

3. Inner potential (Galvani potential) - ϕ work done when a charged particle is transferred from infinite separation in vacuum across a surface shell which contains an excess charge and oriented dipoles



$$\bar{\mu} = \mu + e\phi$$

The inner potential may be regarded as a sum of:

- 1) Potential created by the excess charge, the so called outer potential or Volta potential, denoted as ψ . For a charge q on a sphere of radius a :

$$\psi = \frac{q}{a}$$

2. Potential created by oriented dipoles with dipole moment p referred to as surface potential, denoted as χ and equal to :

$$\chi = 4\pi Np / \epsilon$$

Therefore the inner potential is equal to:

$$\phi = \psi + \chi$$

Thermodynamic relationships

In a charged system the inner potential ϕ is an additional independent variable of the total Gibbs free energy:

$$G = f(p, T, n_j, \phi)$$

Basic thermodynamic definitions:

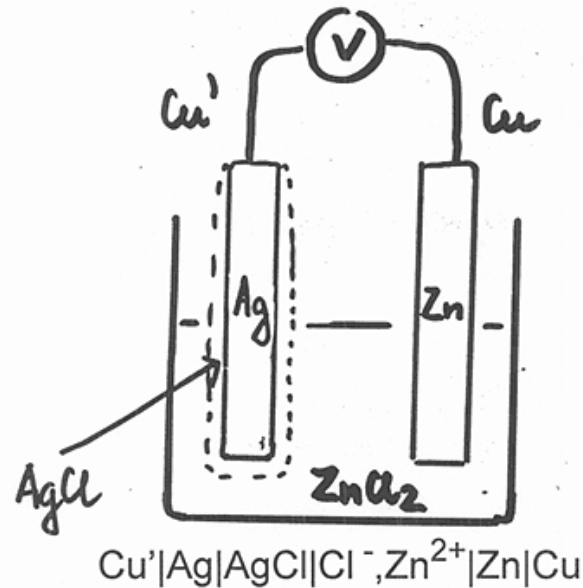
$$1. \bar{\mu}_i = (dG / dn_i)_{p, T, n_j \neq n_i, \phi}$$

$$2. \mu_i = (dG / dn_i)_{p, T, n_j \neq n_i, \phi=0}$$

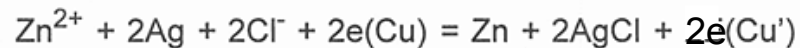
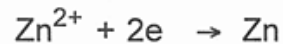
Equilibrium condition: two phases α and β are in thermodynamic equilibrium when:

$$\bar{\mu}_i^\alpha = \bar{\mu}_i^\beta$$

2.2 Electrochemical equilibria and electromotive force (emf) of a cell without liquid junction



Reactions



Note that vertical bars in the scheme of the cell denote a phase boundary

The cell at equilibrium

$$\bar{\mu}_{\text{Zn}^{2+}} + 2\bar{\mu}_e(\text{Cu}) + 2\bar{\mu}_{\text{Cl}^-} + 2\mu_{\text{Ag}} = \mu_{\text{Zn}} + 2\mu_{\text{AgCl}} + 2\bar{\mu}_e(\text{Cu}')$$

After rearrangement

$$\left(\mu_{\text{Zn}^{2+}} - \mu_{\text{Zn}}\right) - \left(2\mu_{\text{AgCl}} - 2\mu_{\text{Ag}} - 2\mu_{\text{Cl}^-}\right) = -2\left(\bar{\mu}_e(\text{Cu}) - \bar{\mu}_e(\text{Cu}')\right)$$

Electromotive force of the cell

recall $\bar{\mu}_e = \mu_e - F\phi$

$$-2\left(\bar{\mu}_e(\text{Cu}) - \bar{\mu}_e(\text{Cu}')\right) = 2F(\phi(\text{Cu}) - \phi(\text{Cu}')) = 2FE$$

Electromotive force of a cell

$$E = \phi(\text{Cu}) - \phi(\text{Cu}')$$

or

$$\frac{\left(\mu_{\text{Zn}^{2+}} - \mu_{\text{Zn}}\right)}{2F} - \frac{\left(2\mu_{\text{AgCl}} - 2\mu_{\text{Ag}} - 2\mu_{\text{Cl}^-}\right)}{2F} = E$$

$$E_1 = \frac{\left(\mu_{\text{Zn}^{2+}} - \mu_{\text{Zn}}\right)}{2F} \quad E_2 = \frac{\left(2\mu_{\text{AgCl}} - 2\mu_{\text{Ag}} - 2\mu_{\text{Cl}^-}\right)}{2F}$$

However this separation is formal or conventional in reality:

$$\mu_{\text{ZnCl}_2} - \mu_{\text{Zn}} + 2\mu_{\text{Ag}} - 2\mu_{\text{AgCl}} = -\Delta G = 2FE$$

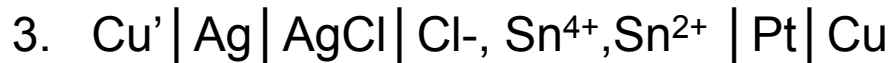
Examples of electrochemical cells and their emf



$$E = \frac{(\mu_{\text{Zn}^{2+}} - \mu_{\text{Zn}})}{2F} - \frac{(2\mu_{\text{AgCl}} - 2\mu_{\text{Ag}} - 2\mu_{\text{Cl}^-})}{2F}$$



$$E = \frac{(\mu_{\text{Mn}^{2+}} - \mu_{\text{Mn}})}{2F} - \frac{(2\mu_{\text{AgCl}} - 2\mu_{\text{Ag}} - 2\mu_{\text{Cl}^-})}{2F}$$



$$E = \frac{(\mu_{\text{Sn}^{4+}} - \mu_{\text{Sn}^{2+}})}{2F} - \frac{(2\mu_{\text{AgCl}} - 2\mu_{\text{Ag}} - 2\mu_{\text{Cl}^-})}{2F}$$

The second term in all three equations is the same hence we can write

$$E = E_{test} - \text{const}$$

Reference electrode convention

$$\frac{(2\mu_{\text{AgCl}} - 2\mu_{\text{Ag}} - 2\mu_{\text{Cl}^-})}{2F} = 0$$



$$E = \frac{(\mu_{\text{Zn}^{2+}} - \mu_{\text{Zn}})}{2F}$$



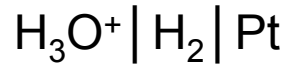
$$E = \frac{(\mu_{\text{Mn}^{2+}} - \mu_{\text{Mn}})}{2F}$$



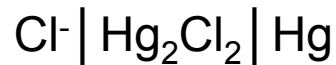
$$E = \frac{(\mu_{\text{Sn}^{4+}} - \mu_{\text{Sn}^{2+}})}{2F}$$

Electrode potential – emf of a cell built up from a given test electrode and a reference electrode

Reference electrodes



Hydrogen electrode



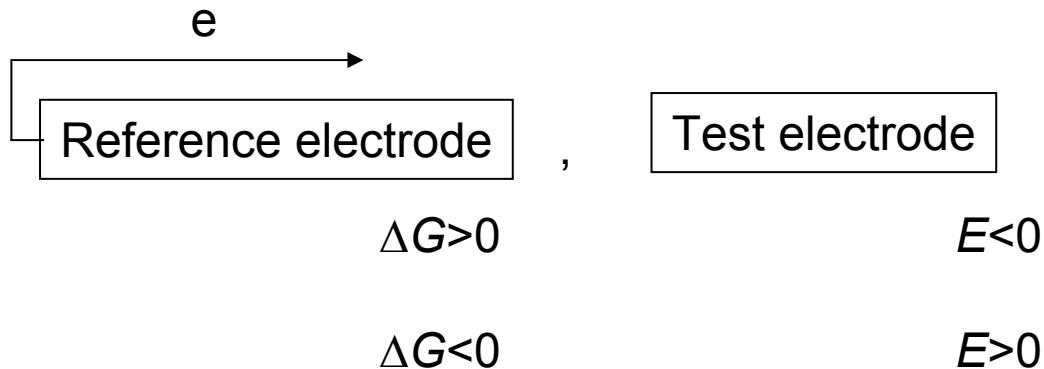
Calomel electrode

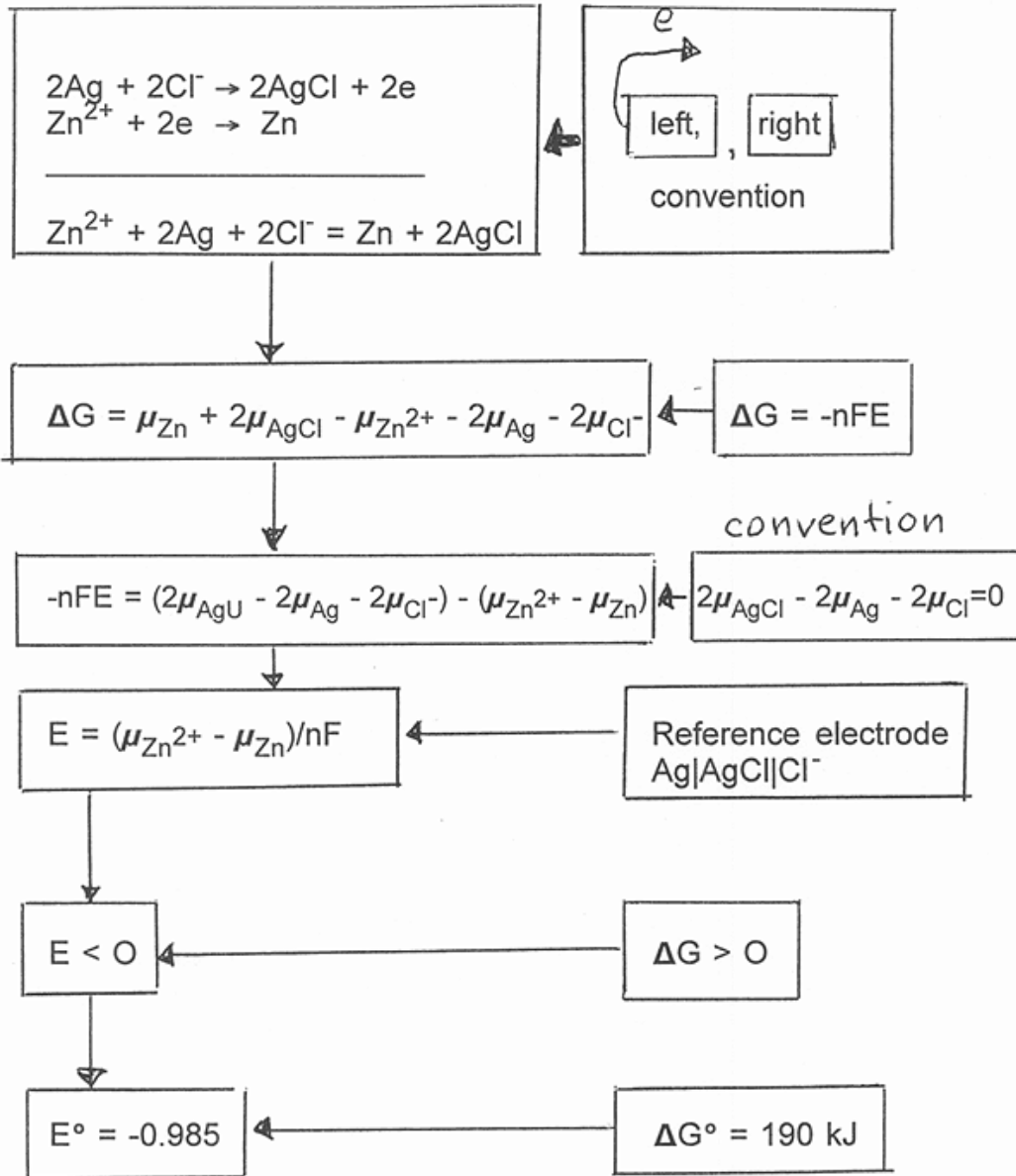


Silver chloride electrode

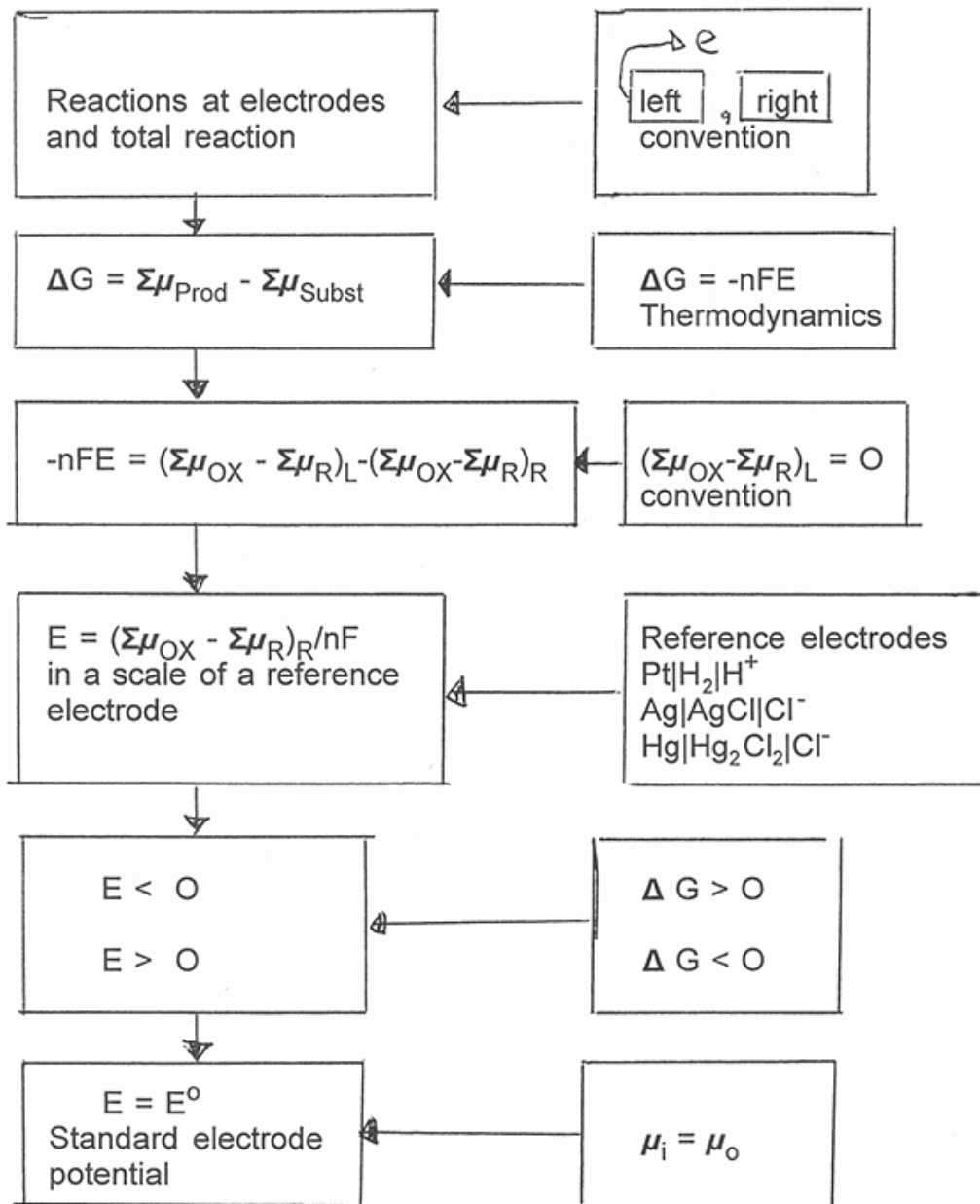
Electrode sign convention

Write electrode reactions such that electrons flow through an external circuit from the reference to the test electrode





Electrochemical cell



Nernst equation

$$2FE = \mu_{\text{Zn}^{2+}} - \mu_{\text{Zn}}$$

$$2FE = \mu_{\text{Zn}^{2+}}^{\circ} - \mu_{\text{Zn}}^{\circ} + RT \ln(a_{\text{Zn}^{2+}}/a_{\text{Zn}})$$

$$E = E^{\circ} + (RT/2F) \ln(a_{\text{Zn}^{2+}}/a_{\text{Zn}})$$

$$E = E^{\circ} + (RT/nF) \ln(a_{\text{OX}}/a_{\text{Red}})$$

electrode - transducer ↑

$$E^{\circ} = \frac{(\mu_{\text{Zn}^{2+}}^{\circ} - \mu_{\text{Zn}})}{2F}$$

or

$$E^{\circ} = \frac{(\mu_{\text{OX}}^{\circ} - \mu_{\text{Red}})}{nF}$$

Type of electrodes

1. Electrodes of the first order



metal in contact with its own ions:

$$E = (\mu_{\text{M}^{n+}} - \mu_{\text{M}})/nF = E^{\circ} + RT/F \ln a_{\text{M}^{n+}}$$

2. Electrodes of the second order, metal covered by insoluble salt of this metal in contact with solution of the anion of the insoluble salt



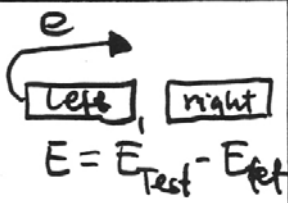
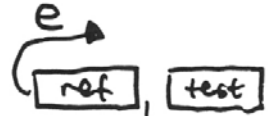
$$E = (\mu_{\text{AgCl}} - \mu_{\text{Ag}} - \mu_{\text{Cl}^{-}})/F = E^{\circ} - RT/F \ln a_{\text{Cl}^{-}}$$

3. Electrodes of the third order Metal covered by two films of two insoluble salts



electrodes sensitive to the metal of the second insoluble salt.

Summary of concepts and conventions

quantity	Assumptions	Conceptual non-measurable quantity	Convention
Electrochemical potential $\bar{\mu}$	separation: $\bar{\mu}_i = \mu_i + z_i F \phi$	ϕ - inner potential μ_i - chemical potential of an ionic species	
Electromotive force E	 $E = E_{\text{test}} - E_{\text{ref}}$	electrode potential	$E_{\text{ref}} = 0$ chemical potentials of all species of the reference electrode equal to zero
Electromotive force		sign of the electrode potential	 $E < 0; \Delta G > 0$ $E > 0; \Delta G < 0$

2.3 Conductance, transference numbers, mobility, flux and current

Transference number

When current flows through a cell a fraction t_+ is carried by cations and a fraction t_- by anions such that:

$$t_+ + t_- = 1$$

or in general

$$\sum_i t_i = 1$$

t_i is the transference or transport number

Conductance

Conductance of an electrolyte equal to the reciprocal or resistance is given by:

$$L = \frac{1}{R} = \frac{\kappa A}{l}$$

Where κ is the conductivity, A is the area and l is the length of a segment of electrolyte conducting current

Ionic mobility

Ionic mobility u_i is a limiting velocity of an ion in an electric field of unit field strength. Ionic mobility is measured in $\text{cm}^2 \text{V}^{-1} \text{s}^{-1}$ or (cm/s per V/m). It is related to the ionic conductivity κ by the formula:

$$\kappa = F \sum_i |z_i| u_i C_i$$

The transference number of ion i is the contribution to conductivity made by that ion divided by the total conductivity:

$$t_i = \frac{\kappa_i}{\kappa} = \frac{|z_i| u_i C_i}{\sum_j |z_j| u_j C_j}$$

Ionic mobilities in aqueous solution at 25 °C, $u/10^{-4} \text{ cm}^2 \text{ s}^{-1} \text{ V}^{-1}$

Cations		Anions	
H ⁺	36.23	OH ⁻	20.64
Li ⁺	4.01	F ⁻	5.70
Na ⁺	5.19	Cl ⁻	7.91
K ⁺	7.62	Br ⁻	8.09
Rb ⁺	7.92	I ⁻	7.96
Ag ⁺	6.42	NO ₃ ⁻	7.40
NH ₄ ⁺	7.63	CO ₃ ²⁻	7.46
Ca ²⁺	6.17	SO ₄ ²⁻	8.29
Cu ²⁺	5.56	CH ₃ CO ₂ ⁻	4.24
La ³⁺	7.21		

Equivalent conductivity

Defined by:

$$\Lambda = \frac{\kappa}{C|z|}$$

since $\kappa = F \sum_i |z_i| u_i C_i$ and $\kappa_i = F |z_i| u_i C_i$

$$\Lambda = F(u_+ + u_-)$$

or

$$\Lambda = (\lambda_+ + \lambda_-)$$

where

$$\lambda_i = F u_i$$

is the equivalent conductivity of individual ion

In the case of a single electrolyte :

$$t_i = \frac{\lambda_i}{\Lambda}$$

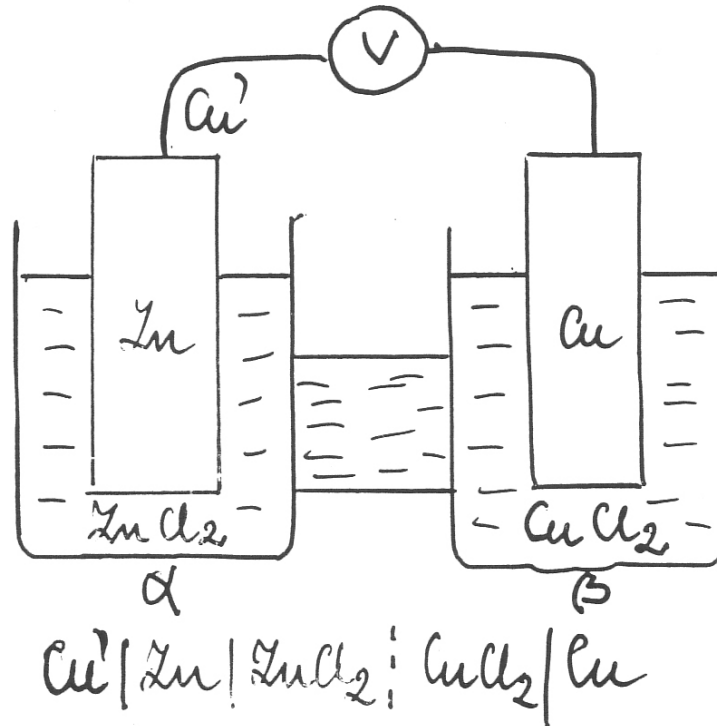
or

$$t_i = \frac{u_i}{u_+ + u_-}$$

or

$$t_i = \frac{|z_i| C_i \lambda_i}{\sum_j |z_j| C_j \lambda_j}$$

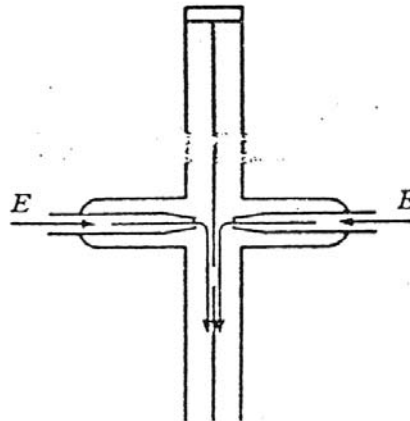
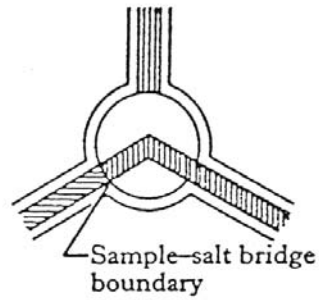
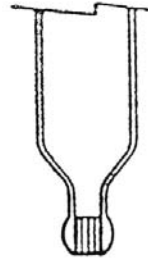
2.4 Electrochemical cell with a liquid junction potential



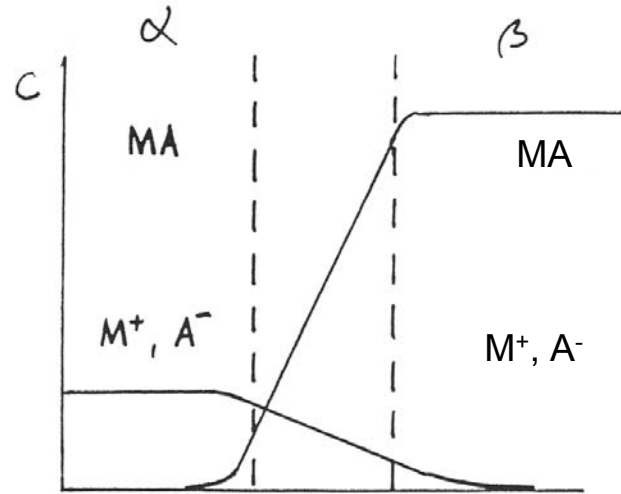
$$E = \phi(Cu) - \phi(Cu') = \{\phi(Zn) - \phi(Cu')\} + \{\phi(\alpha) - \phi(Zn)\} + \{\phi(\beta) - \phi(\alpha)\} + \{\phi(Cu) - \phi(\beta)\}$$

$$\{\phi(\beta) - \phi(\alpha)\} = E_{LJ}$$

Different ways to make the liquid junction potential

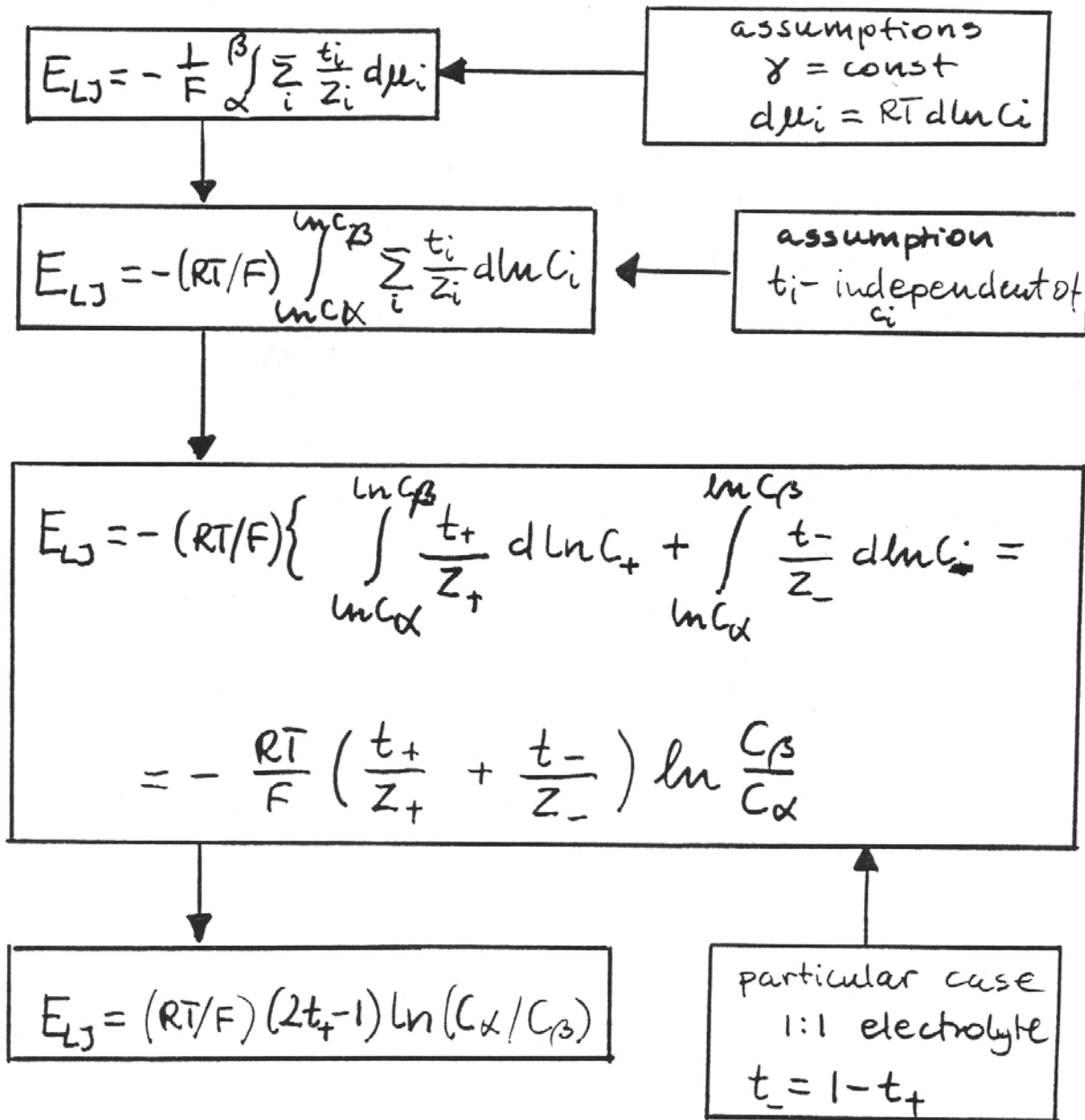


Boundary between two electrolyte solutions

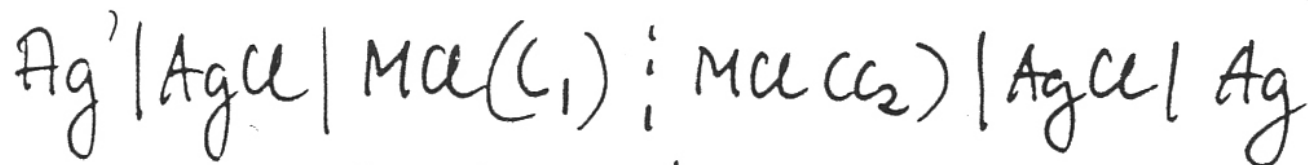


$$E_{LJ} = \phi_{\beta} - \phi_{\alpha} = -\frac{1}{F} \int_{\alpha}^{\beta} \sum_i \frac{t_i}{z_i} d\mu_i$$

Liquid junction potential between two different solutions of the same electrolyte



Computed Potentials of the Liquid Junction in Cells of the Type



$$C_1 = 0.04\text{M} ; C_2 = 0.005\text{M}$$

Electrolyte	t_M	Measured E/mV	E_{LJ}	calculated $E_2 - E_1$ mV
NaCl	0.391	39.6	-11.1	50.7
KCl	0.490	49.6	-1.0	50.6
HCl	0.826	84.2	+33.2	50.9

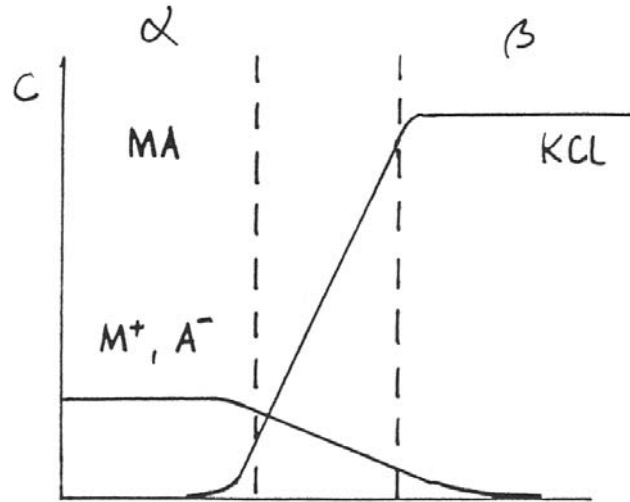
Henderson equation

Activity coefficients independent of concentration and the liquid junction a continuous mixture of the two electrolytes

$$E_{LJ} = \frac{RT}{F} \frac{\sum u_i z_i (c_i'' - c_i')}{\sum z^2 u_i (c_i'' - c_i')} \ln \frac{\sum z^2 c_i' u_i}{\sum z^2 c_i'' u_i}$$

How to eliminate liquid junction potential?

Consider the following interface



$$t_{A^-} = \frac{u_{A^-} C_{A^-}}{u_{A^-} C_{A^-} + u_{Cl^-} C_{Cl^-} + u_{K^+} C_{K^+} + u_{M^+} C_{M^+}}$$

$$t_{A^-} = \frac{u_{A^-} C_{A^-}}{u_{A^-} C_{A^-} + u_{Cl^-} C_{Cl^-} + u_{K^+} C_{K^+} + u_{M^+} C_{M^+}}$$

assume that $C_{KCl} \gg C_{MA}$ then $u_{Cl^-} C_{Cl^-} + u_{K^+} C_{K^+} \gg u_{A^-} C_{A^-} + u_{M^+} C_{M^+}$

in predominant fraction of the liquid – junction region:

$$t_{A^-} = \frac{u_{A^-}}{u_{Cl^-} + u_{K^+}} \left(\frac{C_{MA}}{C_{KCl}} \right) \ll 0$$

$$\text{and } t_{M^+} = \frac{u_{M^+}}{u_{Cl^-} + u_{K^+}} \left(\frac{C_{MA}}{C_{KCl}} \right) \ll 0$$

Consequently:

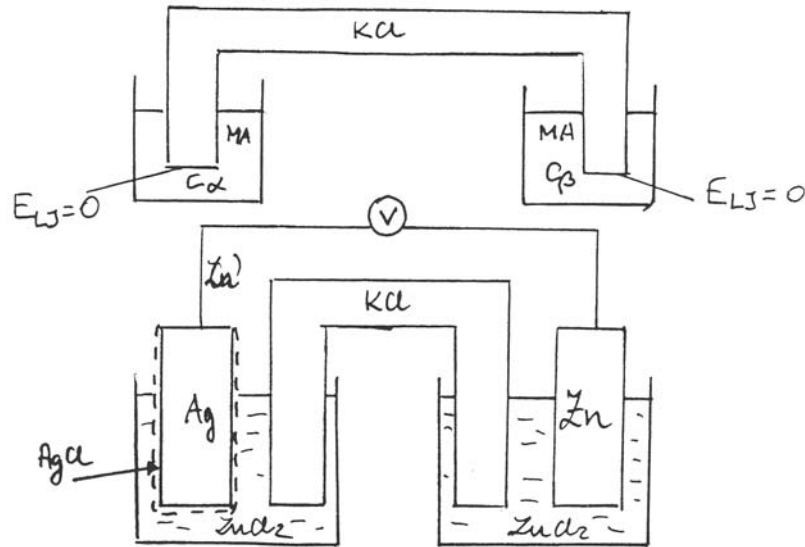
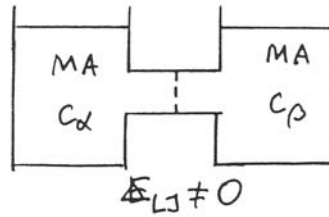
$$E_{LJ} = -\frac{1}{F} \int_{\alpha}^{\beta} \sum_i \frac{t_i}{z_i} d\mu_i = -\frac{1}{F} \int_{\alpha}^{\beta} (t_{K^+} d\mu_{K^+} - t_{Cl^-} d\mu_{Cl^-})$$

To a good approximation $d\mu_{K^+} = d\mu_{Cl^-} = \frac{1}{2} d\mu_{KCl}$ and since

$$t_{K^+} \approx t_{Cl^-}$$

$$E_{LJ} = -\frac{1}{F} \int_{\alpha}^{\beta} (t_{K^+} d\mu_{K^+} - t_{Cl^-} d\mu_{Cl^-}) = -\frac{1}{F} \int_{\alpha}^{\beta} \frac{1}{2} (t_{K^+} - t_{Cl^-}) d\mu_{KCl} \approx 0$$

Elimination of the liquid junction potential by a salt bridge



$$E = \frac{RT}{2F} \ln a_{Zn} + \text{const}$$

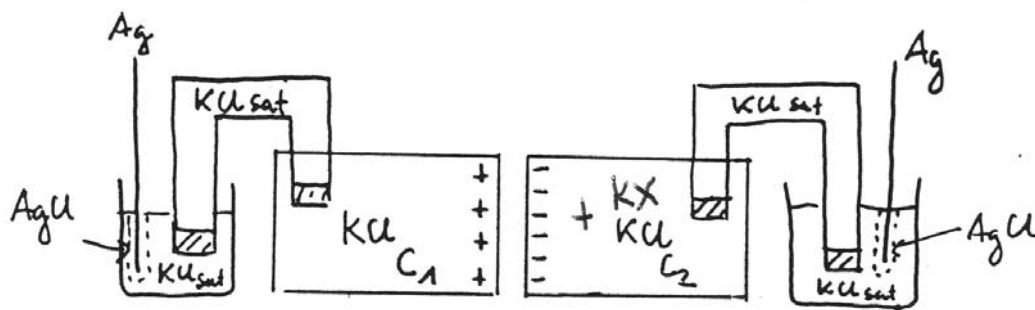
2.5 Donnan equilibrium and Donnan potential(IUPAC definitions)

Donnan equilibrium

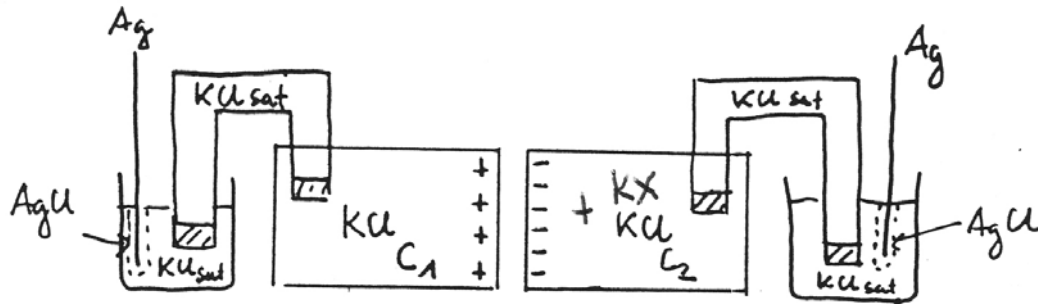
The equilibrium characterized by an unequal distribution of diffusible ions between two ionic solutions (one or both of the solutions may be gelled) separated by a membrane which is impermeable to at least one of the ionic species present, e.g. because they are too large to pass through the pores of the membrane. The membrane may be replaced by other kinds of restraint, such as gelation, the field of gravity, etc., which prevent some ionic components from moving from one phase to the other, but allow other components to do so.

Donnan emf (Donnan potential)

The potential difference E_D at zero electric current between two identical salt bridges, usually saturated KCl bridges (conveniently measured by linking them to two identical electrodes) inserted into two solutions in



Donnan equilibrium and Donnan potential



$$\bar{\mu}_K(1) = \bar{\mu}_K(2)$$

$$\bar{\mu}_{Cl}(1) = \bar{\mu}_{Cl}(2)$$

$$\bar{\mu}_i = \mu_i^\circ + RT \ln a_i + z_i F \phi$$

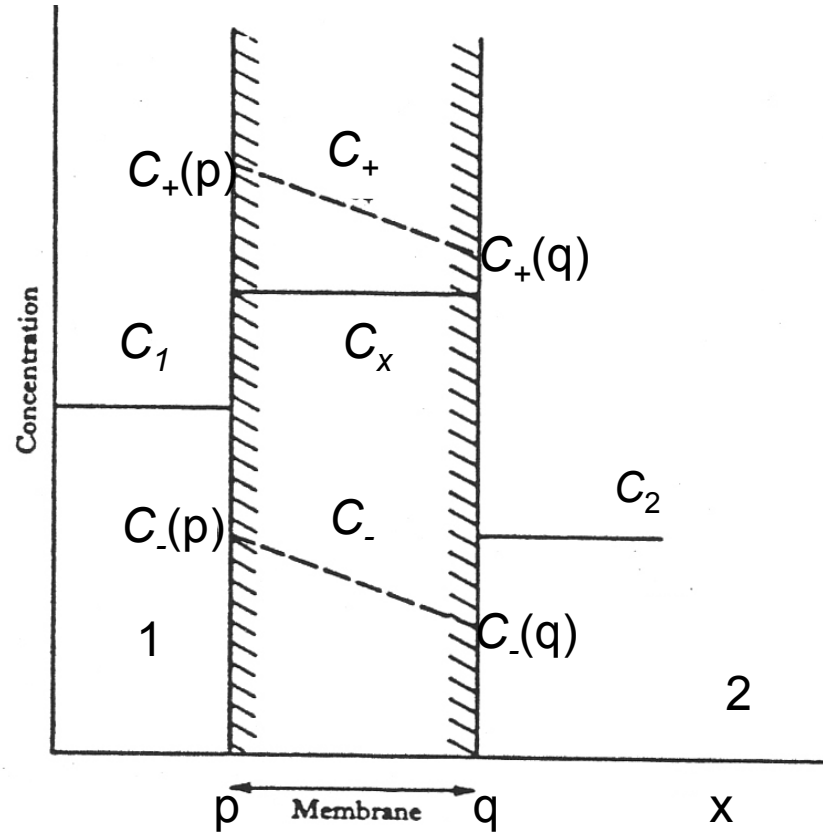
$$\mu_K^\circ + RT \ln a_{K(1)} + F \phi_1 = \mu_K^\circ + RT \ln a_{K(2)} + F \phi_2$$

$$\mu_{Cl}^\circ + RT \ln a_{Cl(1)} - F \phi_1 = \mu_{Cl}^\circ + RT \ln a_{Cl(2)} - F \phi_2$$

$$\Delta \phi_D = \phi_2 - \phi_1 = \frac{RT}{F} \ln \frac{a_{K(1)}}{a_{K(2)}} \approx \frac{RT}{F} \ln \frac{C_{K(1)}}{C_{K(2)}} = \frac{RT}{F} \ln \frac{C_{Cl(2)}}{C_{Cl(1)}}$$

Donnan Potential

2.6 Selectively permeable membranes



$$\Delta\phi = \phi(2) - \phi(1) = \{\phi(2) - \phi(q)\} + \{\phi(q) - \phi(p)\} + \{\phi(p) - \phi(1)\}$$

$$\Delta\phi = \Delta\phi_D(2) + \Delta\phi_{LJ} + \Delta\phi_D(1)$$

Primary ion-selective electrodes

1. Crystalline Electrodes contain mobile ions of one sign and fixed sites of opposite sign. They may be homogeneous or heterogeneous.
 - a. *Homogeneous membrane electrodes* are ion-selective electrodes in which the membrane is a crystalline material prepared from either a single compound or a homogeneous mixture of compounds (e.g., Ag_2S , $\text{AgI}/\text{Ag}_2\text{S}$). **or AgBr**

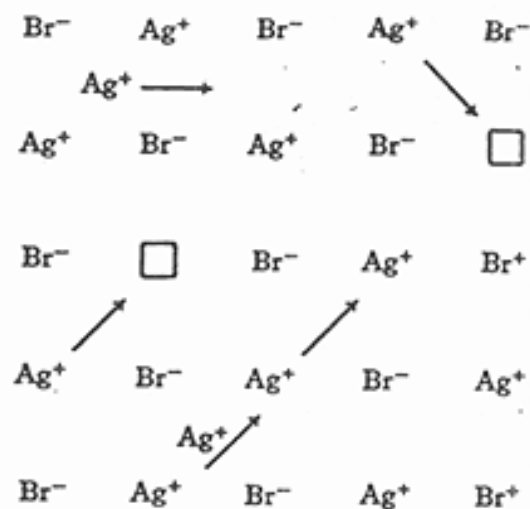


TABLE 5. Numerical Values for the Defect Activities of Various Silver Compounds⁽²²⁾

Compound	Defect activities (25°C, mol liter ⁻¹)
AgCl	1.5×10^{-9}
AgBr	5.0×10^{-7}
AgI	1.0×10^{-6}
Ag_2S	3.1×10^{-6}

Frenkel's scheme for the transport of silver ions in the AgBr crystal lattice. The silver cations are in interstitial positions in the crystal lattice and the same number of unoccupied lattice positions are in the cation part of the lattice

2. Non-crystalline Electrodes. In these electrodes, a support matrix, containing an ion exchanger (either cationic or anionic), a plasticizer solvent, and possibly an uncharged, selectivity-enhancing species, form the ion-selective membrane which is usually interposed between two aqueous solutions. The matrix can be either macroporous (e.g., poly(propylene carbonate) filter, glass frit, etc.) or microporous (e.g., "thirsty" glass or polymeric material such as PVC) yielding with the ion-exchanger and the solvent a "solidified" homogeneous mixture. These electrodes exhibit a response due to the presence of the *selectivity-enhancing species* (which exhibit an ion-exchange property) in the membrane. The *solvent-polymeric-membrane* is an example.
- a. *Rigid, self-supporting, matrix electrodes* (e.g., synthetic cross-linked polymer or glass electrodes) are ion-selective electrodes in which the sensing membrane is a thin polymer with fixed sites or a thin piece of glass. The chemical composition of the polymer (e.g. polystyrenesulfonate, sulfonated poly(tetrafluoroethylene), poly(vinyl chloride) aminated) or the glass determines the membrane selectivity. *pH glass electrode* see in section 3.4.12.

General purpose glass electrode

Glass composition

22% Na₂O

6% CaO

72% SiO₂

SiO₄⁴⁻ - charged silicate groups - charge is balanced by cations

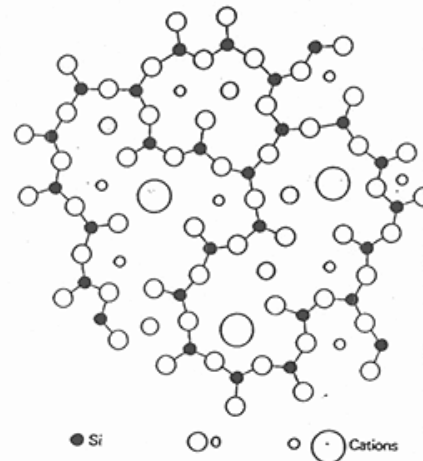
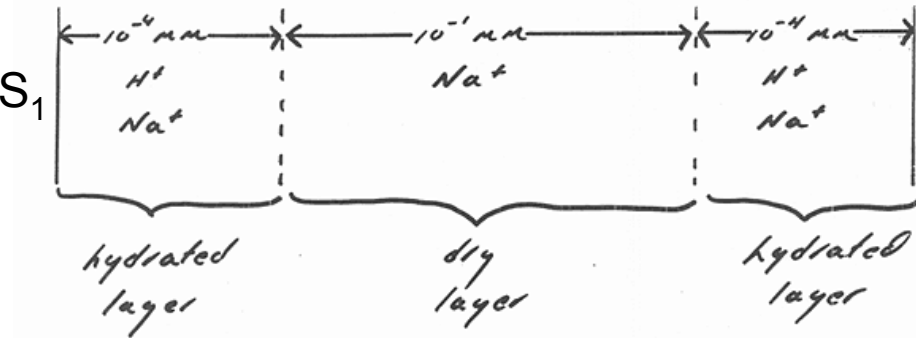


FIGURE 20-4 Cross-sectional view of a silicate glass structure. In addition to the three Si—O bonds shown, each silicon is bonded to an additional oxygen atom, either above or below the plane of the paper. (Adapted with permission

GLASS ELECTRODE



S_2 Glass electrodes suitable for determining Li^+, Na^+, K^+

Cation

Glass composition

Li^+

15% Li_2O - 25% Al_2O_3 - 60% SiO_2

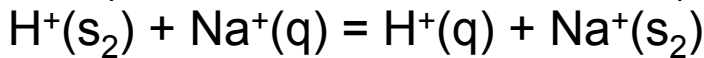
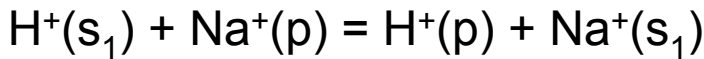
Na^+

11% Na_2O - 18% Al_2O_3 - 71% SiO_2

K^+

27% K_2O - 5% Al_2O_3 - 68% SiO_2

Conduction across the membrane occurs by the following reactions:



In the dry layer mobile Na^+ ions are responsible for conduction

The above equilibria are determined by the H^+ activities in the solutions on the two sides of the membrane

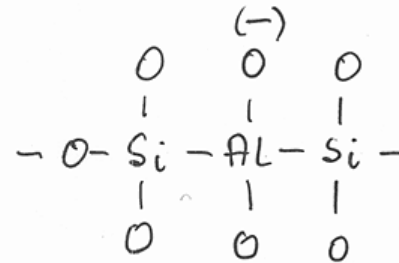
Diffusion coefficients of Na^+

Hydrated layer $5 \times 10^{-11} \text{ cm}^2\text{s}^{-1}$

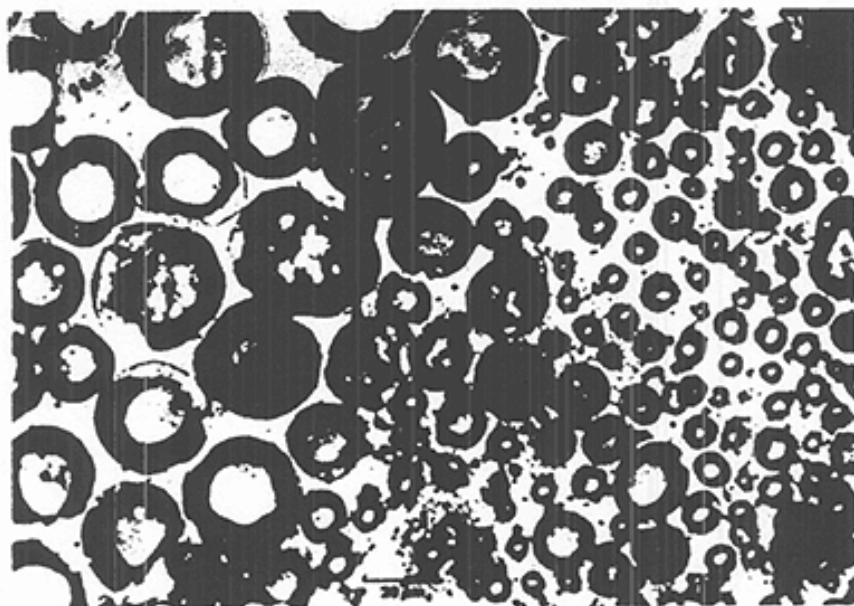
Dry layer $5 \times 10^{-14} \text{ cm}^2\text{s}^{-1}$

Aqueous solution $5 \times 10^{-6} \text{ cm}^2\text{s}^{-1}$

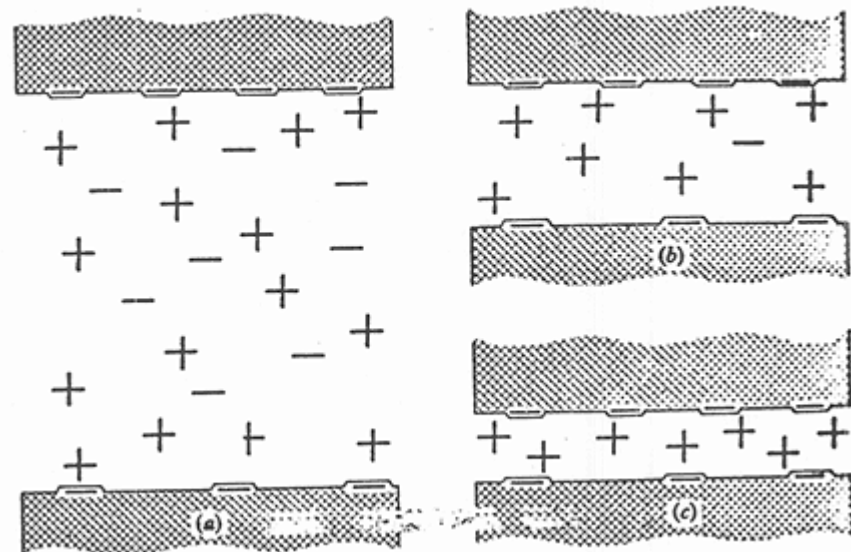
Glass electrodes sensitive to alkali metal ions - contain trivalent metal ions such as Al^{3+} which create the ion exchange centers



A

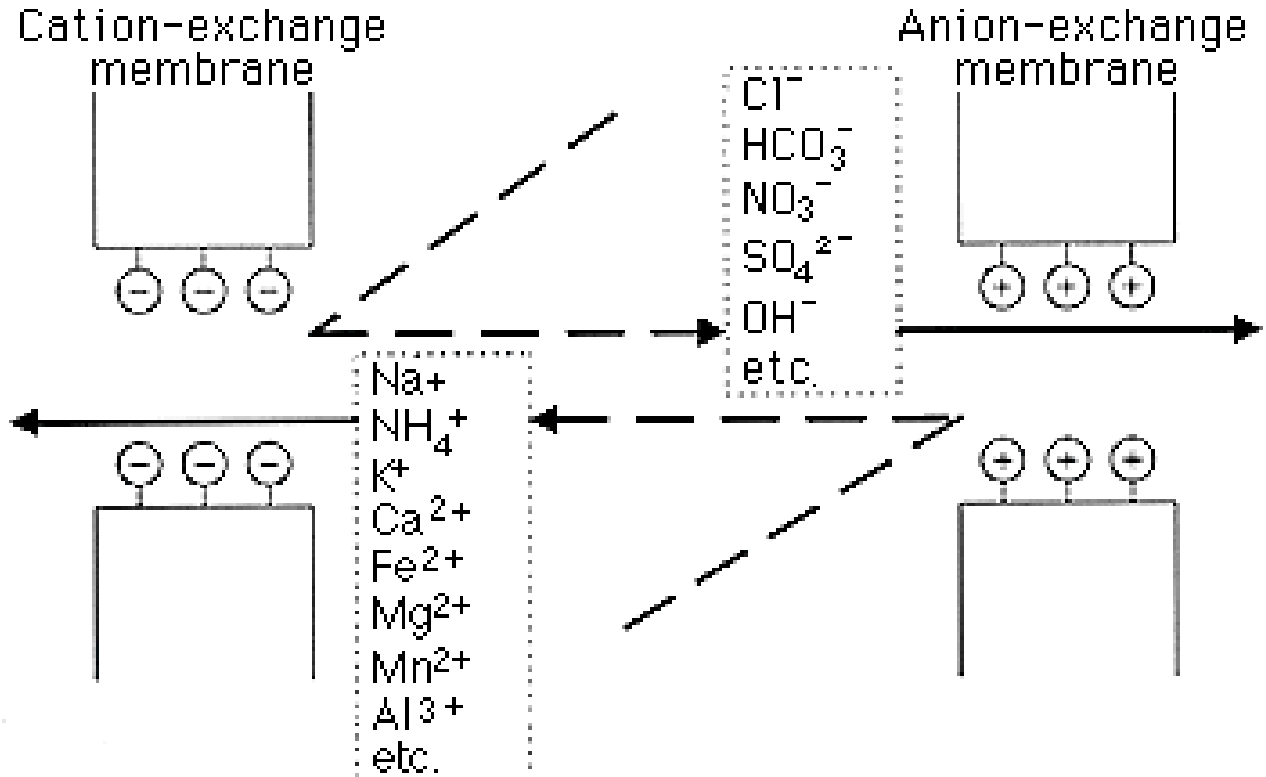


B

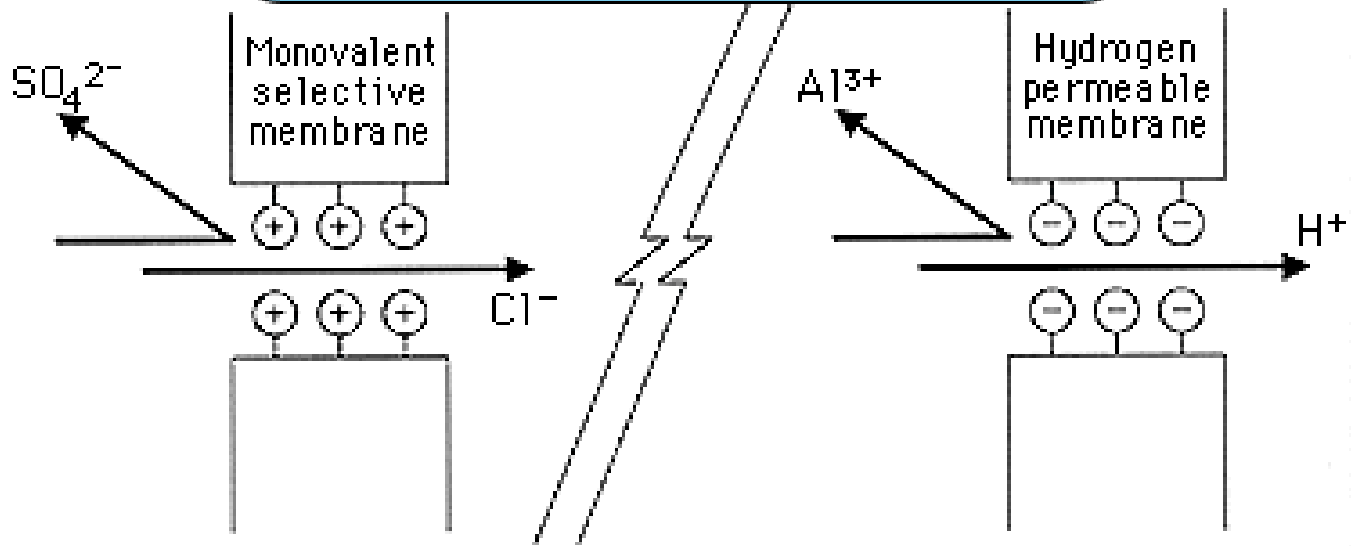


A Visible-light microscope photomicrograph showing pores (dark circles) in polyvinyl chloride matrix membrane incorporating didecylphosphoric acid-dioctylphenylphosphonate shaken with a molar solution of calcium chloride [358]. By permission of the Society for Analytical Chemistry, London.

B Ion distribution in a porous membrane with fixed negative ions: (a) pore diameter is large so that the electric double layer and the pore walls do not affect the passage of anions; (b) pore diameter is smaller so that the electric double layer decreases the permeability for anions; (c) the pore diameter is very small so that the electric double layer completely suppresses the permeability for anions. After Sollner [1025].

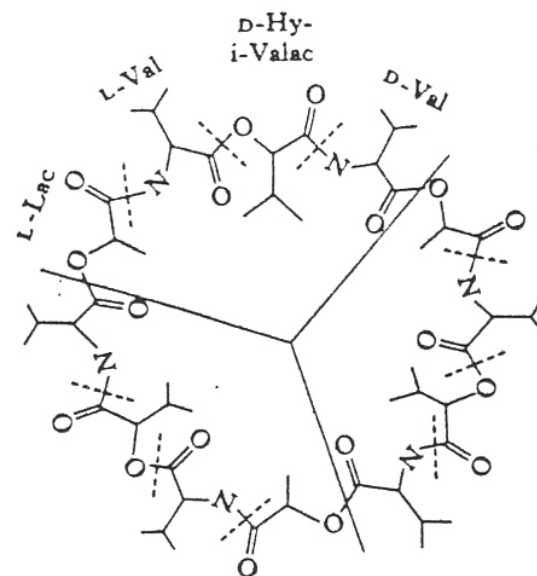
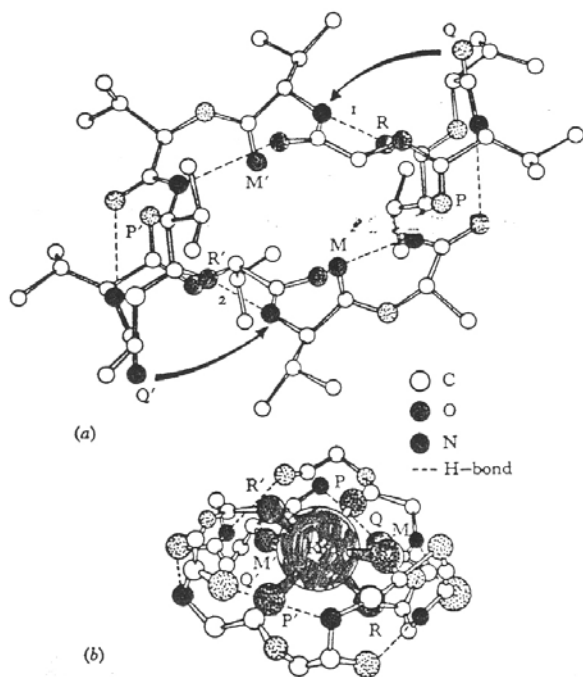


For example such membrane as this is available.



b. *Electrodes with mobile charged sites:*

1. Positively charged, hydrophobic cations (e.g., quaternary ammonium cations or cations of substitutionally inert, transition metal complexes of such ligands as derivatives of 1,10-phenanthroline) of which, when dissolved in a suitable organic solvent and held in an inert support (e.g., poly(propylene



valinomycin

Liquid Membranes with Dissolved Ion – Exchanger

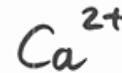
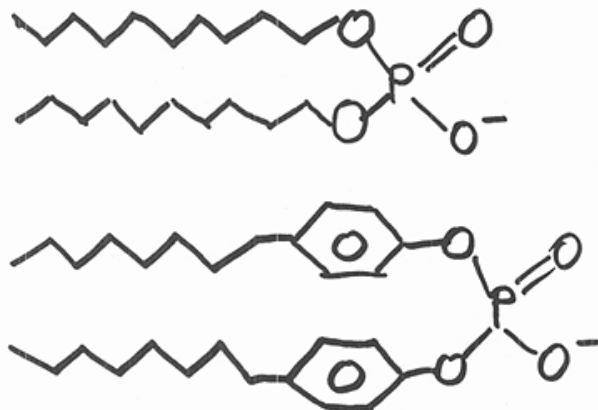
Liquid membranes are formed from immiscible liquids that contain exchangers selectively binding certain ions.

Early liquid membranes were prepared from immiscible liquid and ion exchangers that were retained in the immiscible liquid.

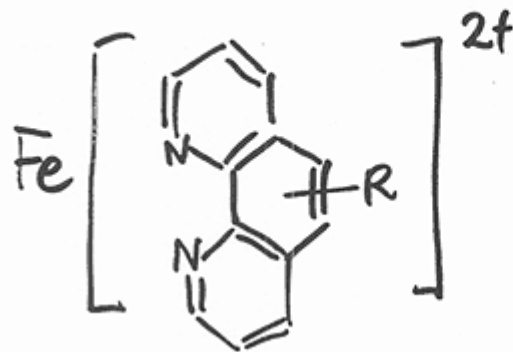
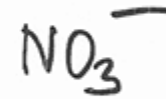
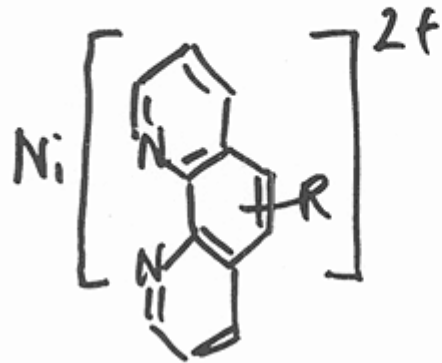
Recently ion – exchangers are dissolved in a PVC membrane. The liquid ion- exchanger and PVC are dissolved in a solvent such as tetrahydrofuran. Evaporation of the solvent leaves a flexible membrane, which can be cut and cemented to the end of a glass or plastic tube.

There are three kinds of active substances in liquid membranes:

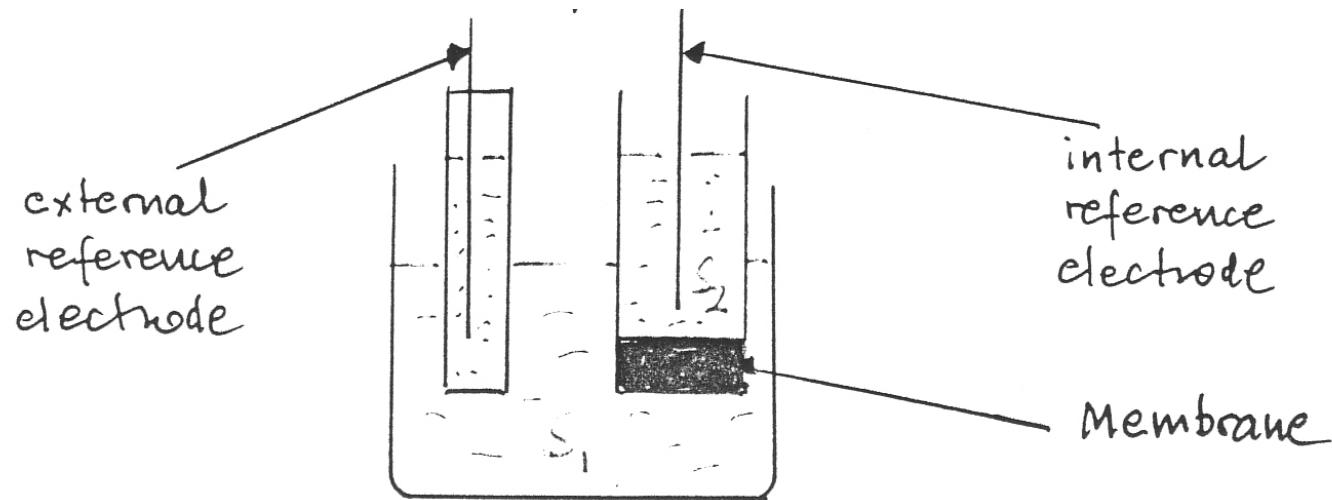
cation exchangers



anion exchangers



2.8. Membrane potential – overview



$$E_{\text{cell}} = E_{\text{ref,int}} - E_{\text{ref,ext}} + \sum E_{L_j} + E_M$$

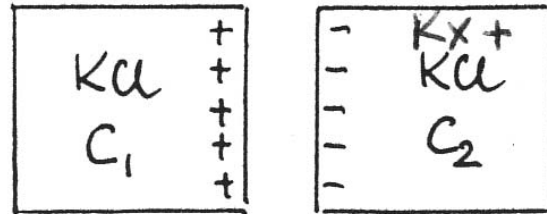
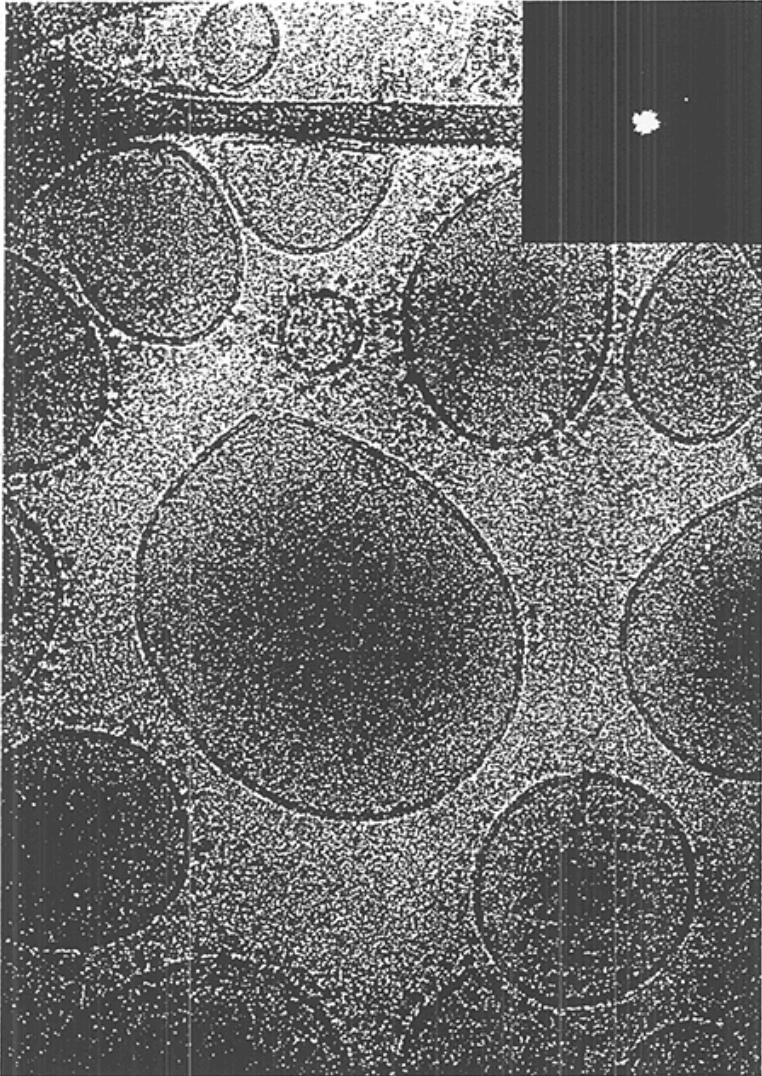
$$\text{if } E_{\text{ref,int}} = E_{\text{ref,ext}} \text{ and } \sum E_{L_j} \approx 0$$

$$E_{\text{cell}} = E_M = \phi(2) - \phi(1)$$

1. Ultrathin membranes (phospholipid bilayer)

1. Biological membranes

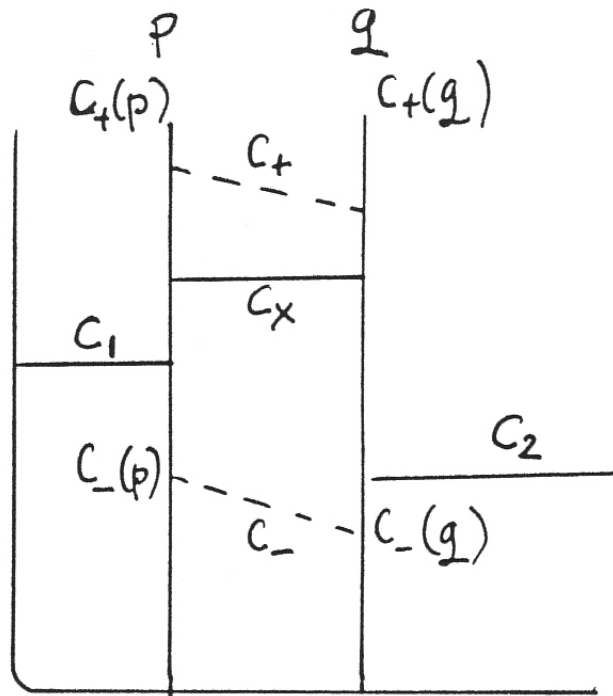
TEM image with nm resolution shows phospholipid bilayer with protein channels that provide selective transport of K^+ and Na^+ across the membrane



Donnan equilibrium

$$\Delta\phi_0 = \phi(2) - \phi(1) = \frac{RT}{F} \ln \frac{C_{K^+}(1)}{C_{K^+}(2)} =$$
$$= - \frac{RT}{F} \ln \frac{C_{Cl^-}(1)}{C_{Cl^-}(2)}$$

2. Macroscopic membranes



$$E_M = \phi_2 - \phi_1 = \underbrace{\{\phi(2) - \phi(q)\}}_{\Delta\phi_D(2)} + \underbrace{\{\phi(q) - \phi(p)\}}_{\Delta\phi_L(2)} + \underbrace{\{\phi(p) - \phi(1)\}}_{\Delta\phi_O(1)}$$

$$E_M = \Delta\phi_D(2) + \Delta\phi_L(2) + \Delta\phi_O(1)$$

General expression for the membrane potential

$$E_M = \frac{RT}{z_k F} \ln \left\{ a_{K^+}(II) + K_{KJ}^{\text{pot}} a_{J^+}(I) \right\} + \text{const}$$

2.8 Selectivity of the membrane electrode

No electrode is entirely selective towards the ion specified. The presence of other ions can seriously impair electrode performance.

If the analyte contains interfering J with activity a_j , the ISE potential is given by :

$$E_M = E_0 + \frac{RT}{z_i F} \ln \left\{ a_i + K_{ij} a_j^{z_i/z_j} \right\}$$

where K_{ij} is called the selectivity coefficient of the ISE for ion I with respect to ion J. K_{ij} is a measure of the effect of interfering ions on the determination of the test ion I. For example, for Na^+ being the interfering ion for the calcium ion selective electrode, $K_{\text{CaNa}} = 10^{-3}$. This means that the electrode is 1000 times more responsive to Ca^{2+} than to Na^+

$$E_M = \Delta\phi_M = \frac{RT}{z_i F} \ln \left\{ a_i + \sum K_{ij}^{\text{pot}} a_j \frac{z_i}{z_j} \right\} + \text{const}$$

Limiting solutions

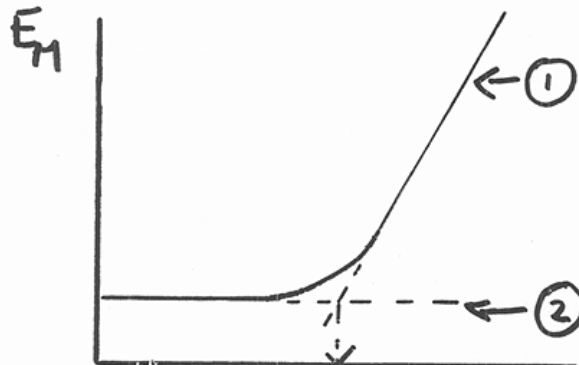
$$\textcircled{1} \quad a_i \gg K_{ij} a_j \frac{z_i}{z_j}$$

$$E_M = E_0 + \frac{RT}{z_i F} \ln a_i \quad (\text{Nernstian behaviour})$$

$$\textcircled{2} \quad a_i \ll K_{ij} a_j \frac{z_i}{z_j}$$

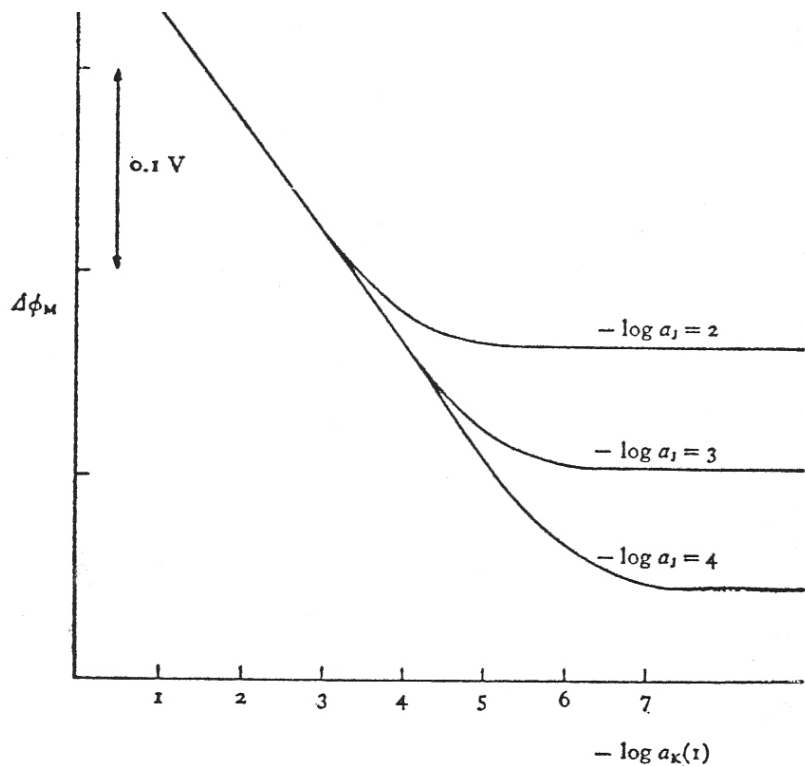
$$E_M = E_0 + \frac{RT}{z_i F} \ln K_{ij} a_j \frac{z_i}{z_j} =$$

$$= E_0 + \frac{RT}{z_i F} \ln K_{ij} + \frac{RT}{z_j F} \ln a_j$$

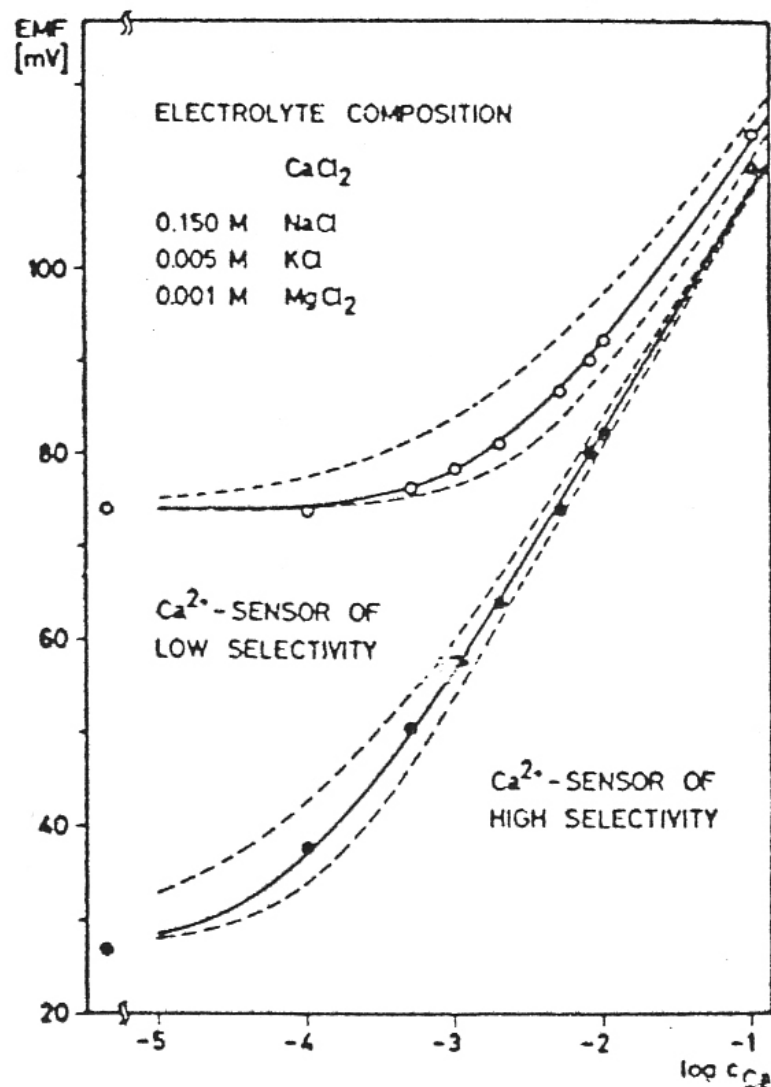


$$a_i^* = K_{ij} a_j \frac{z_i}{z_j} ; \quad K_{ij} = \frac{a_i^*}{a_j \frac{z_i}{z_j}}$$

$$E = E_0 + \frac{RT}{z_i F} \ln \left\{ a_{i_k} + K_{ij} a_j \left(\frac{z_i}{z_j} \right) \right\}$$



Dependence of $\Delta\phi_M$ on the activity of ion K^+ at various activities of ion J^+ when there is a diffusion potential across the membrane.

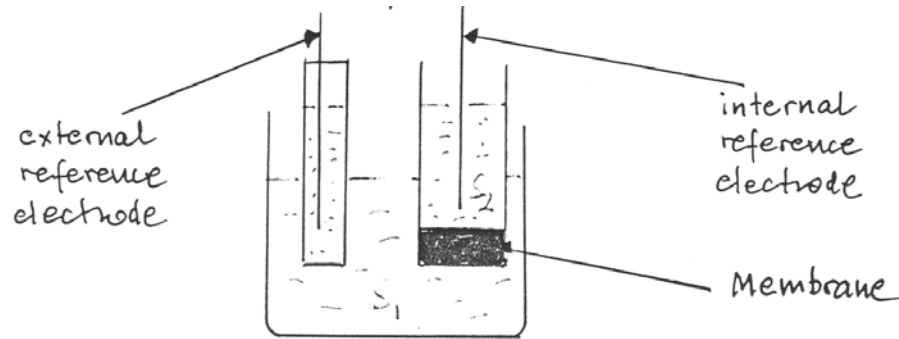


Comparison between calculated and measured EMF-response curves for different Ca^{2+} -sensitive carrier-based PVC membrane electrodes

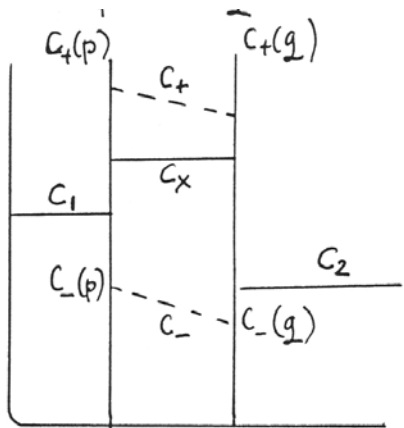
Selectivity Coefficients k_{ij} for Some Important Electrode Systems (Manufacturers' Data)

Electrode system	Interferences
Ca ²⁺ (Beckman)	Fe ²⁺ 5, Cu ²⁺ 0.33, Mg ²⁺ 0.9, Ba ²⁺ 0.1
Ca ²⁺ (Corning)	Mg ²⁺ 0.01, Ba ²⁺ 0.01, Ni ²⁺ 0.01, Na ⁺ 10 ⁻³
Ca ²⁺ (Orion)	Zu ²⁺ 3.2, Fe ²⁺ 0.80, Pb ²⁺ 0.63, Cu ²⁺ 0.27, Mg ²⁺ 0.01, Ba ²⁺ 0.01, Na ⁺ 1.6 × 10 ⁻³
Ca ²⁺ (Philips)	Zu ²⁺ 5.0—0.9, Fe ²⁺ 0.45, Cu ²⁺ 0.07, Mg ²⁺ 0.032, Ba ²⁺ 0.02
Ca ²⁺ + Mg ²⁺ (Beckman)	Zu ²⁺ 1.0, Ba ²⁺ 1.0, Na ⁺ 0.01, K ⁺ 0.01
Ca ²⁺ + Mg ²⁺ (Orion)	Zu ²⁺ 3.5, Fe ²⁺ 3.5, Cu ²⁺ 3.1, Ba ²⁺ 0.94, Na ⁺ 0.01
NO ₃ ⁻ (Beckman)	ClO ₄ ⁻ 100, NO ₂ ⁻ 0.045, Cl ⁻ 0.01, SO ₄ ²⁻ 10 ⁻⁵
NO ₃ ⁻ (Corning)	ClO ₄ ⁻ 1000, Cl ⁻ 4 × 10 ⁻³ , SO ₄ ²⁻ 10 ⁻³
NO ₃ ⁻ (Orion)	ClO ₄ ⁻ 1000, NO ₂ ⁻ 0.06, Cl ⁻ 6 × 10 ⁻³ , SO ₄ ²⁻ 6 × 10 ⁻⁴
ClO ₄ ⁻ (Beckman)	I ⁻ 0.033 NO ₃ 0.005, SO ₄ ²⁻ 10 ⁻⁴
ClO ₄ ⁻ (Corning)	I ⁻ 0.001, NO ₃ ⁻ 0.001, SO ₄ ²⁻ 0.001
ClO ₄ ⁻ (Orion)	OH ⁻ 1.0, I ⁻ 0.012, NO ₃ ⁻ 0.0015, SO ₄ ²⁻ 1.6 × 10 ⁻⁴
K ⁺ (Beckman)	Rb ⁺ 2.2, Cs ⁺ 0.5, NH ₄ ⁺ 0.014, Na ⁺ 2 × 10 ⁻⁴ , 3 × 10 ⁻⁴
K ⁺ (Corning)	Rb ⁺ 10, Cs ⁺ 20, NH ₄ ⁺ 0.023, Na ⁺ 0.012
K ⁺ (Philips)	Rb ⁺ 1.9, Cs ⁺ 0.38, NH ₄ ⁺ 0.012, Na ⁺ 2.6 × 10 ⁻⁴ , Li ⁺ 2.1 × 10 ⁻⁴
K ⁺ (Orion)	Rb ⁺ 2.2, Cs ⁺ 0.5, NH ₄ ⁺ 0.05, Na ⁺ 0.09, Li ⁺ 0.03
NH ₄ ⁺ (Philips)	K ⁺ 0.12, Rb ⁺ 0.043, Cs ⁺ 0.0048, Li ⁺ 0.0042, Na ⁺ 0.002
F ⁻ (Beckman)	OH ⁻ 0.1
F ⁻ (Orion)	OH ⁻ 0.1

Review



$$E_{\text{cell}} = E_M = \phi(2) - \phi(1)$$



$$E_M = \phi_2 - \phi_1 = \underbrace{\{\phi(2) - \phi(g)\}}_{\Delta\phi_D(2)} + \underbrace{\{\phi(g) - \phi(p)\}}_{\Delta\phi_{LJ}} + \underbrace{\{\phi(p) - \phi(1)\}}_{\Delta\phi_D(1)}$$

$$E_M = \Delta\phi_D(2) + \Delta\phi_{LJ} + \Delta\phi_D(1)$$

1. Solid state membrane (AgCl pelet)

$$\Delta\phi_{LJ} = 0$$

2. Membrane with dissolved ion exchanger

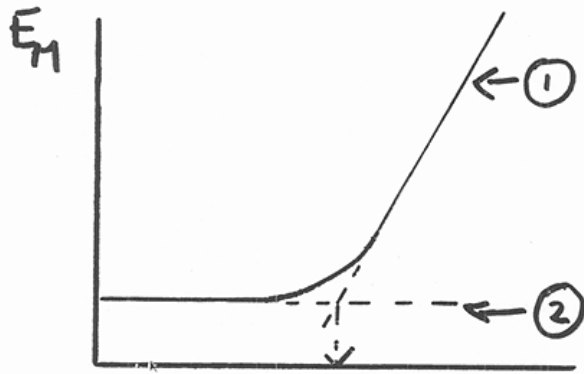
$$\Delta\phi_{LJ} = 0$$

3. Membrane with a fixed ion exchanger

$$\Delta\phi_{LJ} \neq 0$$

General expression for the membrane potential

$$E_M = \Delta\phi_M = \frac{RT}{Fz_i} \ln \left\{ a_i + K_{ij}^{pot} a_j^{\frac{z_i}{z_j}} \right\}$$



$a_i^* = K_{ij} a_j^{z_i/z_j}$; $K_{ij} = \frac{a_i^*}{a_j^{z_i/z_j}}$

Membrane	$\frac{K_{KJ}^{pot}}{u_K u_J}$
1. Fixed ion exchanger $\Delta\phi_{LJ} \neq 0$	$\frac{u_K}{u_J} K_{KJ}$
2. Solid state membrane $\Delta\phi_{LJ} = 0$	$\frac{K_{So, AgCl}}{K_{So, AgI}}$
3. Liquid membrane with dissolved ion exchanger $\Delta\phi_{LJ} = 0$	K_{KJ}

Activity versus Concentration

- **Electrodes respond to Activity not Concentration**
- **Activity and Concentration related by activity Coefficient**

$$a_x = [X] \gamma_x$$

- γ_x **is activity coefficient – it depends on the ionic strength of the solution**

At low ionic strength, $\gamma_x \rightarrow 1$

Ionic strength

$$I = 0.5 \sum_i C_i z_i^2$$

C_i – concentration, z_i – ionic charge, sum extends over all ions in solution

Debye- Hueckel provided expression for the activity coefficient:

$$\log \gamma = - 0.51 z_i^2 \sqrt{I} \quad \text{at } 25^\circ \text{ C}$$

In general electrode response is related to activity rather than analyte concentration

However, we are interested primarily to know concentration. In principle, the determination of this quantity from a potentiometric measurements requires activity coefficient data.

More often than not activity coefficients will be unavailable because the ionic strength of the solution is either unknown or so high that the Deby – Hueckel equation is not applicable.

In order to circumvent the problem of the activity coefficient an excess of an inert electrolyte (ionic strength buffer) and the standard addition methods are used.

2.9 Quantitative analysis – Standard addition method

Standard addition method:

- 1) Use an excess of an “inert electrolyte” (0.15M NaCl in Ca²⁺ analysis) to keep the ionic strength constant ($\gamma = \text{constant}$).
- 2) Take the measurement of the unknown:

$$E_1 = E_0 + \frac{RT}{Fz_A} \ln C_A \gamma$$

- 3) Spike unknown with a standard solution (volume V_s , concentration C_s)

$$E_2 = E_1 + \Delta E = E_0 + \frac{RT}{Fz_A} \ln \left(\gamma \frac{C_A V_A + C_s V_s}{V_A + V_s} \right)$$

- 4) Calculate the difference $E_2 - E_1 = \Delta E$

$$\Delta E = \frac{RT}{Fz_A} \ln \left(\frac{C_A V_A + C_s V_s}{C_A (V_A + V_s)} \right) \quad \text{or} \quad 10^{\frac{z_A F \Delta E}{2.3 RT}} = \frac{C_A V_A + C_s V_s}{C_A (V_A + V_s)}$$

and after rearrangement

$$C_A = \frac{C_s}{10^{\frac{z_A F \Delta E}{2.3 RT}} \left(1 + \frac{V_A}{V_s} \right) - \frac{V_A}{V_s}}$$

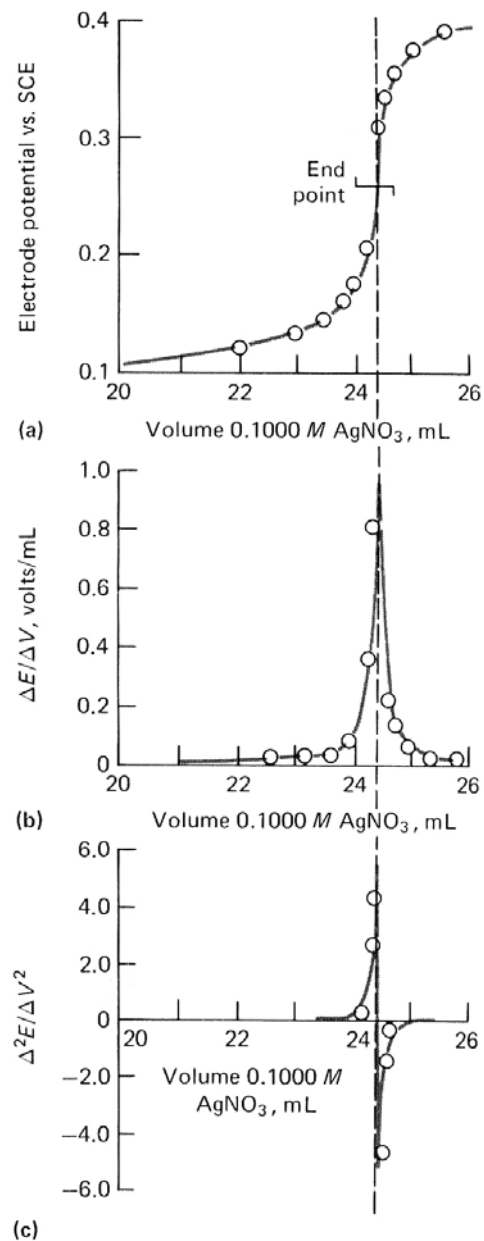
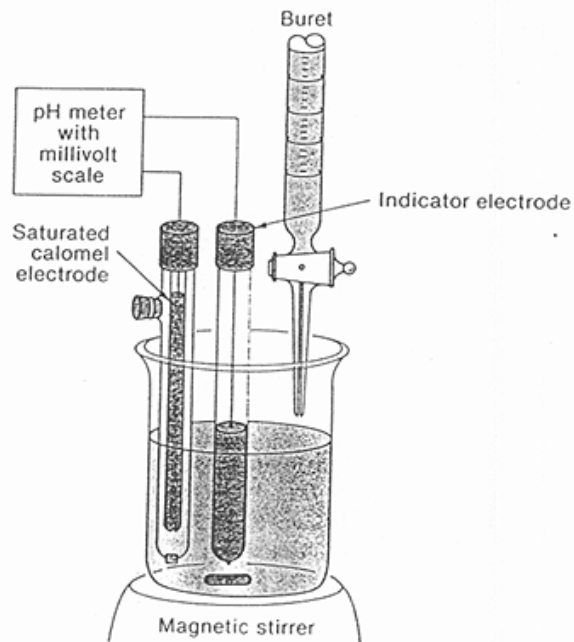
Potentiometric titrations

The measurement of the potential of a suitable indicator electrode permits the establishment of the equilibrium point for a titration.

The potentiometric endpoint provides inherently more accurate data than the corresponding method that makes use of indicators. It is particularly useful for titration of colored solutions.

Potentiometric titration is readily applied with automatic titration devices.

Apparatus for potentiometric titrations



(a) Potentiometric titration curve for 2.433 meq of Cl^- with 0.1000 M AgNO_3 . (b) First-derivative curve. (c) Second-derivative curve.

Potentiometric titration - Gran method

$$A + T = AT$$

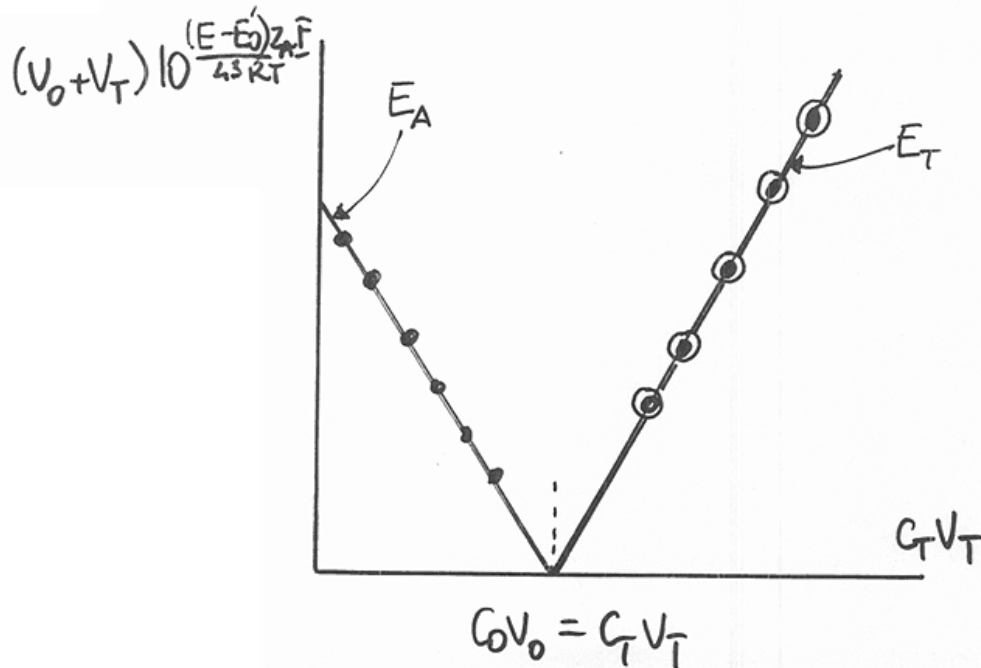
$$C_A = (V_0 C_0 - V_T C_T) / (V_0 + V_T)$$

$$E = \text{const} + \frac{RT}{z_A F} \ln \gamma_A C_A \quad (\text{const} = E_0)$$

$$E = E_0 + \frac{RT}{z_A F} \ln \left\{ \gamma_A \frac{V_0 C_0 - V_T C_T}{V_0 + V_T} \right\}$$

assume $\gamma_A = \text{const}$

$$C_0 V_0 - V_T C_T = (V_0 + V_T) 10^{(E - E_0) z_A F / 2.3 RT}$$



ISE – sources of errors

1. Liquid junction potentials
2. Drift
3. Changes in the activity coefficient
4. Storage
5. Interferences

ISE – Figures of Merit

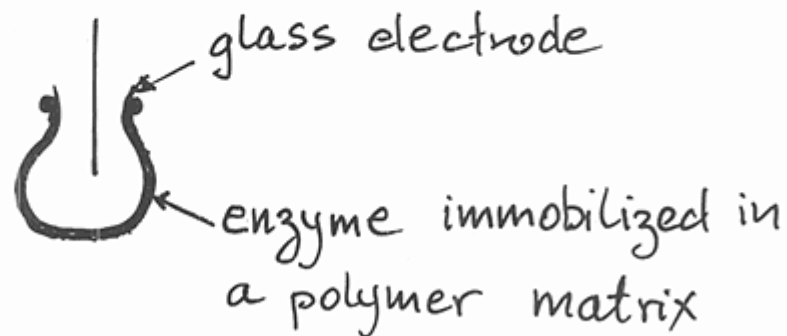
- detection limit 0.1 ppm
- accuracy 1 to 5 %
- precision better than accuracy
- Selectivity high
- cost very low

Activity errors resulting
From errors in the measured
potential

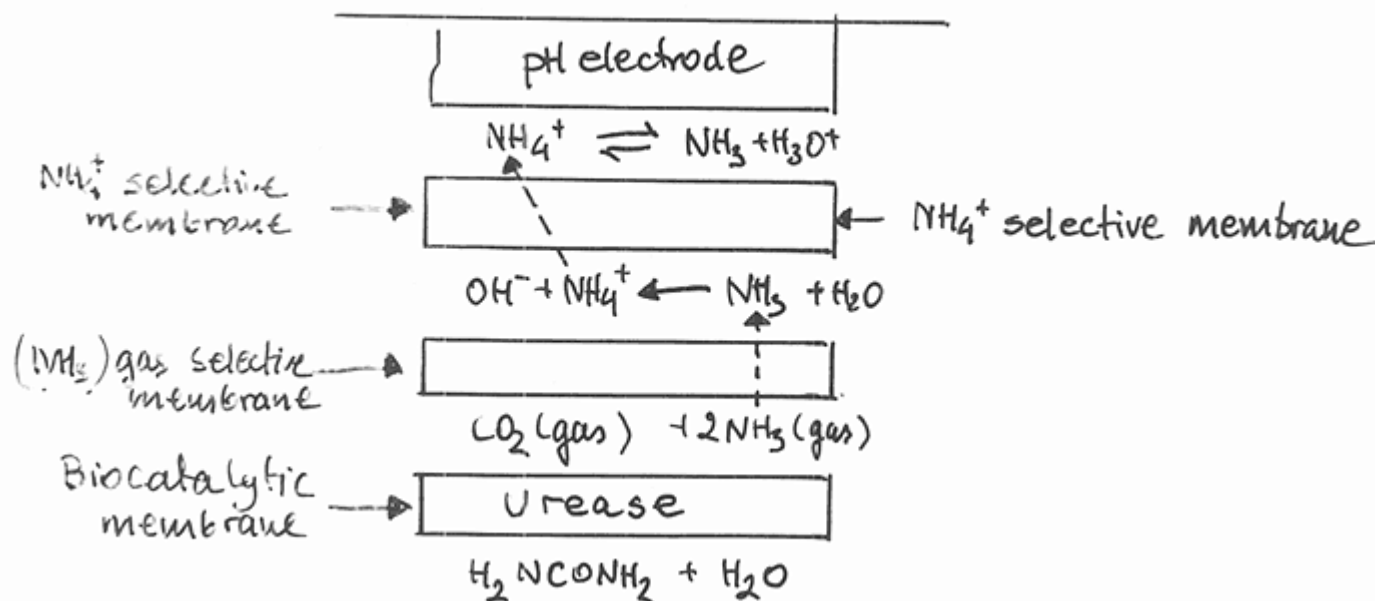
$\Delta E/mV$	% error
0.1	0.4
1.0	4.0
2.0	8.1
5.0	21.5

2.11 Biosensors

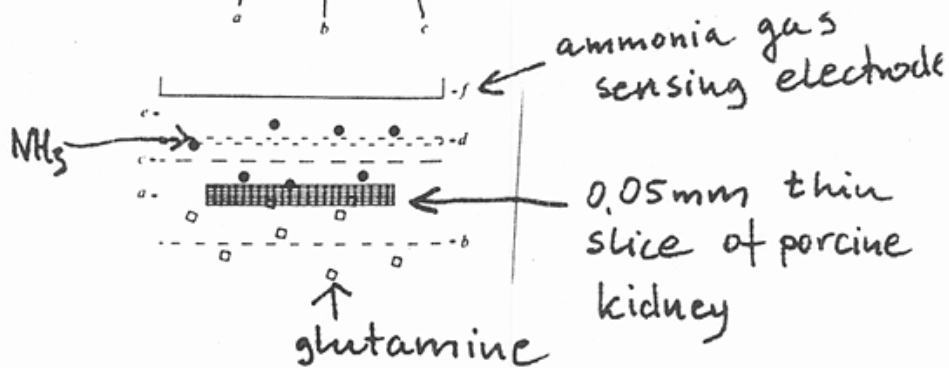
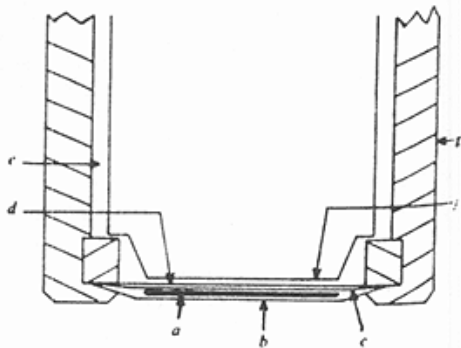
a. Enzyme electrode



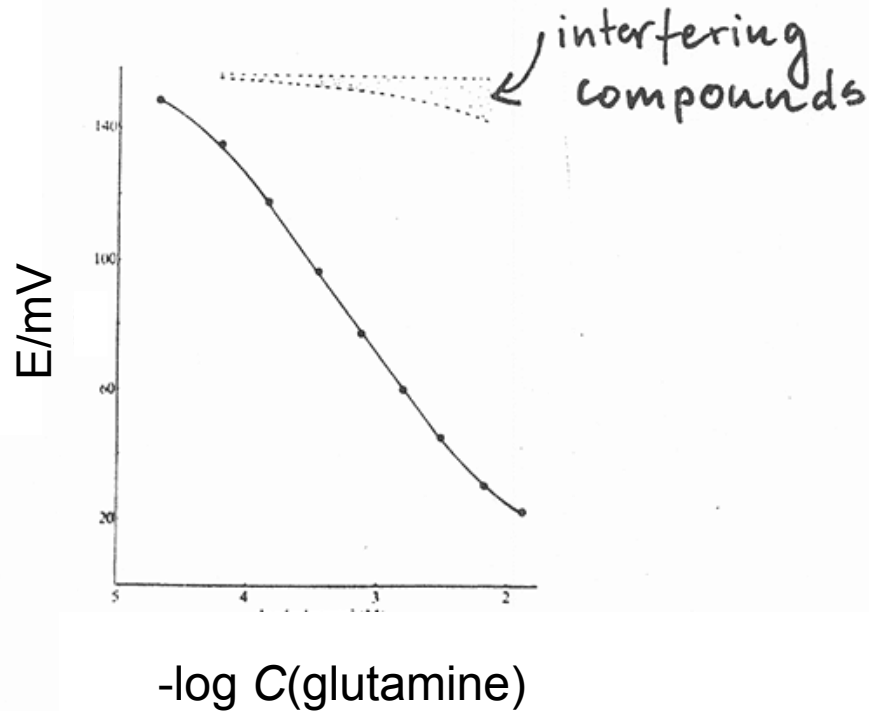
Structure of a biosensor

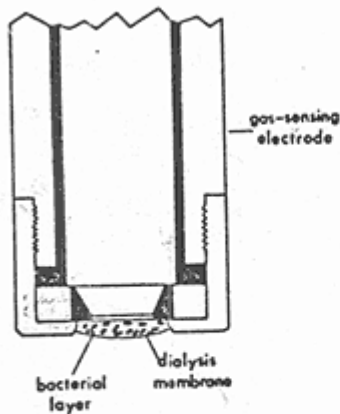


b) Tissue electrode



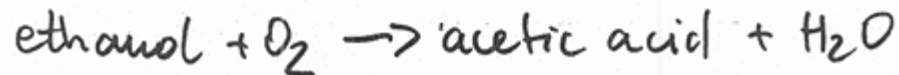
kidney tissue contains glutaminase





c) Bacterial electrode

Fig. 14. Bacterial electrode.



Potentiometric Bacterial Electrodes

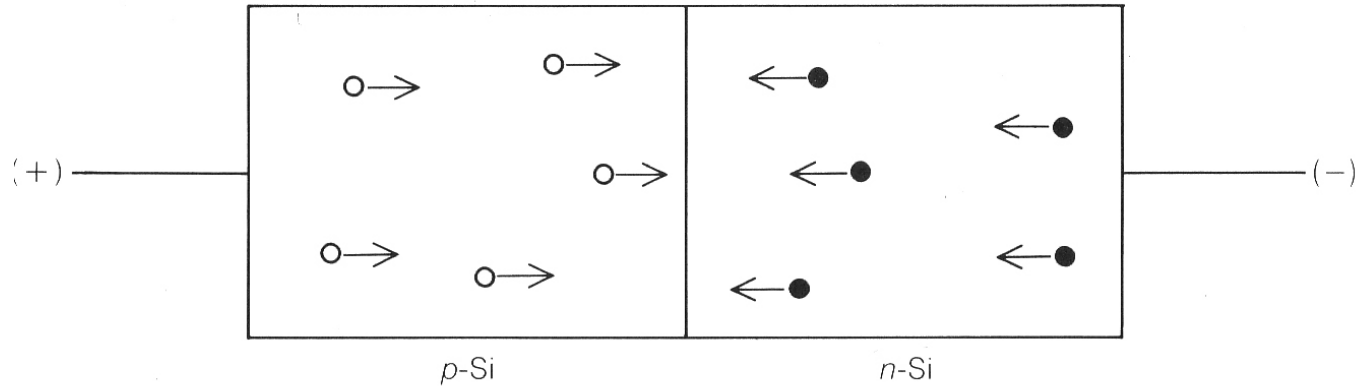
Substrate	Bacterium	Electrode	Concentration range (M)*	Reference
L-Arginine	<i>Streptococcus faecium</i> ATCC # 9790	NH ₃ gas sensing	5 × 10 ⁻⁵ - 1 × 10 ⁻³	249
L-Aspartate	<i>Bacterium cadaveris</i> ATCC # 9760	NH ₃ gas sensing	3 × 10 ⁻⁴ - 7 × 10 ⁻³	250
L-Glutamine	<i>Sarcina flava</i> ATCC # 147	NH ₃ gas sensing	2 × 10 ⁻⁵ - 1 × 10 ⁻²	251
L-Cysteine	<i>Proteus morganii</i> ATCC # 8019	H ₂ S gas sensing	5 × 10 ⁻⁵ - 9 × 10 ⁻⁴	252
NAD	NADase and <i>Escherichia coli</i> ATCC # 27195	NH ₃ gas sensing	5 × 10 ⁻⁵ - 8 × 10 ⁻⁴	253
Nitrate	<i>Azotobacter vinelandii</i> ATCC # 9104	NH ₃ gas sensing	1 × 10 ⁻⁵ - 8 × 10 ⁻⁴	254

*Analytically useful range.

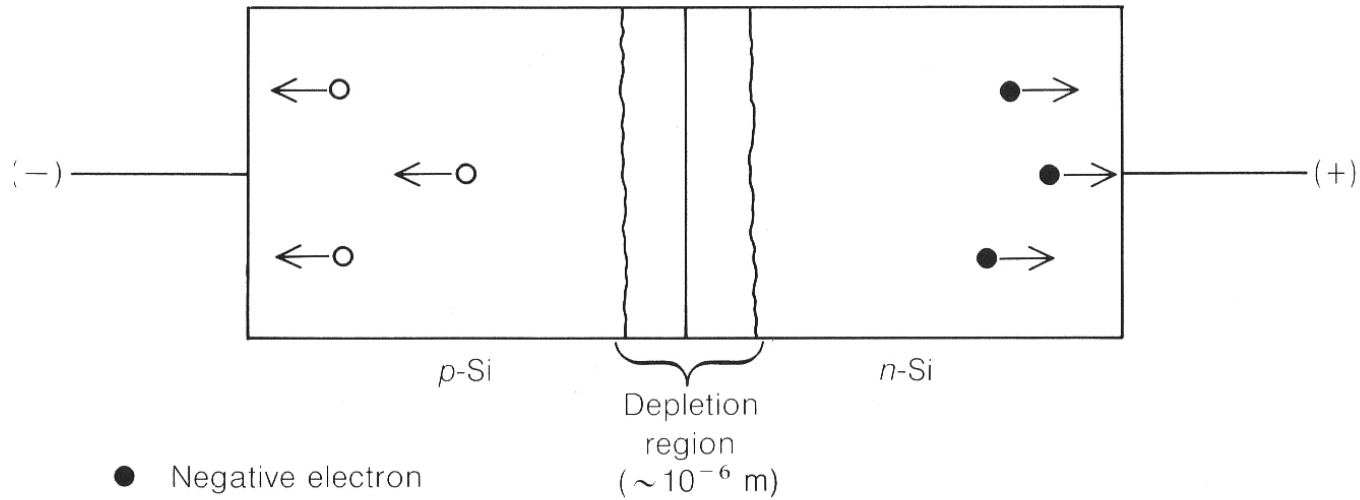
d) Chemically modified field effect transistor

pn-junction

Forward bias (current flows)



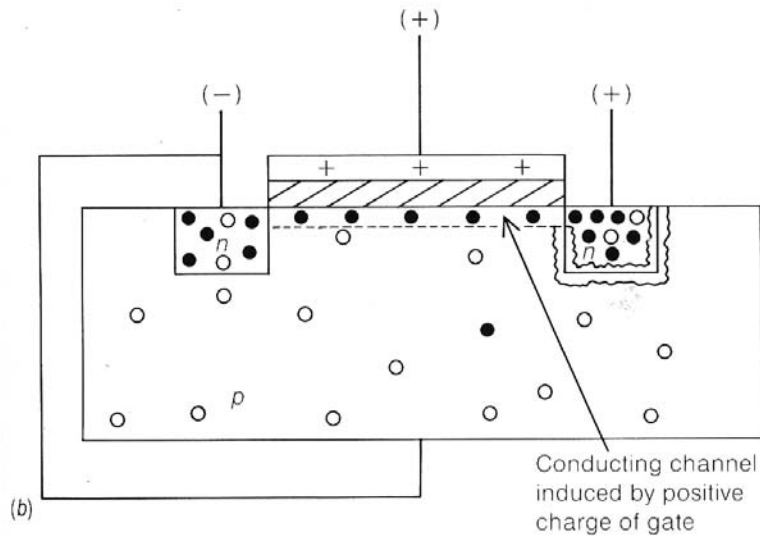
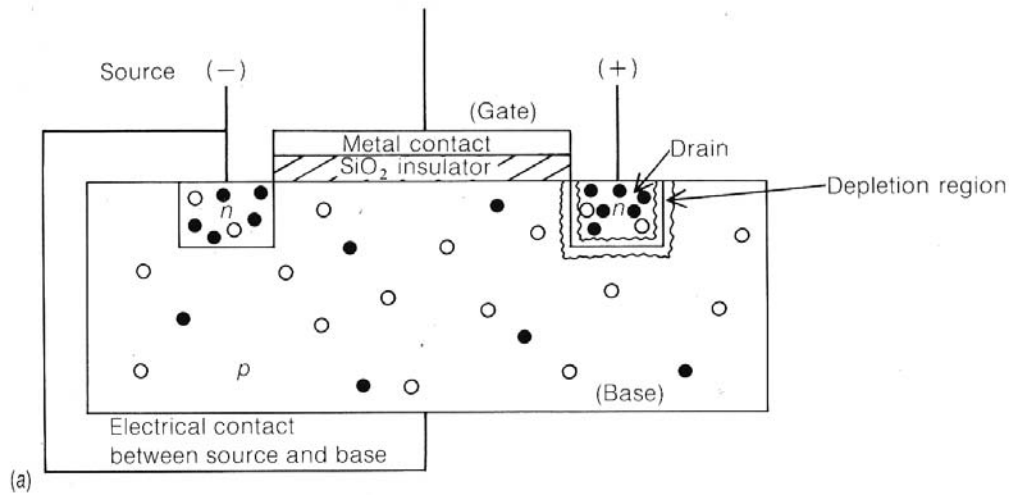
Reverse bias (no current flows)



● Negative electron

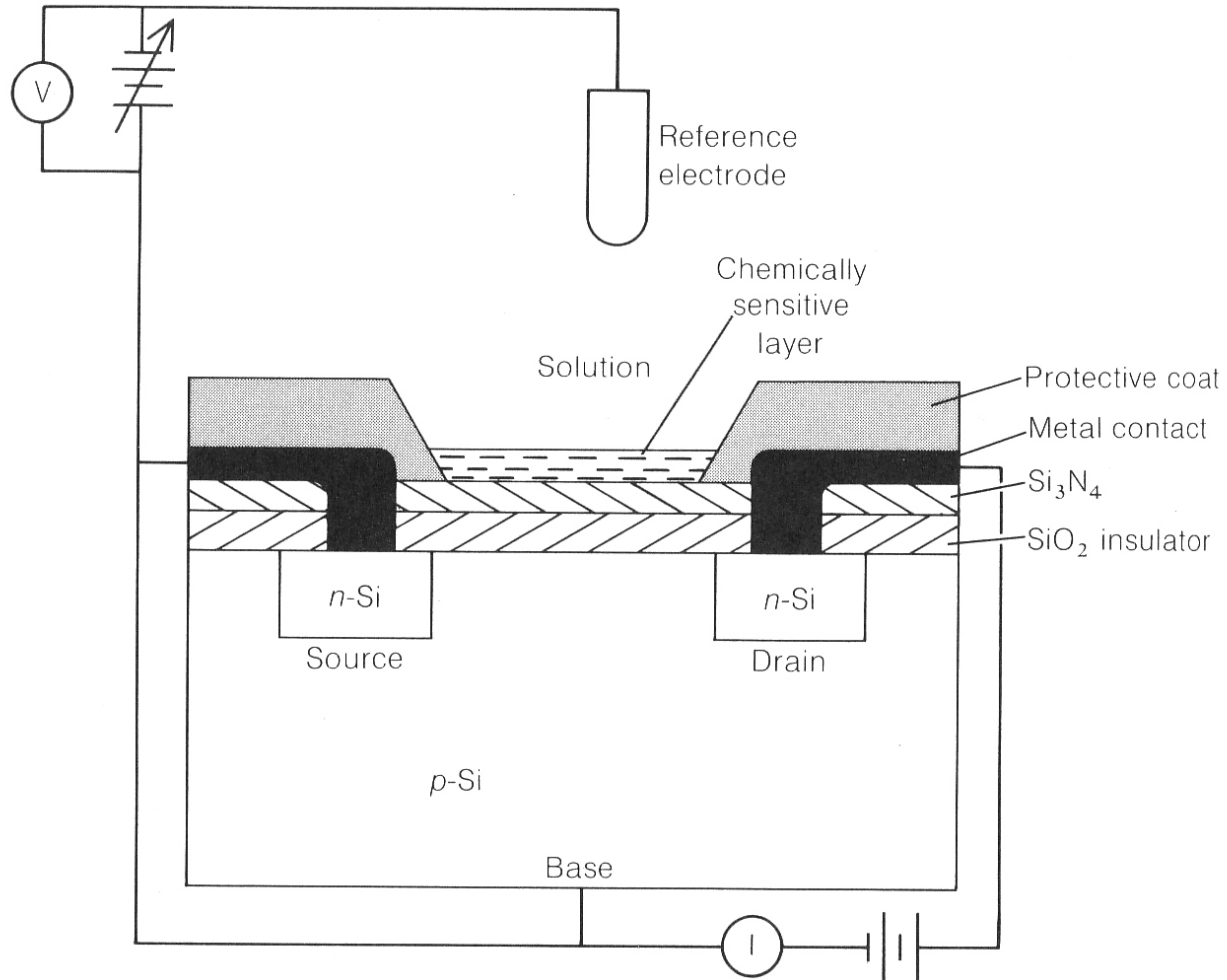
○ Positive hole

Field effect transistor



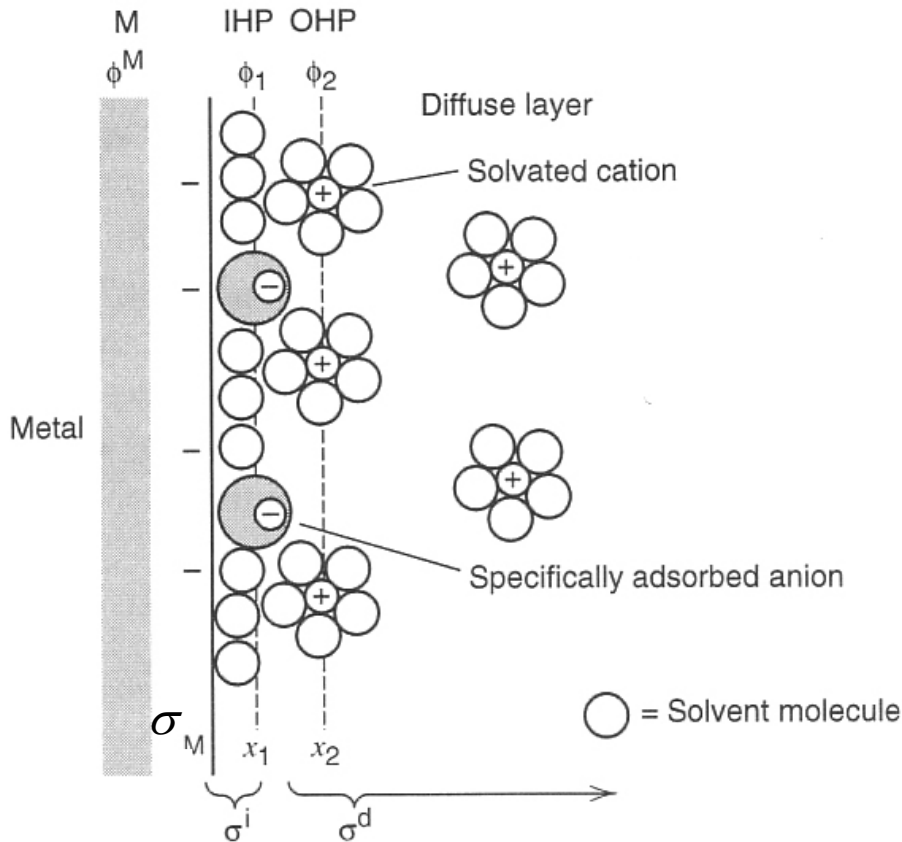
Operation of a field effect transistor.
 (a) Nearly random distribution of holes and electrons in the base in the absence of gate potential. (b) Positive potential at the gate causes electrons to accumulate in a channel beneath the gate. Current can flow through this channel between the source and drain.

Chemically modified field effect transistor



3. Introduction to electrometric methods

3.1 Structure of the metal interface



neutrality condition

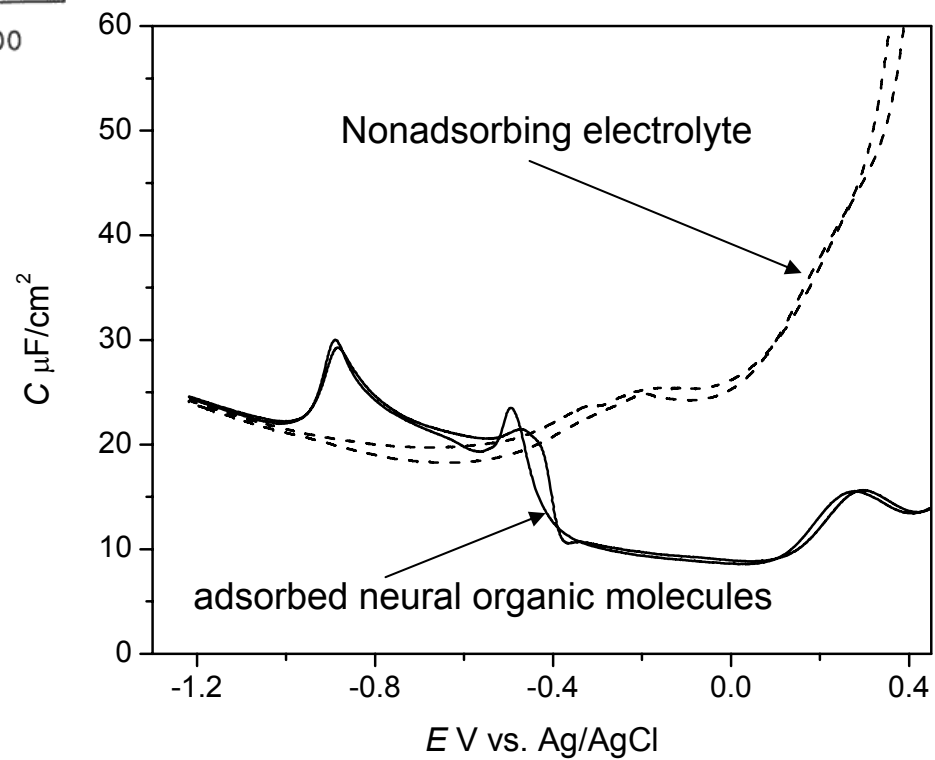
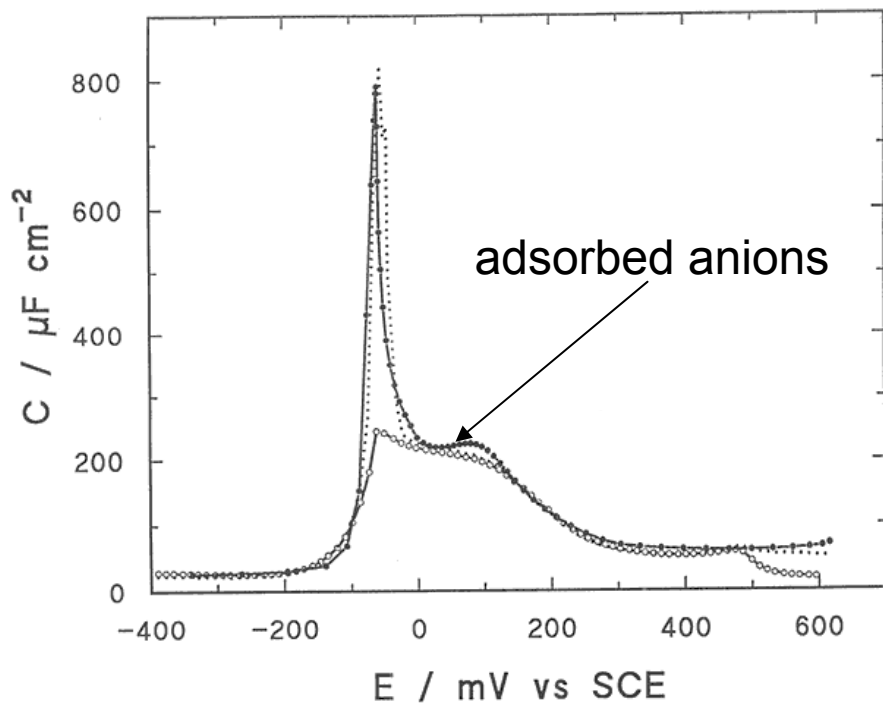
$$\sigma_M = -(\sigma_i + \sigma_d)$$

interface – two capacitors in series

$$\frac{1}{C} = \frac{1}{C_i} + \frac{1}{C_d}$$

OHP- outer Helmholtz plane; distance of the closest approach of solvated ions
 IHP – inner Helmholtz plane; plane in which specifically adsorbed ions are located
 Diffuse layer – layer within which ionic cloud screening the charge on the metal is located

Capacity of an Au electrode




Capacity of an electrode changes with potential – the changes reflect changes in the Coverage by specifically adsorbed ions or molecules

$$\sigma_M = f(E, \Gamma)$$

$$d\sigma_M = \left(\frac{\partial \sigma_M}{\partial E} \right)_{\Gamma} dE + \left(\frac{\partial \sigma_M}{\partial \Gamma} \right)_{E} d\Gamma$$

$$C = \frac{d\sigma_M}{dE} = \left(\frac{\partial \sigma_M}{\partial E} \right)_{\Gamma} + \left(\frac{\partial \sigma_M}{\partial \Gamma} \right)_{E} \frac{d\Gamma}{dE}$$

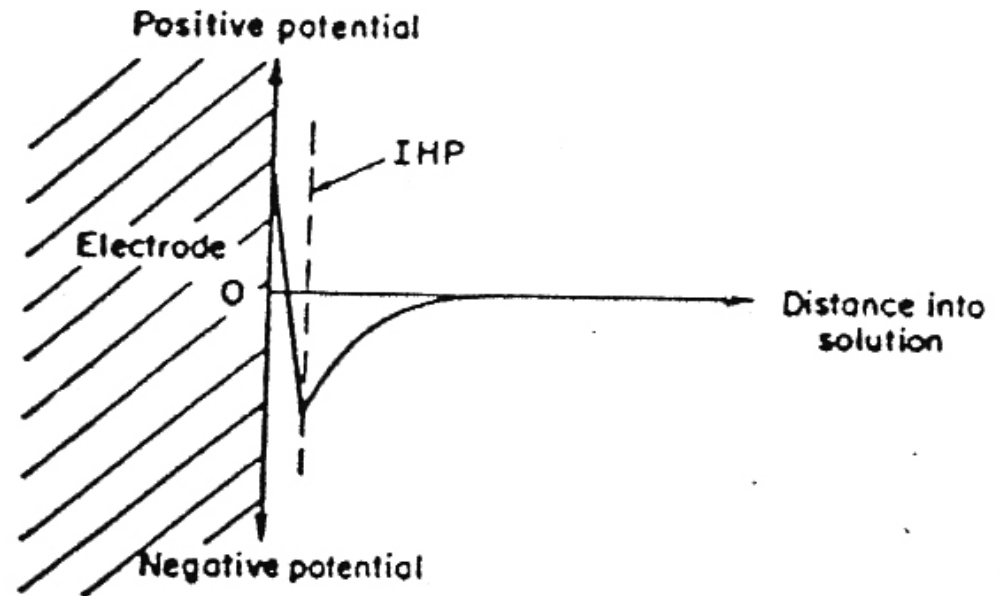
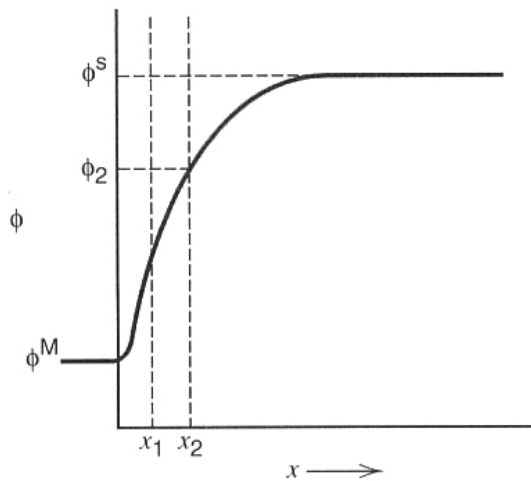
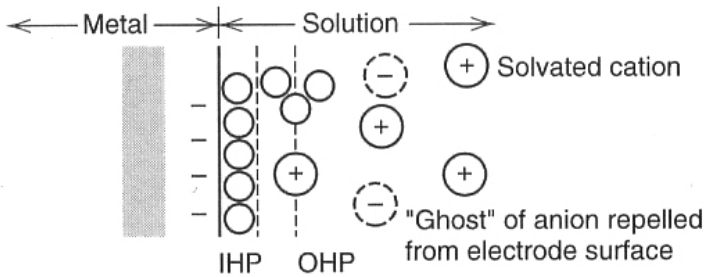

true capacity


pseudo capacity

Potential drop across the metal solution interface

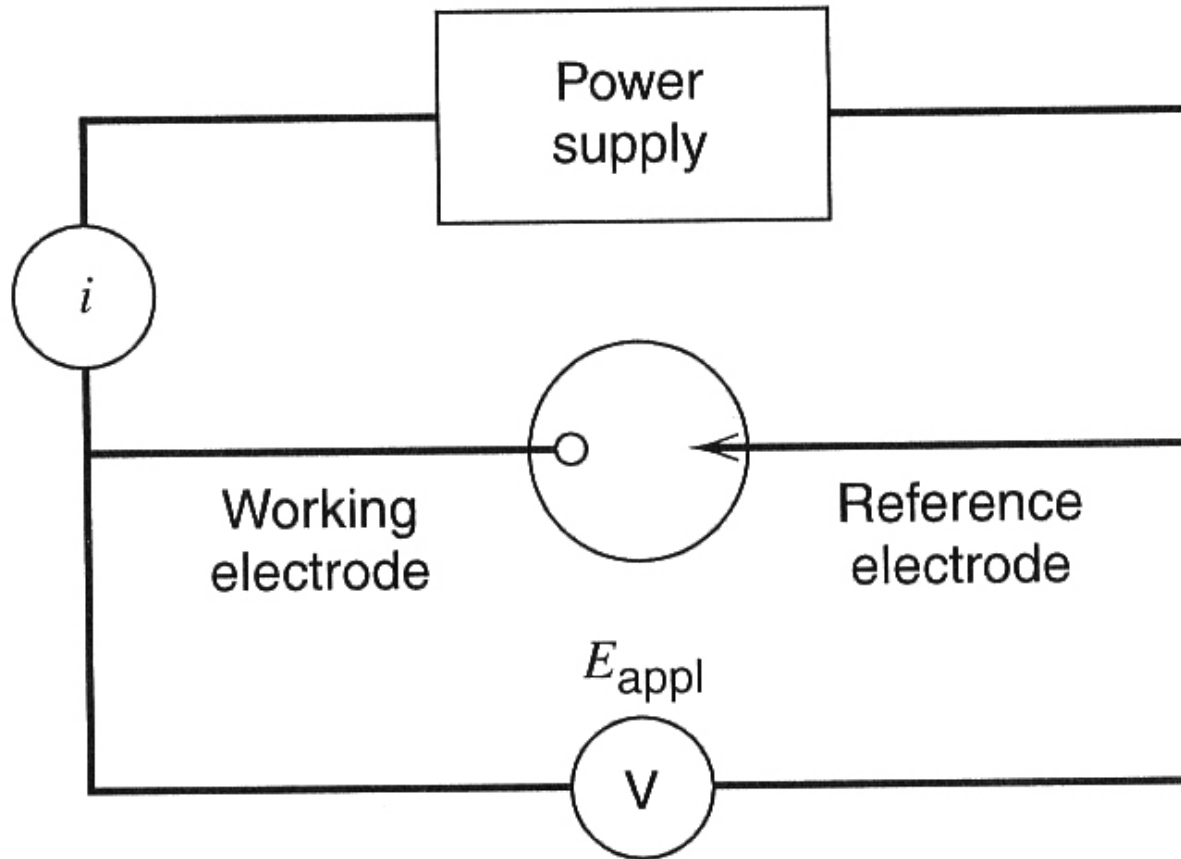
no specific adsorption

specific adsorption of anions



3.2 Electrochemical cell in the presence of a current flowing through the cell

Two electrode cell

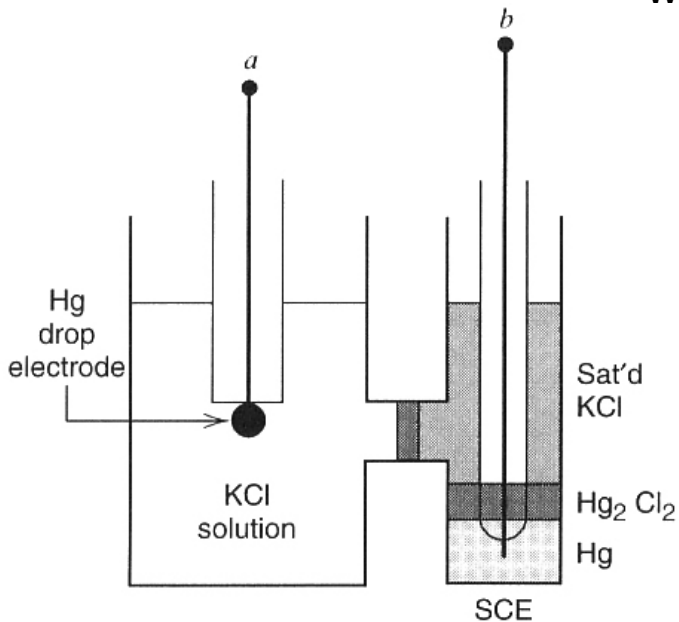


when potential E is applied from an external source
current flows through the cell

From Ohm's Law:

$$i = \frac{E}{Z}$$

$$Z = Z_i + Z_e + Z_{Ref} + Z_{ext}$$



Z_i – impedance of the indicator electrode

Z_e – impedance of the electrolyte

Z_{Ref} – impedance of the reference electrode

Z_{ext} – impedance of the external circuits

In an electrochemical experiment Z_e , Z_{Ref} , Z_{ext} must be eliminated

a. Elimination of Z_{Ref}

$$Z = f(R, C)$$

$$Z_{Ref} = R = \rho \frac{l}{A}$$

ρ - specific resistivity;

l - length;

A - area

$$Z_C = \frac{1}{\omega C}$$

C - capacity

$\omega = 2\pi\nu$ -angular frequency

$$C \propto A \quad \text{hence} \quad Z \propto A^{-1}$$

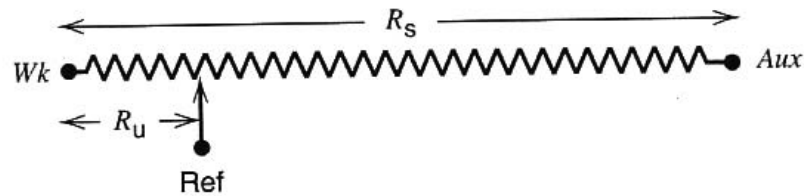
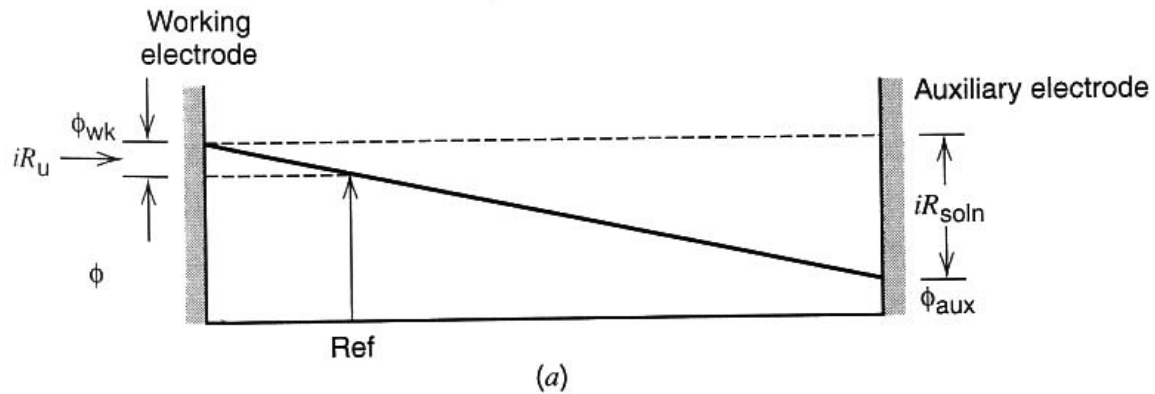
Consequently if : $A_i \ll A_{Ref}$ then $Z_i \gg Z_{Ref}$

The surface area of an indicator electrode should be much smaller than the surface area of the reference or auxiliary electrodes

b) Elimination of Z_e

$$Z_e = R_e$$

Use 3-electrode system and Luggin capillary



Luggin capillary and uncompensated resistance R_u

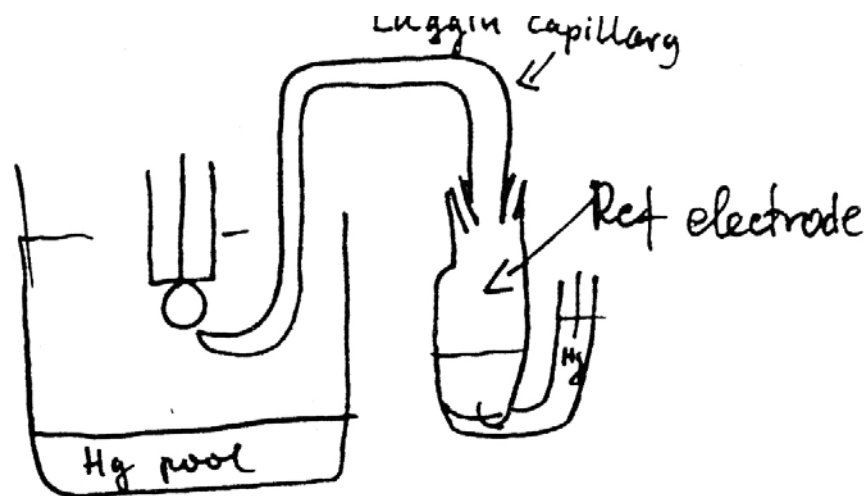
For a planar electrode :

$$R_u = \rho \frac{x}{A}$$

For a spherical electrode:

$$R_u = \rho \frac{1}{4\pi r_0} \left(\frac{x}{r_0 + x} \right)$$

r_0 - radius of the spherical electrode; x - distance from the electrode surface



Change of potential across the capacitor as a function of time

$$E = iR + \frac{q}{C_d}$$

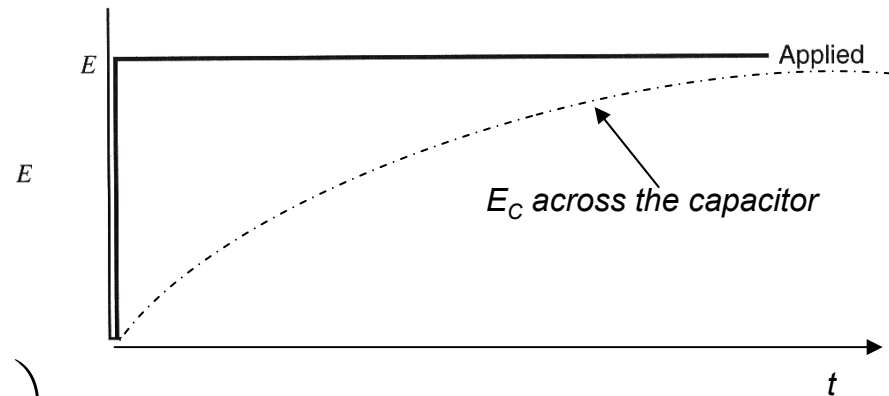
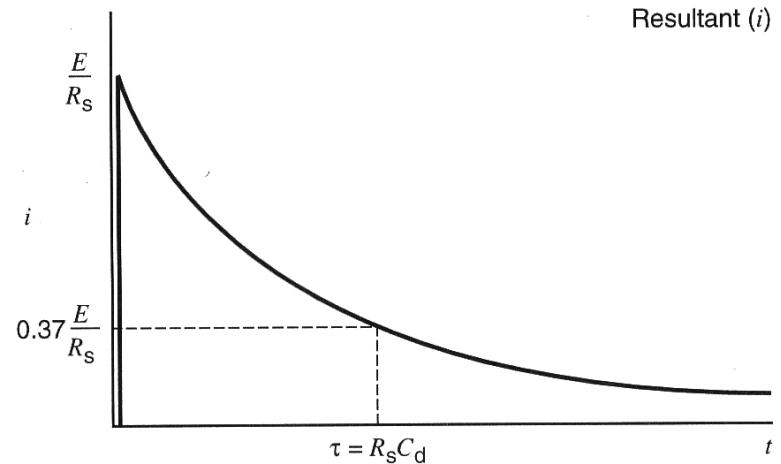
$$E_c = \frac{q}{C_d} = \frac{\int_0^t i dt}{C_d}$$

since:

$$i = \frac{E}{R_s} e^{-\frac{t}{R_s C_d}}$$

one obtains:

$$E_c = \frac{E}{R_s C_d} \int_0^t e^{-\frac{t}{R_s C_d}} dt = E \left(1 - e^{-\frac{t}{R_s C_d}} \right)$$



Linear potential sweep or voltage ramp

$$E = vt$$

where v is the sweep rate in $V s^{-1}$

$$E = iR + \frac{q}{C_d}$$

or

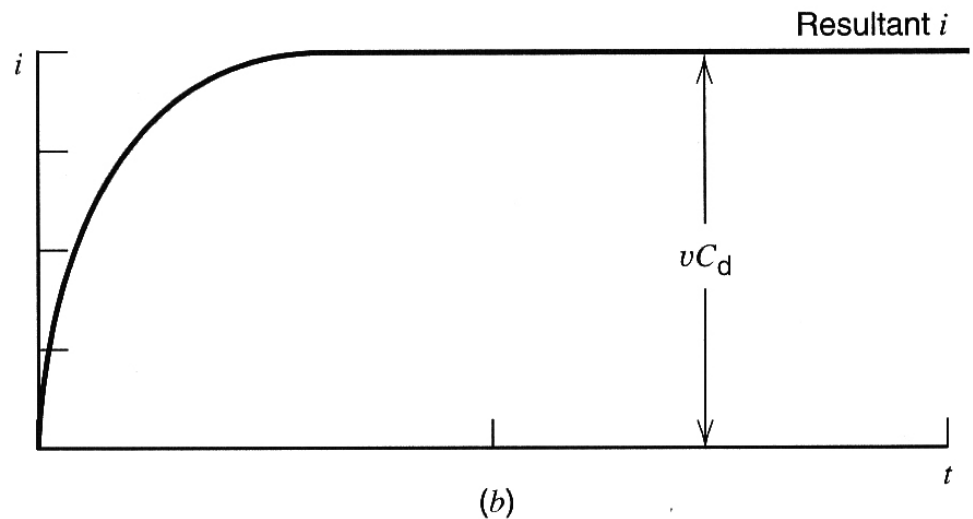
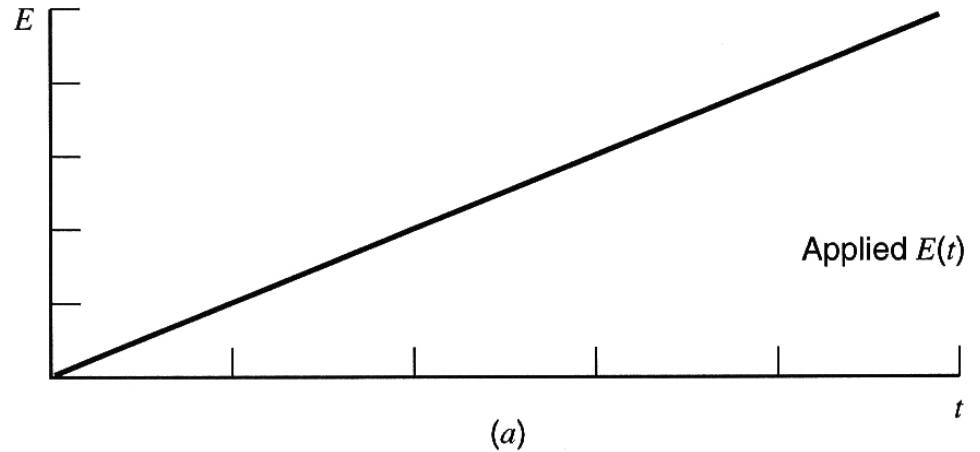
$$vt = R_s \frac{dq}{dt} + \frac{q}{C_d}$$

if $q=0$ at $t=0$

$$i = vC_d \left(1 - e^{-\frac{t}{R_s C_d}} \right)$$

if $t \gg R_s C_d$

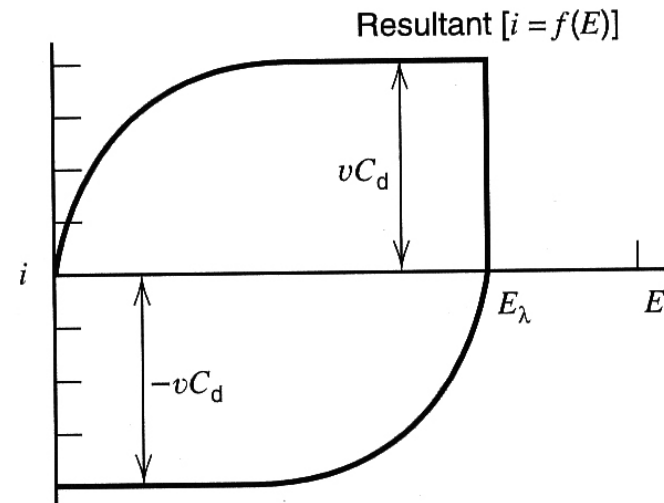
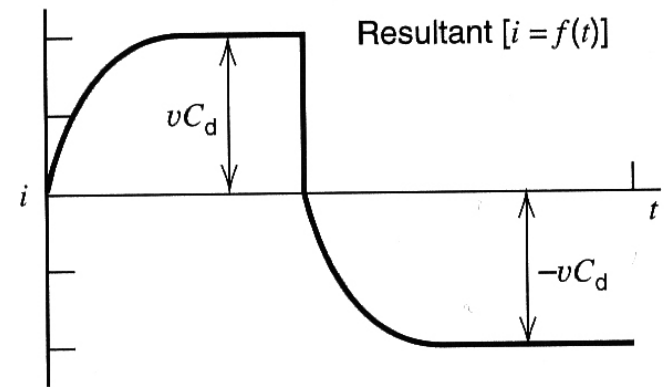
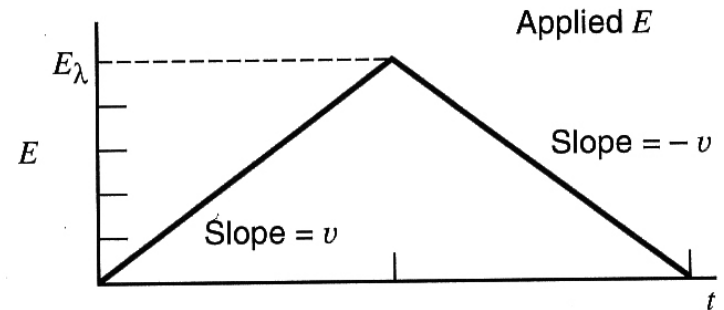
$$i = vC_d$$



Cyclic-linear potential sweep

$$E = vt$$

$$i = vC_d \left(1 - e^{-\frac{t}{R_s C_d}} \right)$$



4.1 Electrode reaction as a series of multiple consecutive steps

A charge transfer reaction provides an additional channel for current to flow through the interface. The amount of electricity that flows through this channel depends on the amount of species being oxidized or reduced according to the Faraday law:

$$m = \frac{M_A}{nF} it$$

Faraday law links electrical quantity such as current to the chemical quantity such as concentration or mass of the analyte:

$$m = CVM_A$$

This expression may be rearranged to give expression for current:

$$i = nF \frac{m}{M_A t} = nF \frac{N}{t}$$

n - number of electrons in a redox reaction, N -number of moles,
 M_A - molecular weight, F - Faraday constant, C -concentration, V -volume

Currents which are described by the Faraday law are called faradaic currents

$$i = nF \frac{m}{M_A t} = nF \frac{N}{t}$$

This equation describes average current flowing through the electrode during time – t. During infinitesimal period dt the number of electrolyzed moles is dN and the expression for the instantaneous current is:

$$i = nF dN / dt$$

The rate of a chemical reaction is :

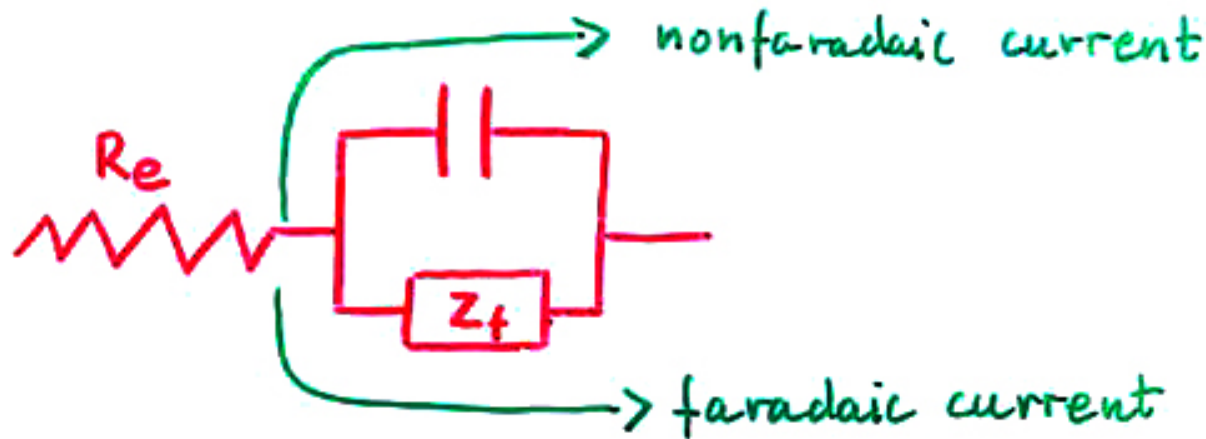
$$v = dN / dt$$

Hence faradaic current is a measure of a reaction rate

$$i = nF \frac{dN}{dt} = nFv$$

Current flowing in the absence of a redox reaction – nonfaradaic current

In the presence of a redox reaction – faradaic impedance is connected in parallel to the double layer capacitance. The scheme of the cell is:



The overall current flowing through the cell is :

$$i = i_f + i_{nf}$$

Only the faradaic current $-i_f$ contains analytical or kinetic information 98

Non-faradaic (capacitive) current constitutes a limitation to the detection limit of electrometric techniques

Experimental conditions for electroanalytical measurements:

1. $i_f \gg i_{non}$ (large concentration of electroactive species, long times of experiment)

2. $i_f = i - i_{non}$ (correction for non-faradaic current)

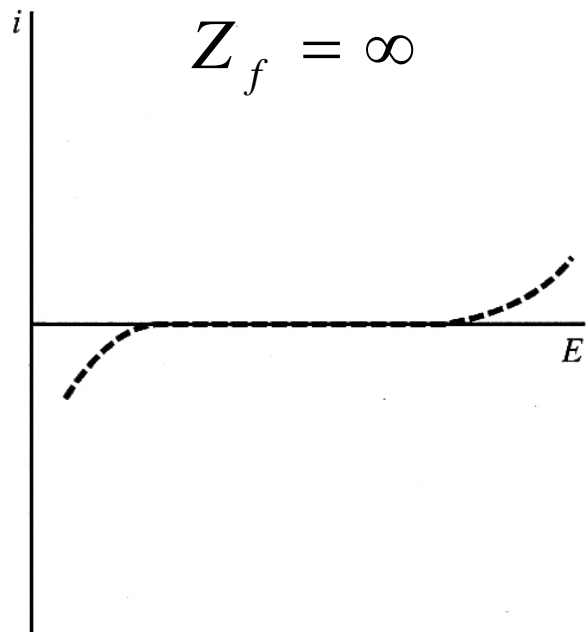
i_f and i_{non} are different functions of time

Under a steady state condition:

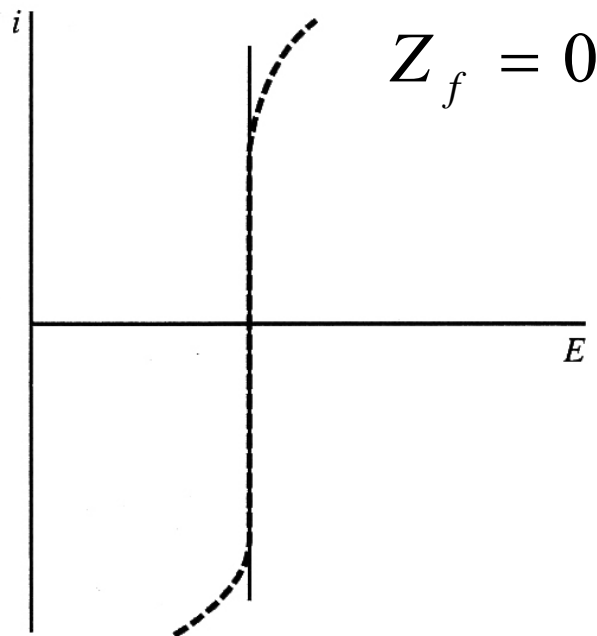
$$i_f \neq 0 \quad \text{but} \quad i_{non} = 0$$

Current – voltage characteristics of an ideal polarizable and ideal non-polarizable electrode

$$i = \frac{E}{Z}$$



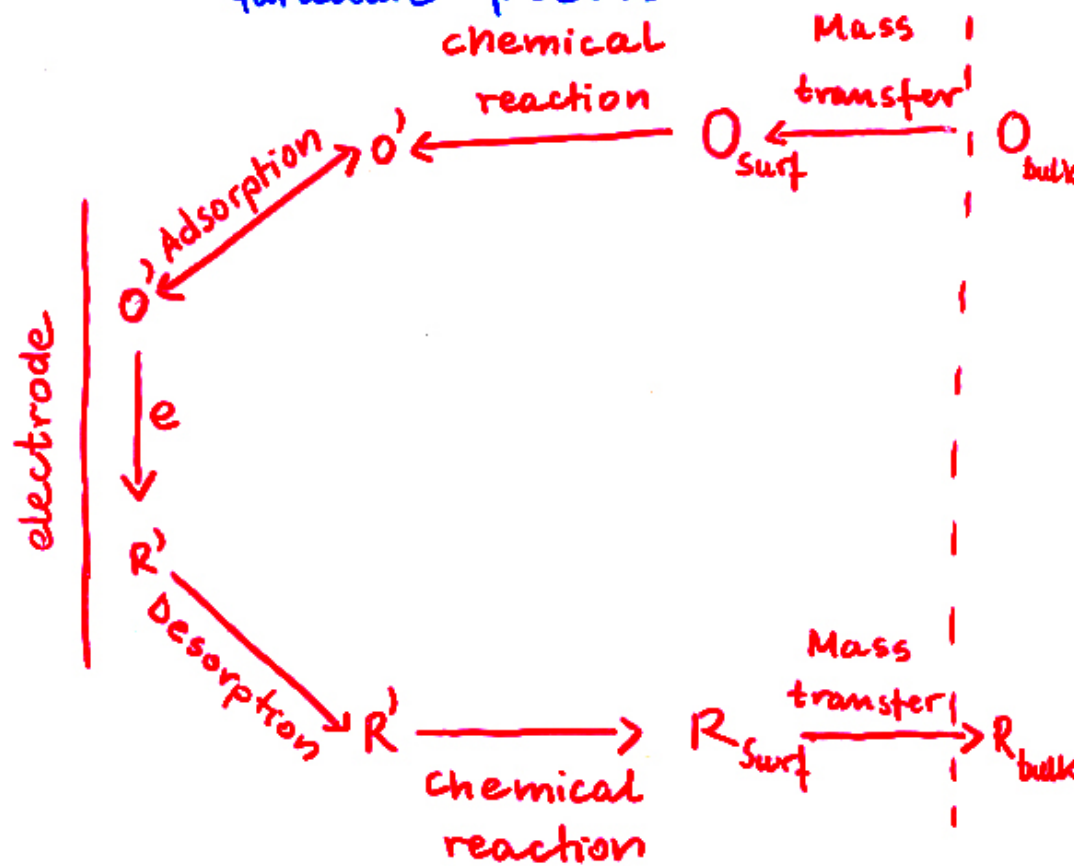
(a) Ideal polarizable electrode



(b) Ideal nonpolarizable electrode

Current-potential curves for ideal (a) polarizable and (b) nonpolarizable electrodes. Dashed lines show behavior of actual electrodes that approach the ideal behavior over limited ranges of current or potential.

General Scheme of a faradaic process



Electrode reaction - multistep reaction

Mechanism of el reaction - consecutive multistep mechanism

$$\frac{1}{v} = \sum_i \frac{1}{v_i}$$

For a multistep reaction

$$\frac{1}{v} = \sum \frac{1}{v_i} \quad \frac{1}{i} = \sum \frac{1}{i_i}$$

The current flowing through the cell is limited by the current corresponding to the slowest reaction step

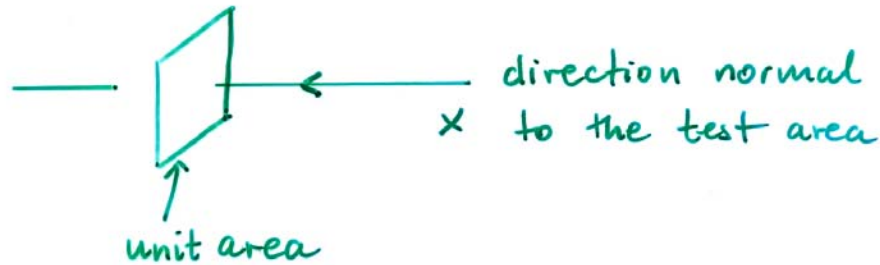
Types of faradaic currents

- 1) Charge transfer currents
- 2) adsorption currents
- 3) kinetic currents
- 4) mass transfer currents
 - a) diffusion currents
 - b) migration currents
 - c) convection currents

5. Currents controlled by mass transfer

5.1. General introduction

J_i - flux of species i is the number of moles of i which pass through a unit area in a unit of time



Species i can be transported across the tested area if:

- 1) there is a gradient of electrochemical potential
- 2) the solution moves in the direction normal to the surface

Hence the flux is given by:

$$J_i = -\left(\frac{C_i D_i}{RT}\right) \frac{\partial \bar{\mu}_i}{\partial x} + C_i v \quad / \text{mol s}^{-1} \text{cm}^{-2}$$

where v - is the solution velocity in the direction normal to the surface

$$\frac{\partial \bar{\mu}_i}{\partial x} = \frac{\partial \mu_i}{\partial x} + z_i F \frac{\partial \phi}{\partial x} = \frac{RT}{c_i} \frac{\partial c_i}{\partial x} + z_i F \frac{\partial \phi}{\partial x}$$

$$|z_i| F D_i / RT = u_i / (\text{m/s}) / (\text{V/m})$$

u_i - electrical mobility

$$J_i = -D_i \frac{\partial c_i}{\partial x} - u_i c_i \frac{\partial \phi}{\partial x} + c_i v$$

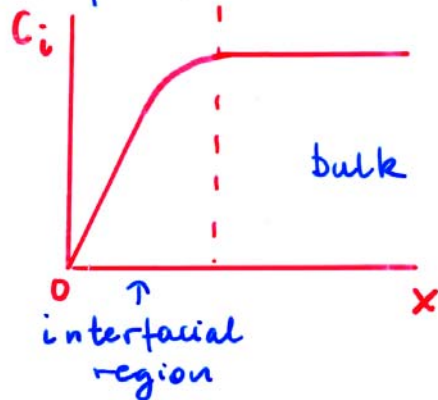
↑
↑
↑
 diffusion migration convection

$$i_i = -n F A J_i$$

n - number of electrons per one mol of i

5.2. migration currents

assumption - convection negligible



in the interfacial region for i -electro-
active

$$i = nFA D \frac{\partial C_i}{\partial x} + nFA u_i C_i \frac{\partial \phi}{\partial x} = i_d + i_m$$

in the bulk $\frac{\partial C_i}{\partial x} = 0$ current depends
on migration of all the ions

$$i = \sum_j z_j F A u_j C_j \frac{d\phi}{dx}$$

$$\frac{i_m}{i} = \frac{nFA u_i C_i \frac{d\phi}{dx}}{\sum_j z_j F A u_j C_j \frac{d\phi}{dx}} = \frac{n}{z_i} t_i$$

$$t_i = \frac{z_i u_i C_i}{\sum_j z_j u_j C_j}$$

$$i_d = i - i_m = i \left(1 - \frac{n}{z_i} t_i \right)$$

to minimize i_m - use an excess of
a supporting electrolyte.

5.3. Diffusion currents

a) Fick's first law of diffusion

In the absence of migration and convection the flux of species i at a location x and a given time t is equal to:

$$J_i = -D_i \frac{\partial C_i(x,t)}{\partial x}$$

If diffusion take place to an electrode, the electrode is placed at the distance $x=0$. Hence the current controlled by diffusion is equal to:

$$i = -nFAJ_i = nFAD_i \left(\frac{\partial C_i(x,t)}{\partial x} \right)_{x=0}$$

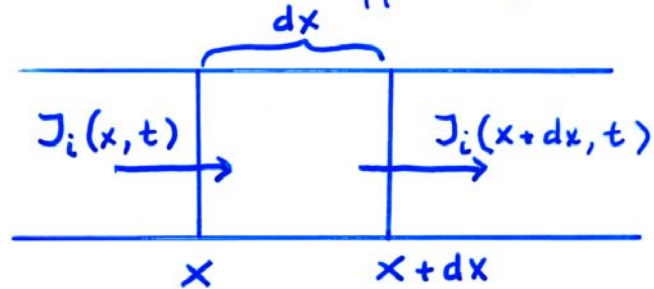
To find exact value of $\left(\frac{\partial C_i(x,t)}{\partial x} \right)_{x=0}$

exact dependence of C_i on x and t has to be known.

b) Fick's second law of diffusion

If species i diffuses in solution its concentration at location x varies with time. The variation of C_i with time depends on the geometry of diffusing space.

b.1. Linear diffusion



$$\frac{\partial C_i(x, t)}{\partial t} = \frac{J_i(x, t) - J_i(x+dx, t)}{dx}$$

$$J_i(x+dx, t) = J_i(x, t) + \frac{\partial J_i(x, t)}{\partial x} dx$$

$$\frac{\partial C_i(x, t)}{\partial t} = - \frac{\partial J_i(x, t)}{\partial x}$$

$$J_i = -D_i \frac{\partial C_i(x, t)}{\partial x}$$

$$\boxed{\frac{\partial C_i(x, t)}{\partial t} = D_i \frac{\partial^2 C_i(x, t)}{\partial x^2}}$$

5.4. Linear diffusion to a planar electrode - exact solution

What we want to find?

$$i = nFA D_i \left(\frac{\partial C_i(x,t)}{\partial x} \right)_{x=0}$$

This is to be found

What we have to solve?

$$\frac{\partial C_i(x,t)}{\partial t} = D_i \frac{\partial^2 C_i(x,t)}{\partial x^2}$$

This is a partial differential equation
Solution of this equation involves three integrations. Hence, we need three extra relationships to determine the three integration constants. This is provided by one initial and two boundary conditions.

initial condition

$$\text{at } t=0 \quad C_i(x,t) = C^*$$

boundary conditions

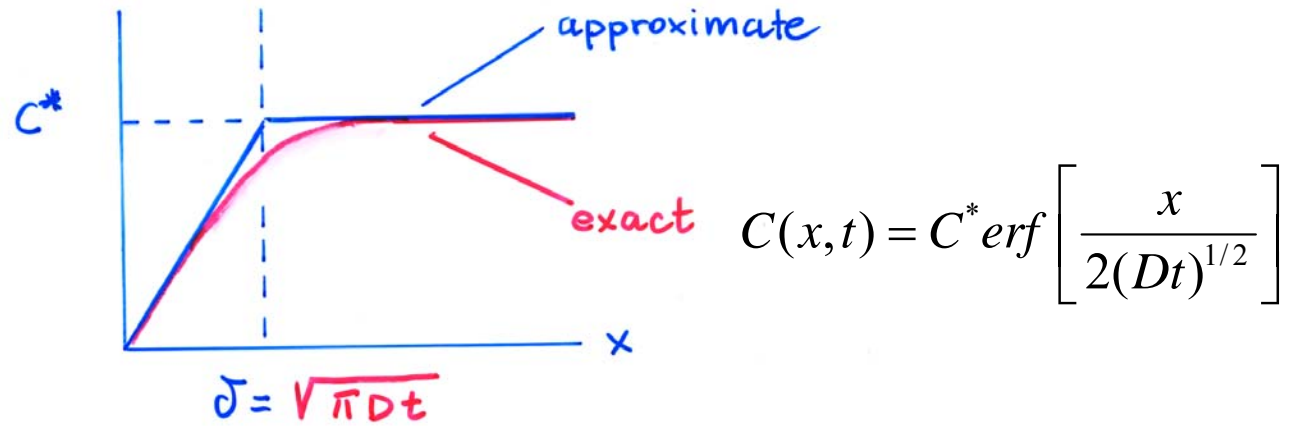
1. $\lim_{x \rightarrow \infty} C_i(x,t) = C^*$

2. at $t > 0 \quad C_i(0,t) = 0$ (limiting current)

$$i = nFA D_i \frac{C_i^*}{\sqrt{\pi D t}}$$

Cottrell Equation

5.5. Comparison of the approximate and the exact solutions for the diffusion current flowing through a planar electrode



approximate

$$i = n F A D_i \frac{C_i^*}{\delta}$$

exact

$$i = n F A D_i \frac{C_i^*}{\sqrt{\pi D t}}$$

δ - thickness of the diffuse layer
 for $D \approx 5 \cdot 10^{-6} \text{ cm}^2 \text{ s}^{-1}$ and $t = 1 \text{ s}$
 $\delta = 4 \cdot 10^{-3} \text{ cm}$

5.7. Diffusion to a spherical electrode

Differential equation

$$\frac{\partial C_i(r,t)}{\partial t} = D_i \left\{ \frac{\partial^2 C_i(r,t)}{\partial r^2} + \frac{2}{r} \frac{\partial C_i(r,t)}{\partial r} \right\}$$

initial condition

$$C_i(r, 0) = C_i^* \quad (r > r_0)$$

r_0 - radius of the electrode

boundary condition

$$1. \quad \lim_{r \rightarrow \infty} C_i(r, t) = C_i^*$$

$$2. \quad C_i(r_0, t) = 0 \quad (t > 0)$$

(limiting current)

Solution

$$i(t) = nFA D_i C_i^* \left[\underbrace{\frac{1}{\sqrt{\pi D_i t}}}_{\text{Linear diffusion term}} + \underbrace{\frac{1}{r_0}}_{\text{Correction for sphericity}} \right]$$

5.8. Comparison of the expressions for diffusion currents to a planar and a spherical electrode

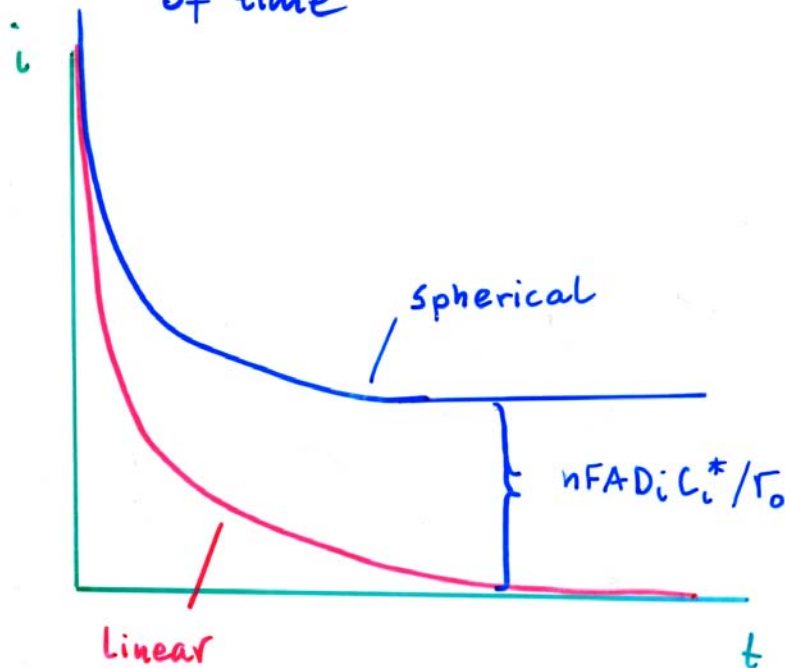
$$i(t) = nFAD_i C_i^* \left[\frac{1}{\sqrt{\pi D_i t}} + \frac{1}{r_0} \right]$$

$$\text{if } \sqrt{\pi D_i t} \ll r_0$$

$$i_{\text{sph}} = i_{\text{lin}}$$

$$\text{if } \sqrt{\pi D_i t} \gg r_0$$

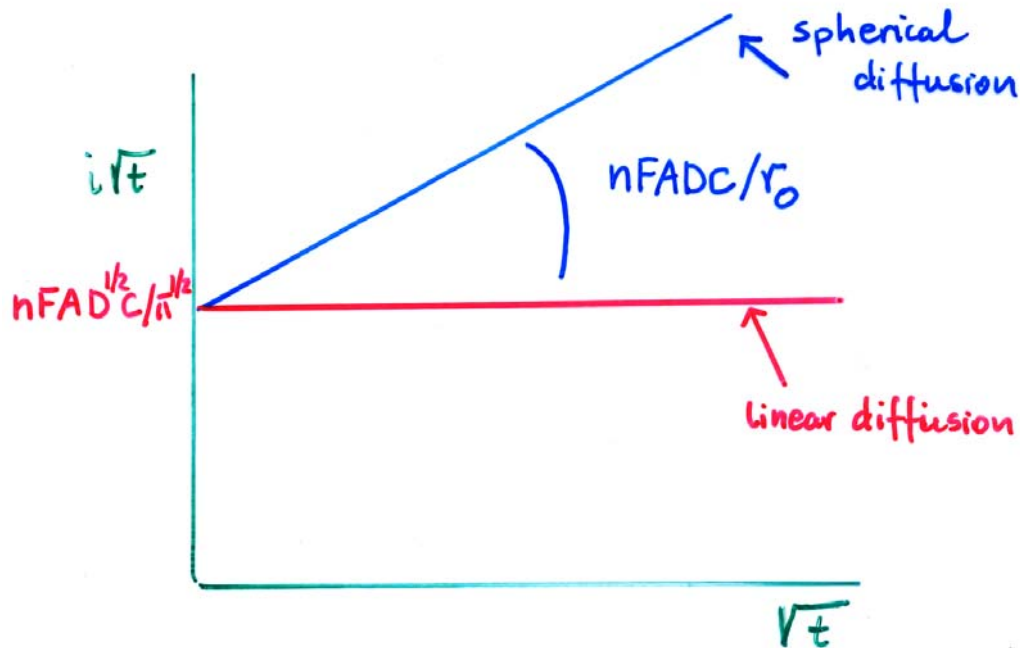
$i_{\text{sph}} = nFAD_i C_i^* / r_0$ - independent of time



Determination of diffusion coefficients

$$\bar{i} = nFADc^* \left(\frac{1}{\sqrt{\pi Dt}} + \frac{1}{r_0} \right)$$

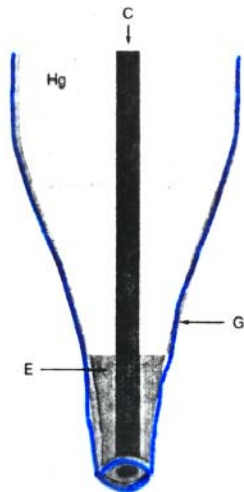
$$i\sqrt{t} = nFAD^{1/2}c^*/\pi^{1/2} + (nFADC^*/r_0)t^{1/2}$$



$$\frac{\text{slope}}{\text{intercept}} = \frac{D^{1/2}}{\pi^{1/2}r_0}$$

$$D = \left(\frac{\text{slope}}{\text{intercept}} \right)^2 \pi^{-1} r_0^2$$

ultramicroelectrodes



for $r = 10 \mu\text{m}$ $i = nFADC/r$ at $t > 50 \text{ms}$

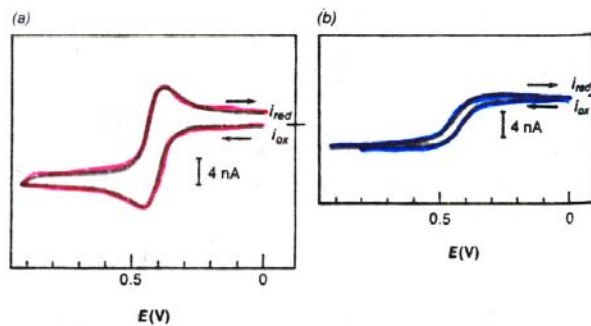
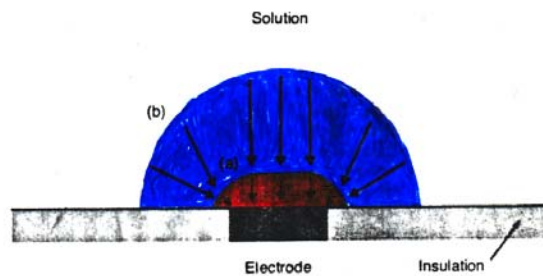


Figure 1. Cyclic voltammogram of ferrocene (1.0 mM) in acetonitrile with 0.1 M tetra-*n*-butylammonium perchlorate at a gold microdisk electrode ($r = 6.5 \mu\text{m}$). (a) 10 V s^{-1} scan rate. (b) 0.1 V s^{-1} scan rate



Examples of Instrumental Analysis

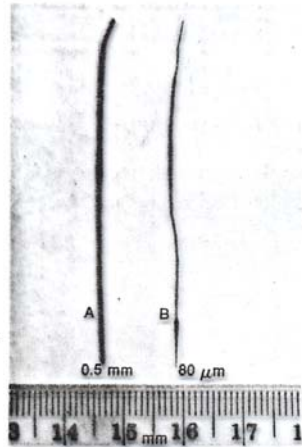


Figure 5. Micro graphite electrodes for in vivo brain voltammetry
 A: teflon-sleeved (ventricle type) electrode, ca. 0.5 mm exposed graphite paste surface; B: micro glass capillary filled with graphite-epoxy resin, tip diameter ca. 80 μm

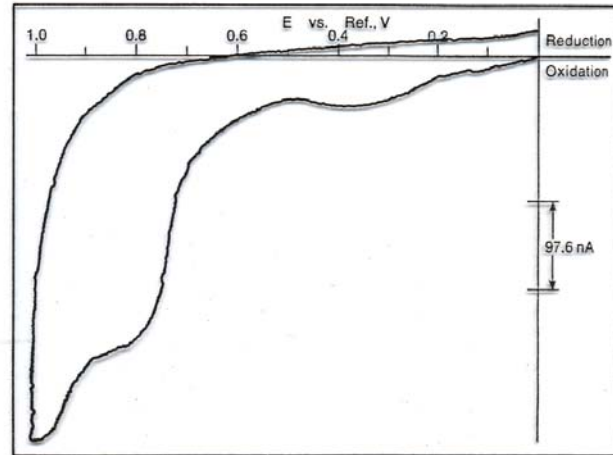


Figure 6. Typical tissue voltammograms in rat caudate nucleus

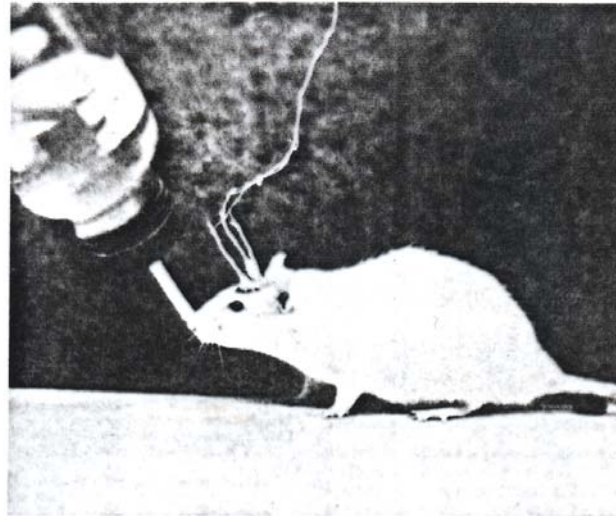


Figure 7. Unrestrained rat with chronically implanted voltammetric electrodes
 Implanted electrodes consist of micro graphite electrode of Figure 5B, miniature enclosed SCE, and platinum auxiliary. Shrinkable Teflon shields extend up to protect thin connecting leads from breakage. Entire electrode "package" is conventionally sealed to skull with dental acrylic. During typical water drinking period shown in photograph, a cyclic voltammogram and chronoamperometric ($i^{1/2}$) measurement were being recorded via minicomputer-controlled potentiostat

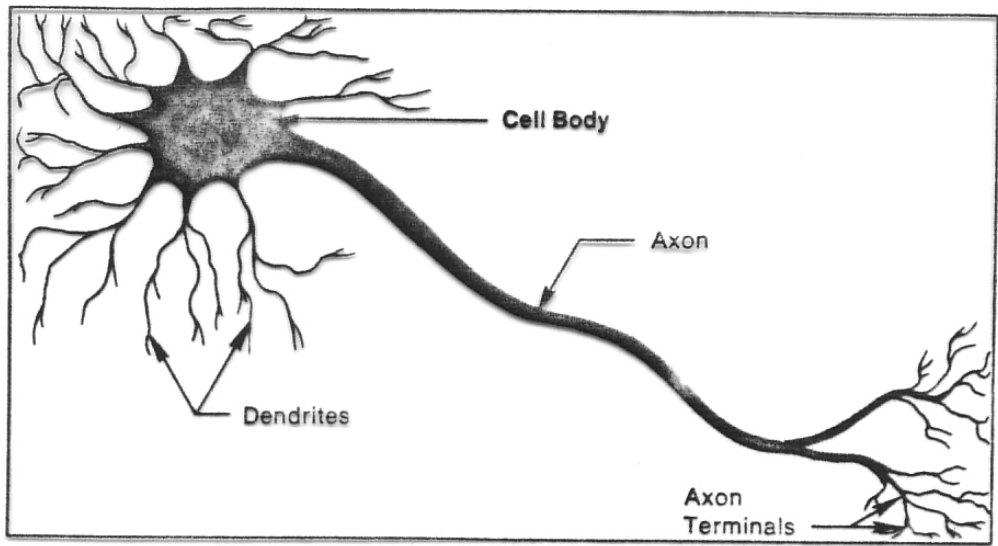
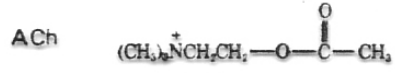


Figure 1. "Typical" neuron in mammalian brain

Table I. Chemical Neurotransmitter Systems

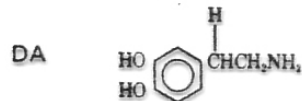
CHOLINERGIC

Acetylcholine

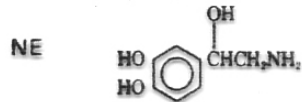


ADRENERGIC

Dopamine

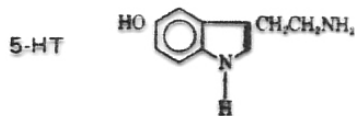


Norepinephrine



SEROTONINERGIC

5-Hydroxytryptamine
(Serotonin)

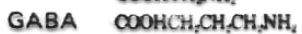


AMINO ACIDS

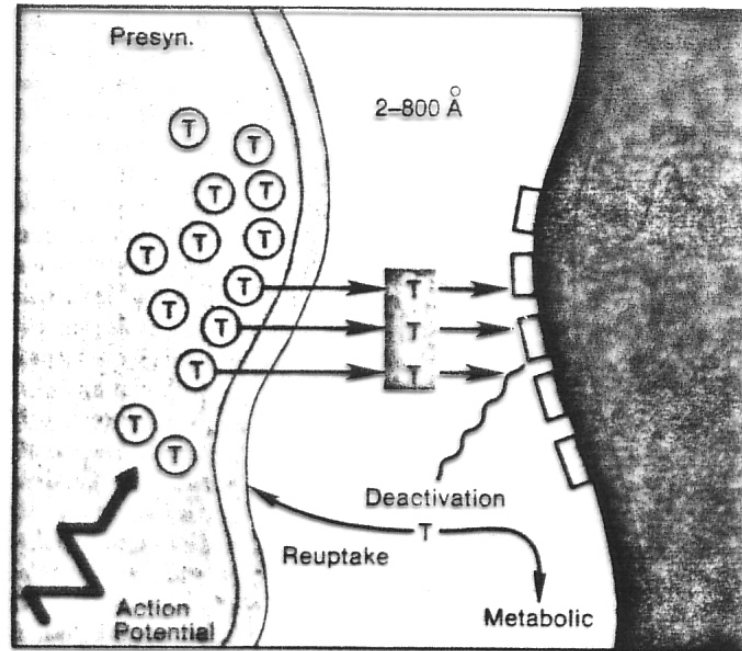
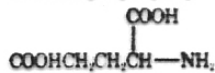
Glycine



γ -Aminobutyric acid



Glutamic acid



Review

Currents controlled by mass transport



$$i = nFAD \left(\frac{\partial C(x,t)}{\partial x} \right)_{x=0}$$

Cell a processor solving partial differential equations

$$\frac{\partial C(x,t)}{\partial t} = D \frac{\partial^2 C(x,t)}{\partial x^2} \quad \text{planar electrode}$$

$$\frac{\partial C(r,t)}{\partial t} = D \left\{ \frac{\partial^2 C(r,t)}{\partial r^2} + \frac{2}{r} \frac{\partial C(r,t)}{\partial r} \right\} \quad \text{spherical electrode}$$

1. Initial condition : $t=0$

$$C(x,0) = C^* \quad ; \quad C(r,0) = C^*$$

2. Boundary conditions

$$(i) \quad x=0 \quad \text{or} \quad r=r_0 \quad C(0,t) = 0$$

$$(ii) \quad x \rightarrow \infty \quad \text{or} \quad r \rightarrow \infty \quad C(\infty,t) = C^*$$

Solutions

$$i = nFA DC^* / \sqrt{\pi D t} \quad - \text{planar electrode}$$

$$i = nFA DC^* \left\{ \frac{1}{\sqrt{\pi D t}} + \frac{1}{r_0} \right\} \quad - \text{spherical electrode}$$

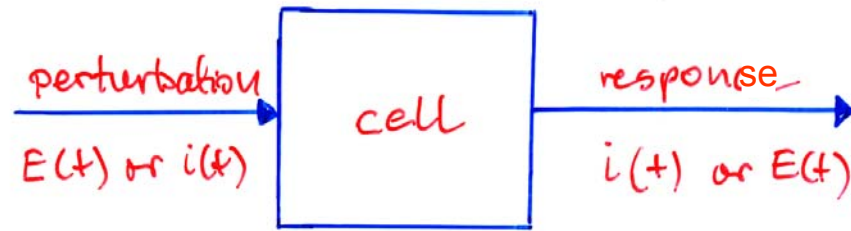
$$\text{if } \sqrt{\pi D t} \ll r_0$$

$$i_{\text{sph}} = i_{\text{plan}}$$

$$\text{if } \sqrt{\pi D t} \gg r_0$$

ultramicroelectrodes

6. Electroanalytical Techniques



1. Chronoamperometry
2. Polarography
3. Fast Polarography
4. Normal Pulse Polarography
5. Differential Pulse Polarography
6. Cyclic Voltammetry

Response Depends on:

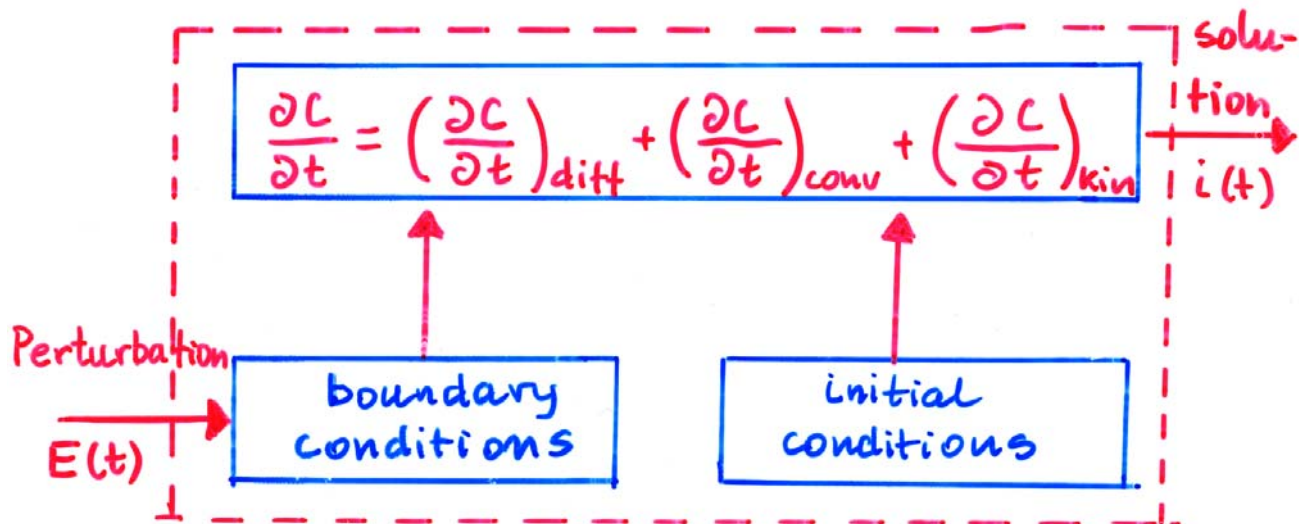
- (i) Perturbation
- (ii) Transport (diffusion or convection)
- (iii) Electrode Geometry
- (iv) Signal processing

6.1 Electroanalytical techniques based on electrolysis at the constant electrode potential

1. Introduction



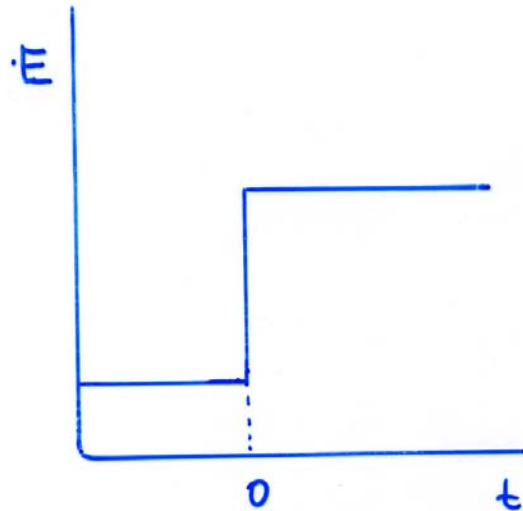
The cell can be visualized as a processor solving the partial differential equation for the boundary conditions set up by the type of electroanalytical technique used.



6.2. Chronoamperometry

1. perturbation

$$E = \text{const}$$



2. no convection

3. all type of electrode geometries possible but in analytical practice only planar and spherical electrodes are used

4. no signal processing

Potential-dependence of the

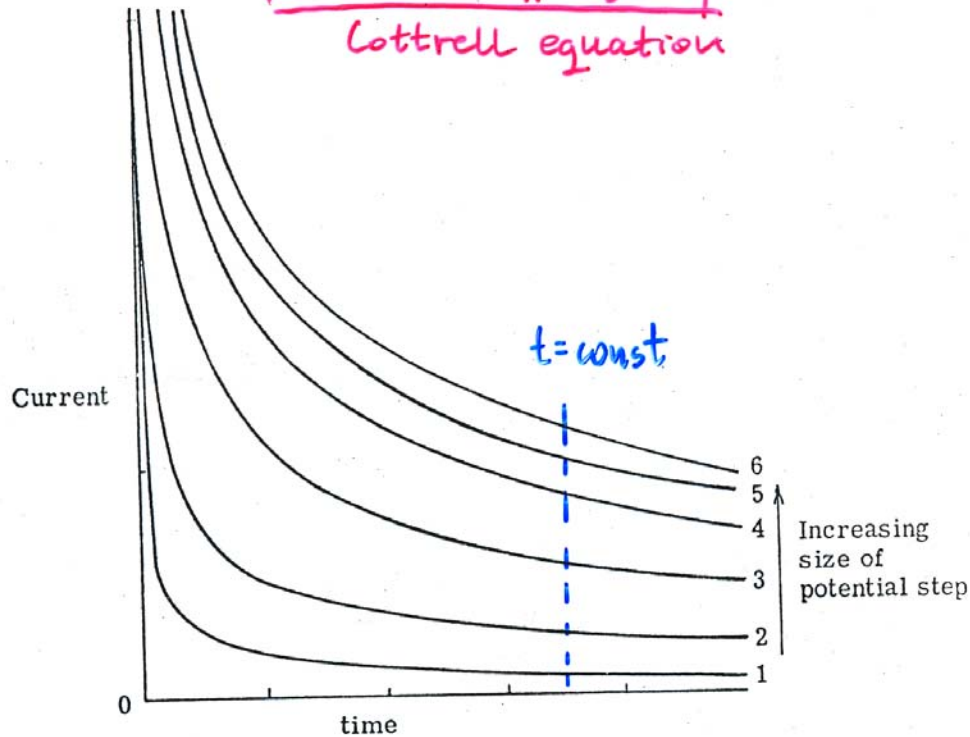
Chronoamperometric Response

Limiting current

$$C_i(0,t) = 0$$

$$i(t) = \frac{nFA D^{1/2} C_i^*}{\pi^{1/2} t^{1/2}}$$

Cottrell equation



at $C_i(0,t) \neq 0$

$$i(t) = nFA D^{1/2} \frac{C_i^* - C_i(0,t)}{\pi^{1/2} t^{1/2}}$$

diffusion control - reversible current

$$E = E_0 + \frac{RT}{nF} \ln \frac{C_{ox}(0,t)}{C_R(0,t)}$$

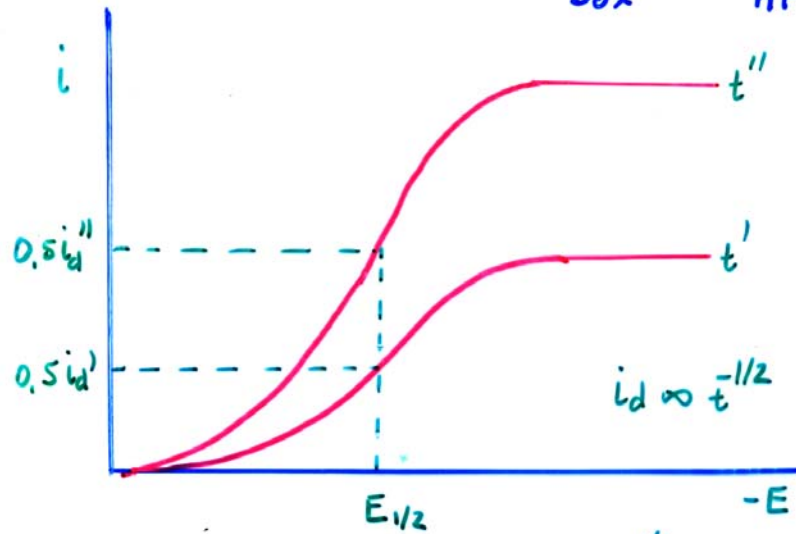
Reversible reactions

How $i(t)$ depends on E ?

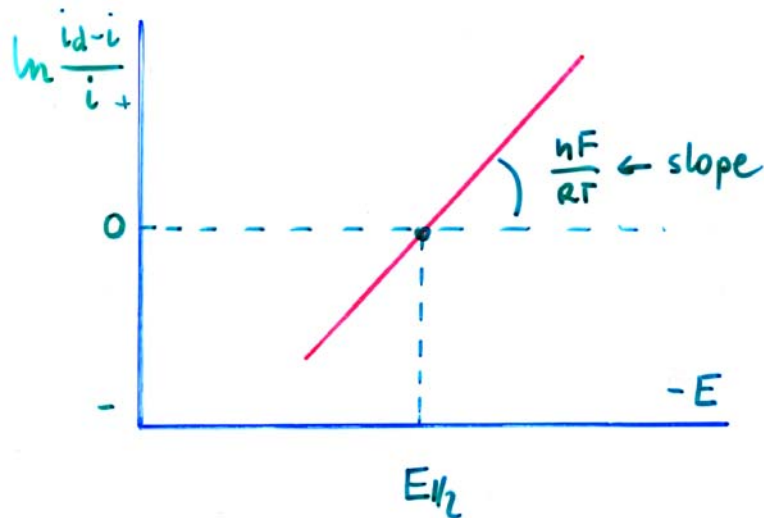
at $t = \text{const}$

$$E = E_0 + \frac{RT}{nF} \ln \left(\frac{D_{O_2}}{D_{O_1}} \right)^{1/2} + \frac{RT}{nF} \ln \frac{i_d - i}{i}$$

$$E = E_0 + \frac{RT}{nF} \ln \left(\frac{D_R}{D_{Ox}} \right)^{1/2} + \frac{RT}{nF} \ln \frac{i_d - i}{i}$$

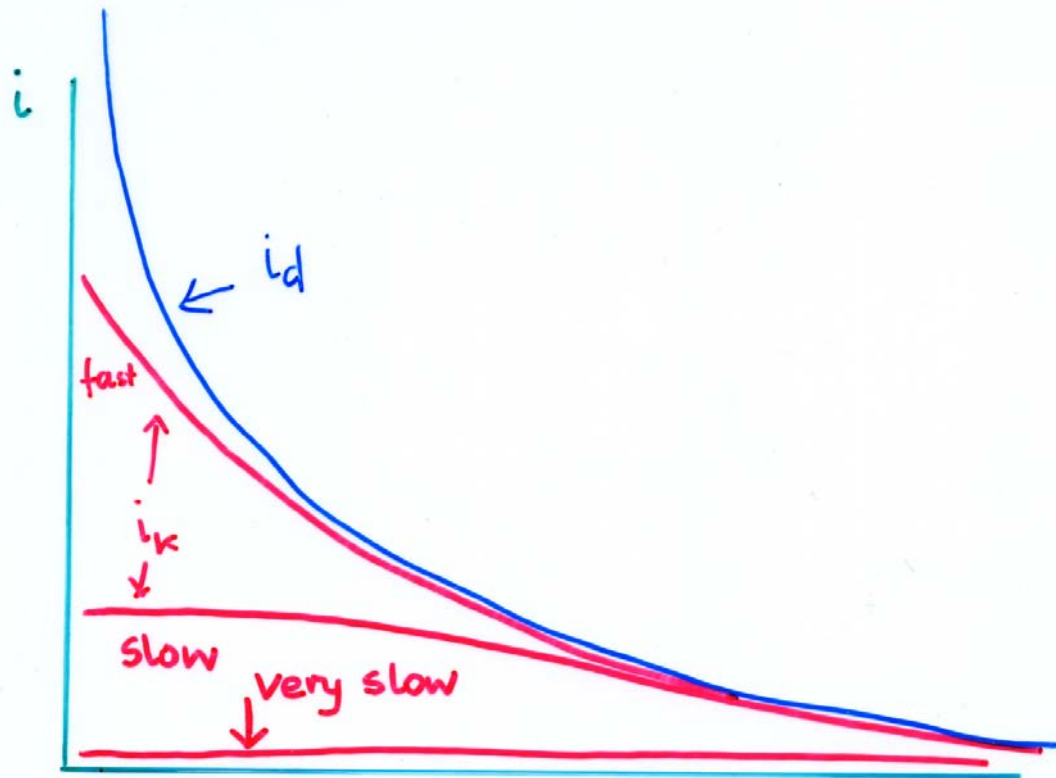


$$E_{1/2} = E^0 + \frac{RT}{nF} \ln \left(\frac{D_R}{D_{Ox}} \right)^{1/2}$$



6.3 chronoamperometry - current controlled by slow charge transfer kinetics (irreversible process)

a) experimental transients



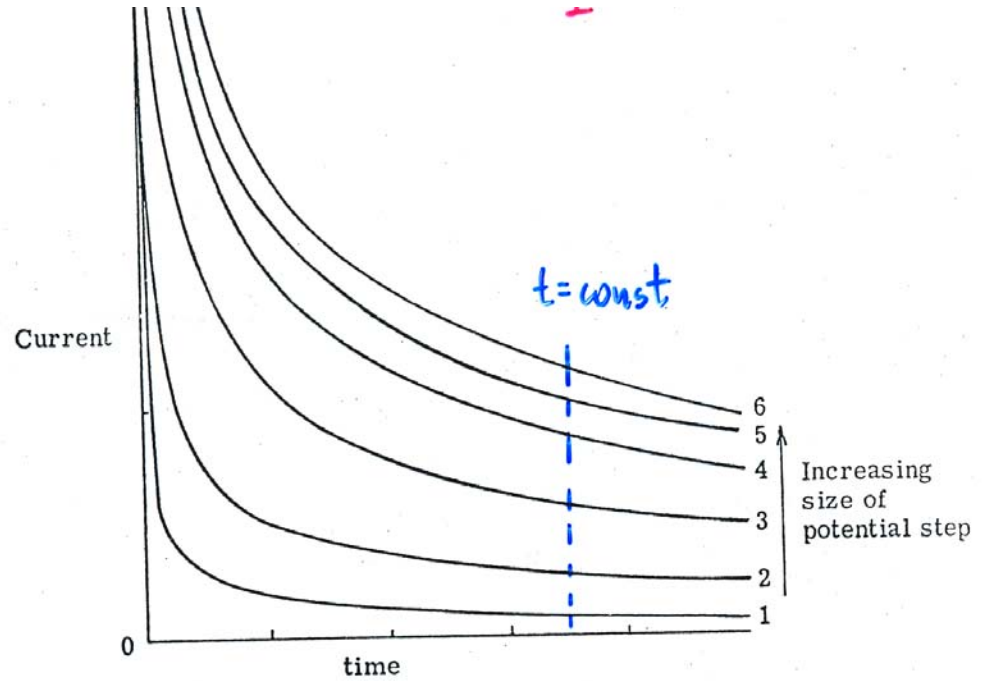
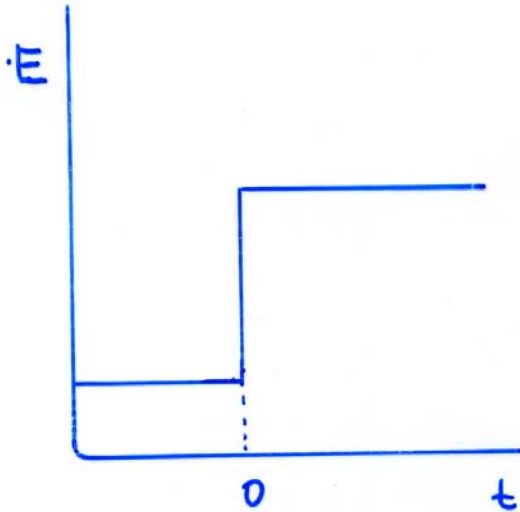
$$i_d = nFA D^{1/2} \frac{C_i^* - C_i(0,t)}{\pi^{1/2} t^{1/2}}$$

$$i_k = nFA k_{f,h} C_i(0,t)$$

Review

response

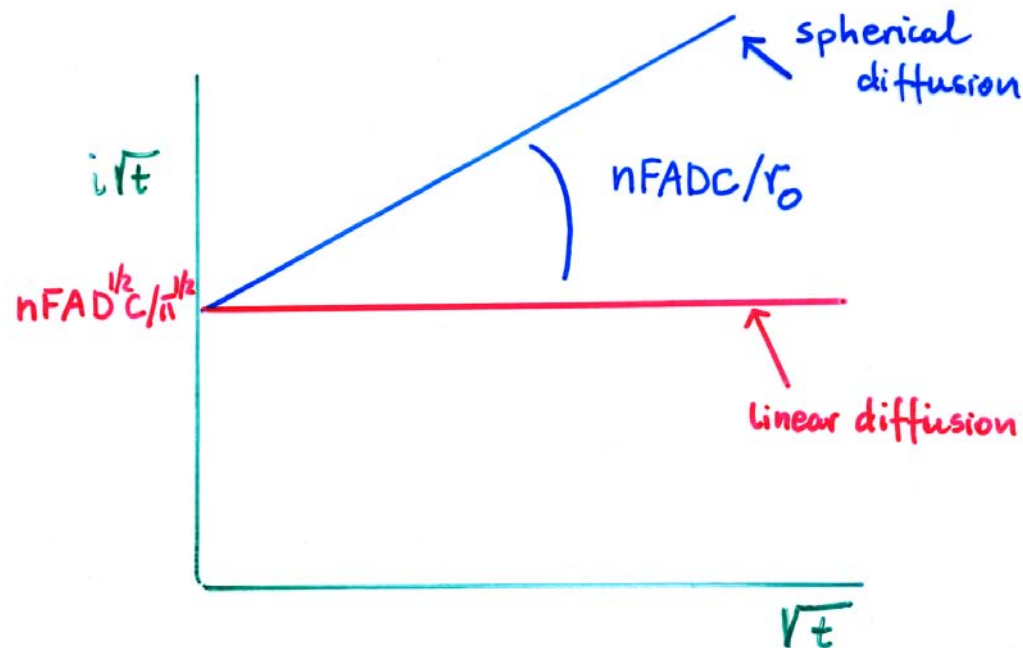
Chronoamperometry
perturbation $E = \text{const}$



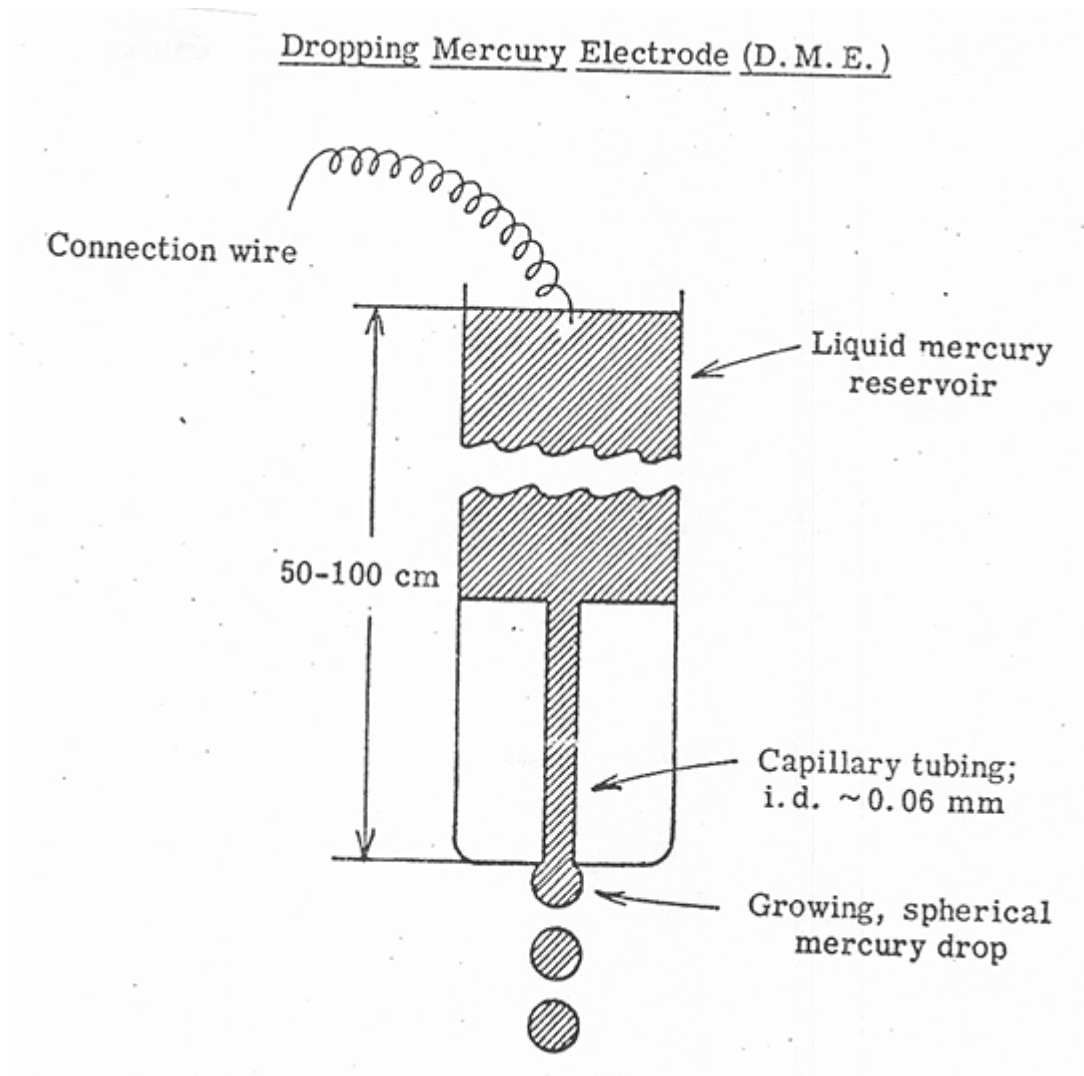
From limiting chronoamperometric curves – analytical information

$$\bar{i} = nFADc^* \left(\frac{1}{\sqrt{\pi Dt}} + \frac{1}{r_0} \right)$$

$$i\sqrt{t} = nFAD^{1/2}c^*/\pi^{1/2} + (nFADC^*/r_0)t^{1/2}$$

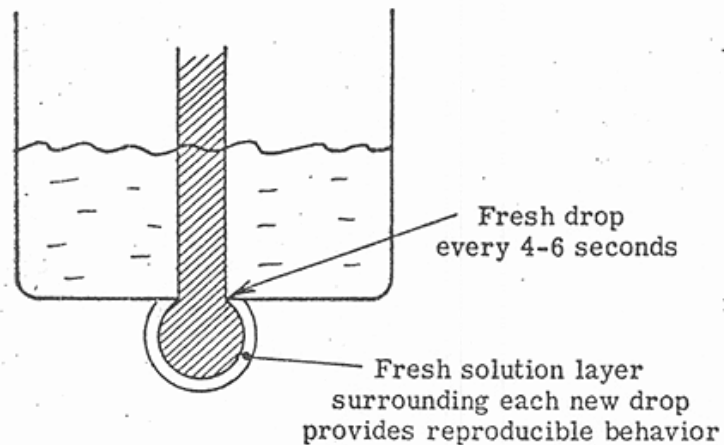


7.1 Polarography

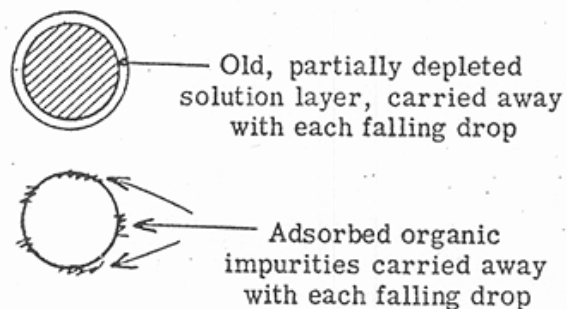


Virtues of the Dropping Mercury Electrode

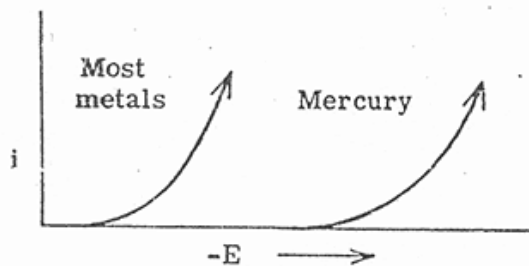
1. Reproducibility:



2. Self-cleansing:



3. High "hydrogen overvoltage": $\text{H}_2\text{O} + \text{e}^- \rightarrow \frac{1}{2}\text{H}_2 + \text{OH}^-$



polarography exact solution

1. perturbation $E = \text{const}$
2. diffusion and convection
3. spherical electrodes

Ilkovic equation - solution of the partial differential equation

$$\frac{\partial C_{Ox}(x,t)}{\partial t} = D_{Ox} \frac{\partial^2 C_{Ox}}{\partial x^2} + \frac{2x \partial C_{Ox}(x,t)}{3t \partial x}$$

$$i = \sqrt{\frac{7}{3}} \frac{nF D_{Ox}^{1/2} A C}{(\pi t)^{1/2}} = 708 n D^{1/2} C^b m^{2/3} t^{1/6}$$

Polarography:

1. Electrolysis at constant electrode potential at DME
2. Mass transport - convection + diffusion

$$i = \left(\frac{7}{3}\right)^{1/2} \underbrace{n F A D^{1/2} (C_b - C_{x=0}) / \sqrt{\pi t}}_{\substack{\uparrow \\ \text{diffusion} \\ \text{toward electrode}}}$$

\uparrow
correction for convection

$$A = 0.85 m^{2/3} t^{2/3}$$

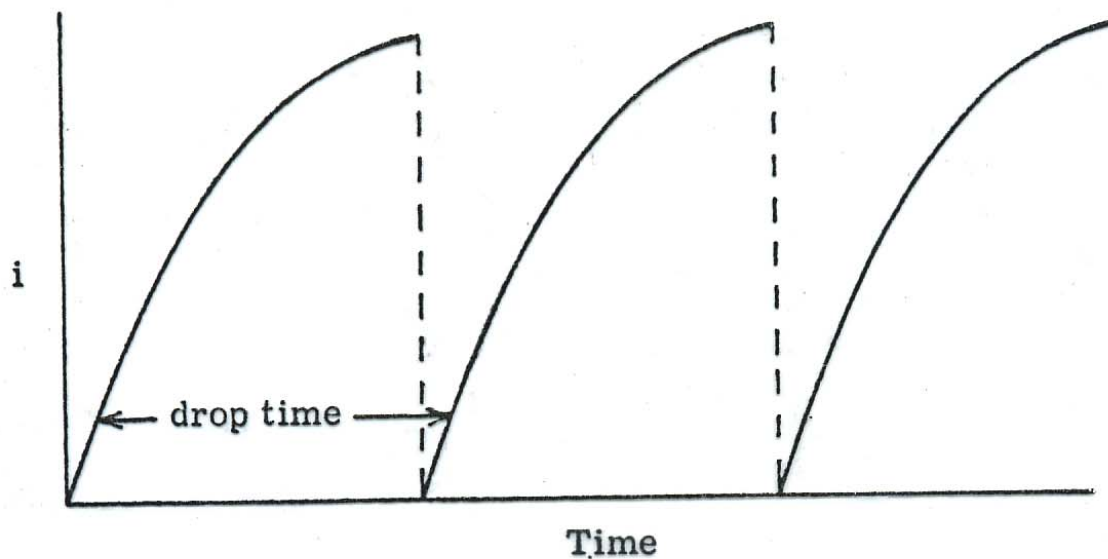
$$i = 708 n D^{1/2} m^{2/3} t^{1/6} (C_b - C_{x=0})$$

Limiting current

$$i = 708 n D^{1/2} m^{2/3} t^{1/6} C_b$$

Ilkovič equation

Instantaneous Current-time Curves for
a Dropping Mercury Electrode



The Ilkovič Equation:

$$i_d (\mu \text{ amp}) = 708 n D^{1/2} C^b m^{2/3} t^{1/6}$$

i_d = instantaneous current

m = mercury flow rate, milligrams/sec

t = drop age, sec

C^b = bulk concentration, millimolar

D = diffusion coefficient, $\text{cm}^2 \text{sec}^{-1}$

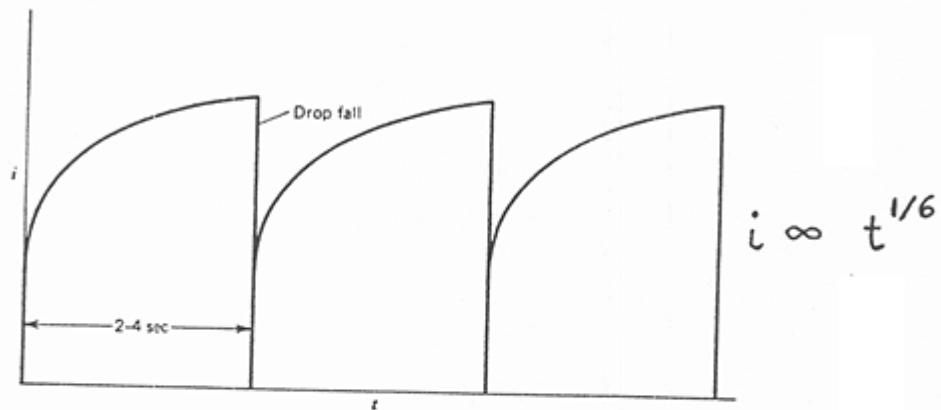


Figure 2
Current growth during three successive drops of a DME.

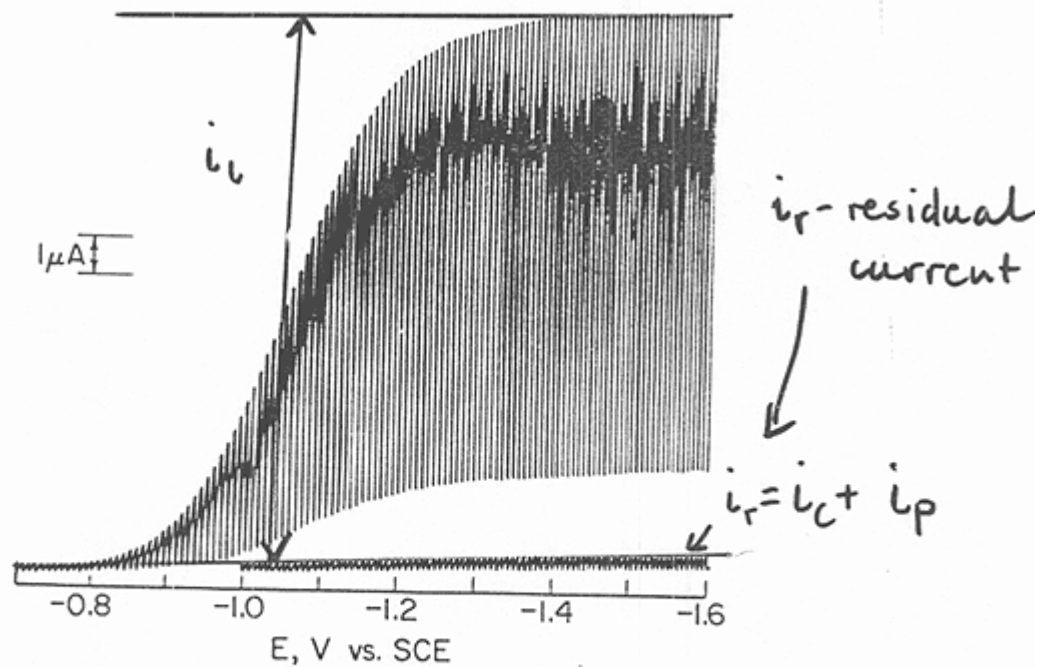


Figure 2
Polarogram for 1 mM CrO_4^{2-} in deaerated 0.1 M NaOH. The lower curve is the residual current observed in the absence of CrO_4^{2-} .

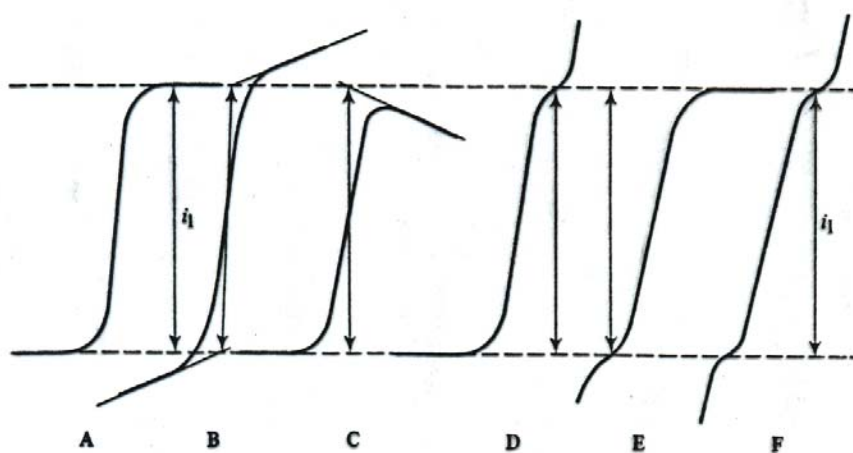


FIGURE 3.12. Illustration of several methods for measuring the wave height of variously shaped polarographic waves. Curves A-C illustrate the technique of extrapolating the linear portions of the waves before and after the current rise. Curves D-F illustrate the technique of estimating current magnitudes for ill shaped waves.

average current

$$\bar{I} = \frac{\int_0^{t_d} i dt}{t_d}$$

$$\bar{I} = 708 n D^{1/2} C^b m^{2/3} \frac{\int_0^{t_d} t^{1/6} dt}{t_d}$$

$$\bar{I} = \left(\frac{6}{7}\right) 708 n D^{1/2} C^b m^{2/3} t^{1/6}$$

$$\bar{I} = 607 n D^{1/2} m^{2/3} t_d^{1/6} C^b$$

charging current

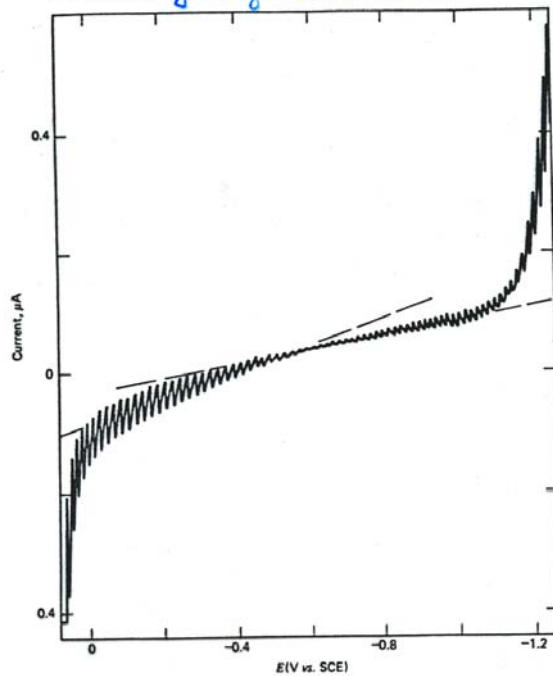


Figure 5.3.5

Residual current curve for 0.1 M HCl. (From L. Meites, "Polarographic Techniques," 2nd ed., Wiley-Interscience, New York, 1965, p. 101, with permission of John Wiley and Sons, Inc.)

instantaneous charging current

$$q = C_i A (E - E_2)$$

$$i_c = \frac{dq}{dt} = C_i (E - E_2) \frac{dA}{dt}$$

$$A = 4\pi \left(\frac{3mt}{4\pi d_{Hg}} \right)^{2/3}$$

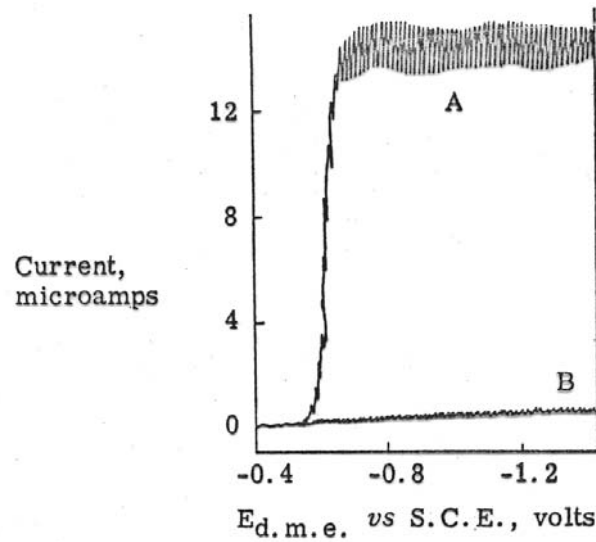
$$i_c = 0.00567 C_i (E - E_2) m^{2/3} t^{-1/3}$$

average charging current

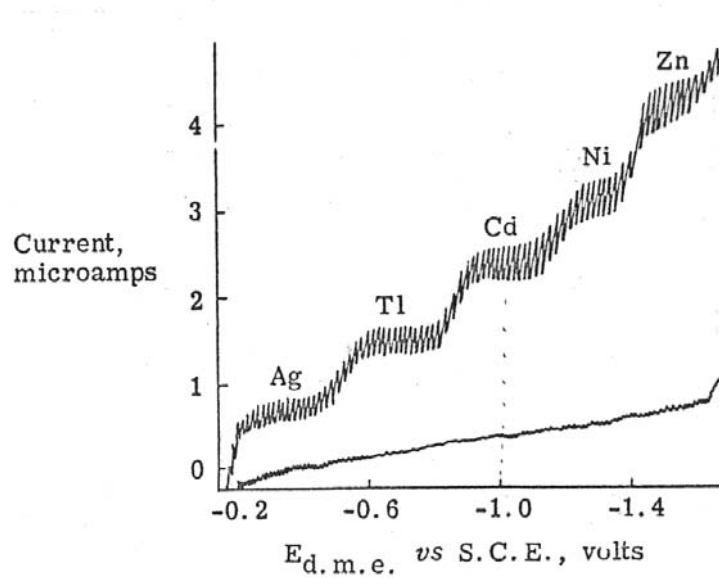
$$\bar{i}_c = \frac{\int_0^{t_d} i_c dt}{t_d}$$

$$\bar{i}_c = 0.0085 C_i (E - E_2) m^{2/3} t_d^{-1/3}$$

Typical Polarogram



Polarogram of a Mixture of Ions



[Adapted from L. Meites, "Polarographic Techniques," Interscience Publishers, New York, 1965]

polarography - detection limit

$$\bar{I}_d = 607 n D^{1/2} C^b m^{2/3} t_d^{1/6}$$

$$\bar{I}_c = 0.0085 C_1 (E - E_2) m^{2/3} t_d^{-1/3}$$

detection limit $\bar{I}_d = 2\bar{I}_c$

$$607 n D^{1/2} C^b m^{2/3} t_d^{1/6} = 2 \cdot 0.0085 C_1 (E - E_2) m^{2/3} t_d^{-1/3}$$

suppose

$$E - E_2 = 0.1 \text{ V}$$

$$C_1 = 20 \mu\text{F}/\text{cm}^2$$

$$n = 2$$

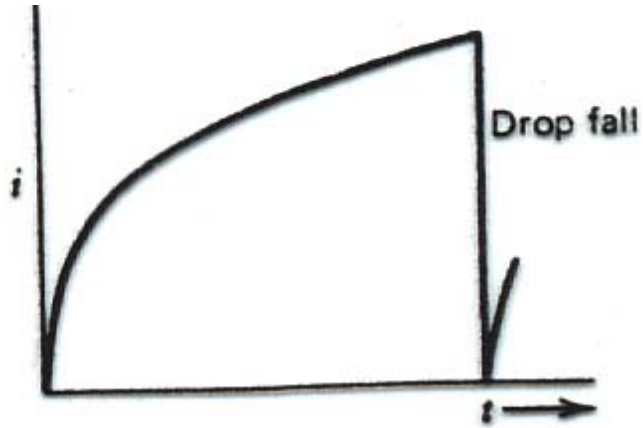
$$t_d = 4 \text{ s}$$

$$D = 10^{-6} \text{ cm}^2 \text{ s}^{-1}$$

$$C^b = \frac{2 \cdot 0.0085 C_1 (E - E_2) t_d^{-1/2}}{607 n D^{1/2}}$$

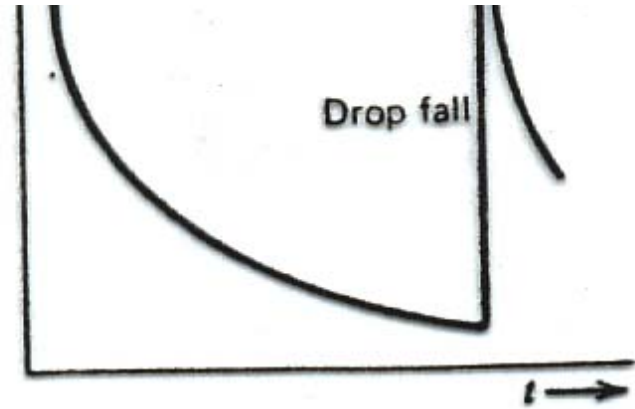
$$\underline{C^b \approx 10^{-5} \text{ M}}$$

7.2 Tast Polarography



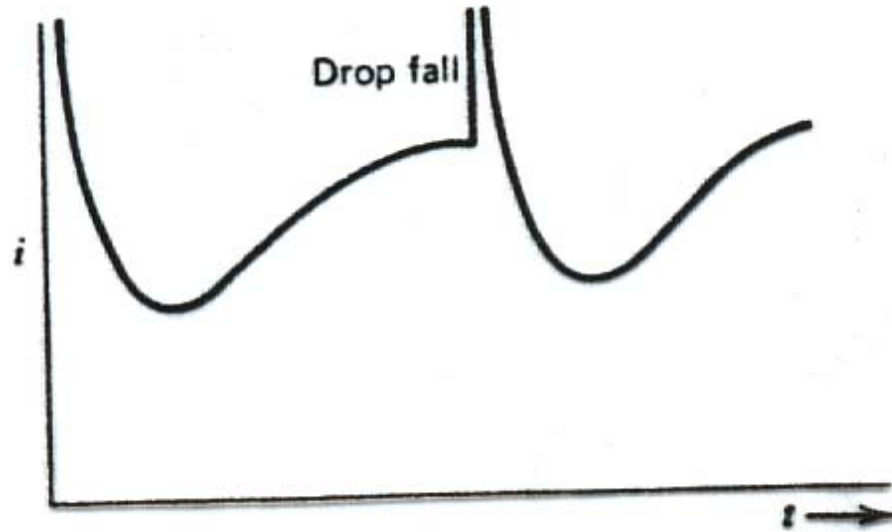
Faradaic current

$$i_d \propto t^{\frac{1}{6}}$$

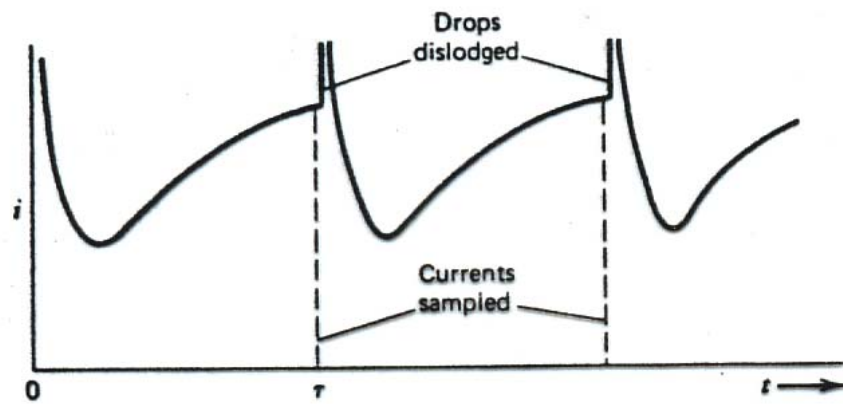


Charging current

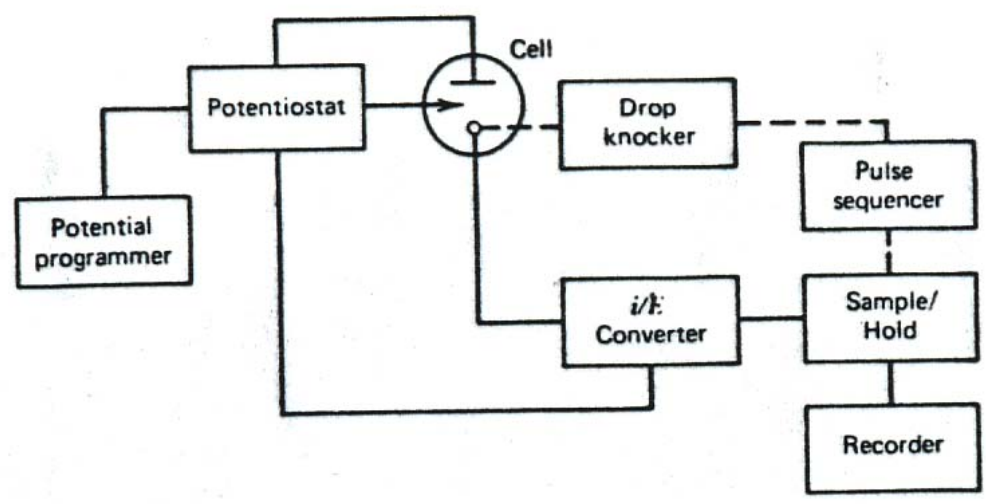
$$i_c \propto t^{-\frac{1}{3}}$$



Total current



Sampling scheme for fast polarography.



Schematic experimental arrangement for fast polarography.

Tast polarography

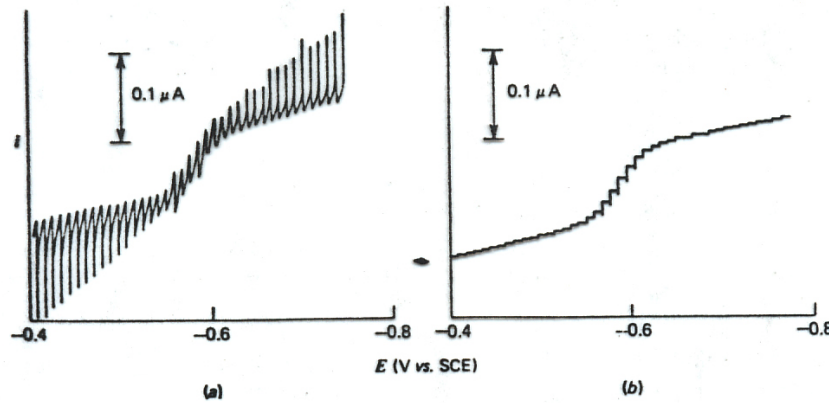


Figure 5.8.3

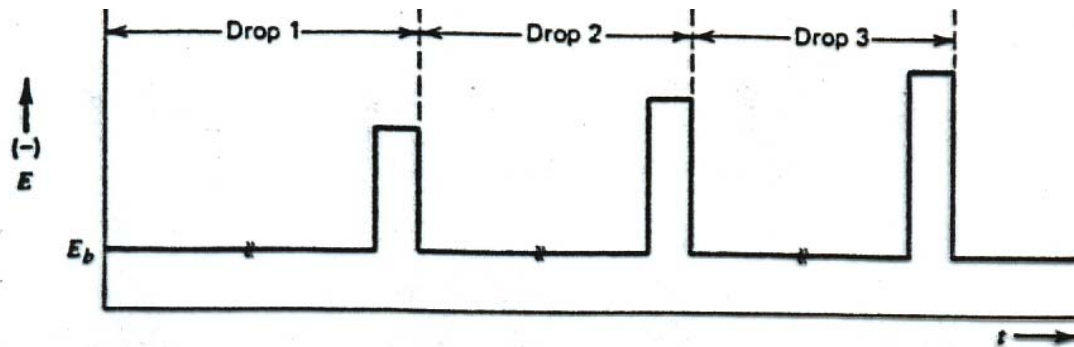
Polarograms for $10^{-5} M \text{Cd}^{2+}$ in $0.01 M \text{HCl}$. (a) Conventional dc mode. (b) Tast mode.

$$\frac{i_d}{i_c} = \text{const}'' \tau^{1/2}$$

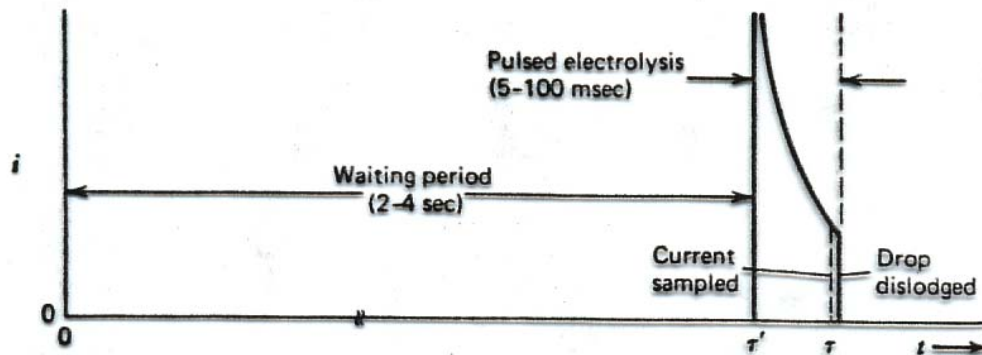
τ - sampling time

Detection limit $10^{-6} M$

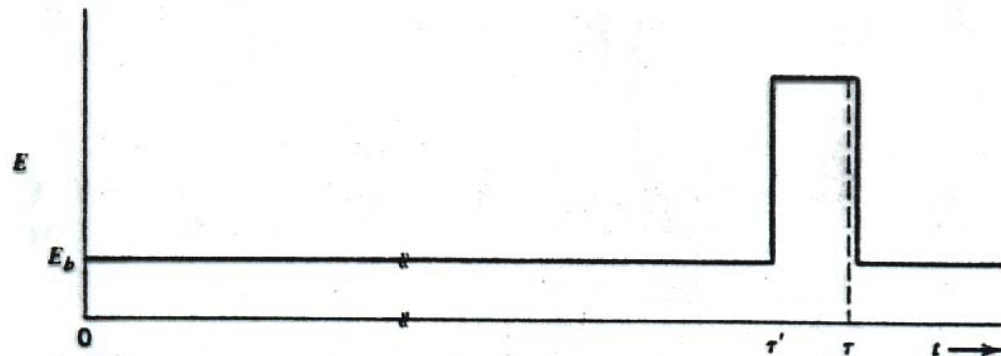
7.3 Pulse Polarography



(a)



(b)



(c)

$$i = \left(\frac{7}{3}\right)^{\frac{1}{2}} nFD^{\frac{1}{2}}C^* A / \sqrt{\pi t}$$

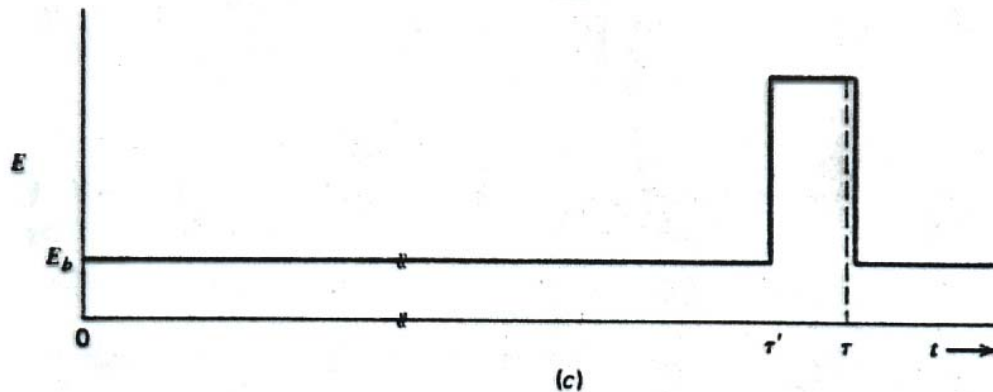
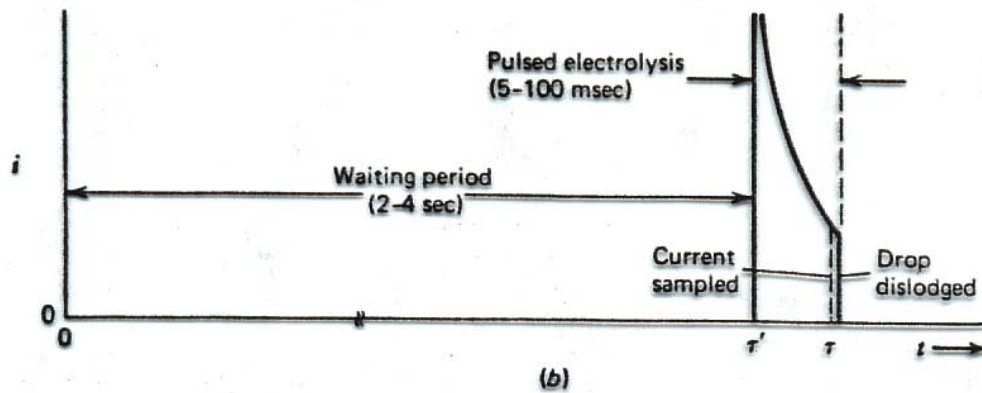
$$A = 0.85m^{\frac{2}{3}}t^{\frac{2}{3}}$$

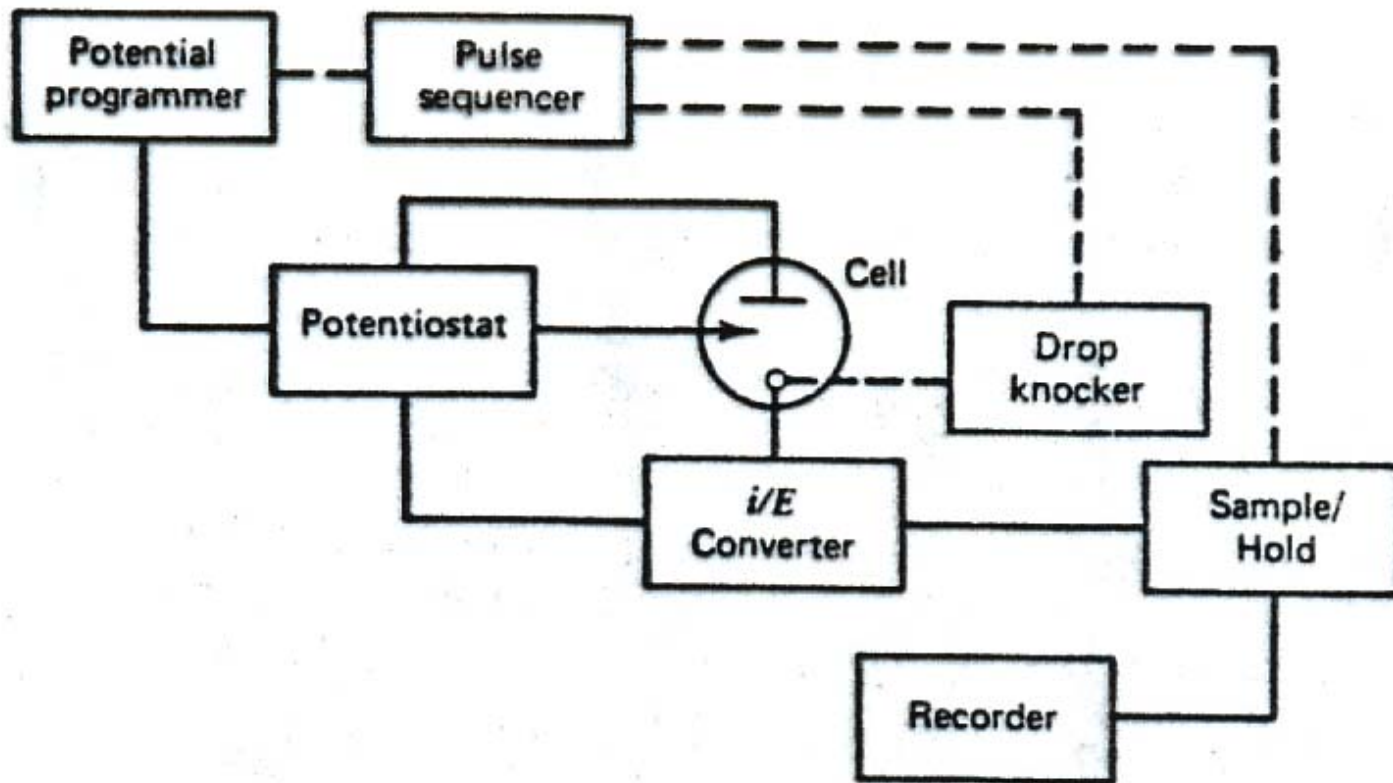
Polarography

$$i = \left(\frac{7}{3}\right)^{\frac{1}{2}} nFD^{\frac{1}{2}}C^* 0.85m^{\frac{2}{3}}t^{\frac{2}{3}} / \sqrt{\pi t}$$

Pulse Polarography

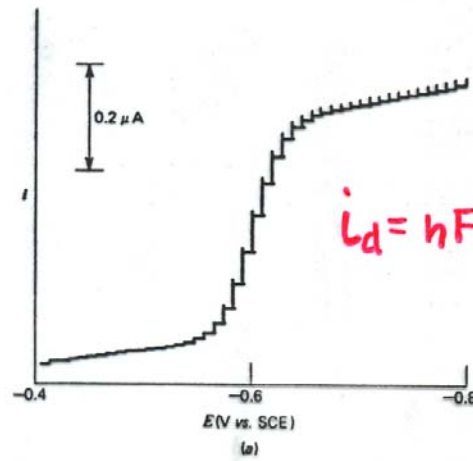
$$i = \left(\frac{7}{3}\right)^{\frac{1}{2}} nFD^{\frac{1}{2}}C^* 0.85m^{\frac{2}{3}}t^{\frac{2}{3}} / \sqrt{\pi(t-t')}$$



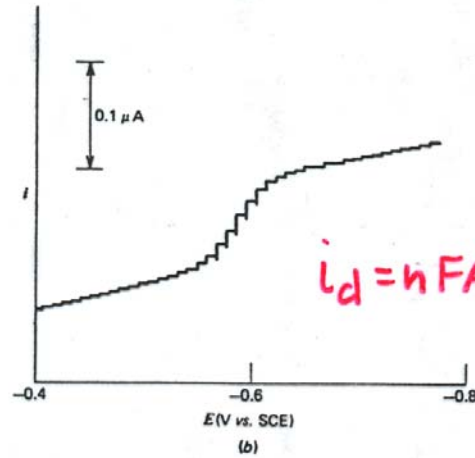


Schematics of a set up for pulse polarography

Detection limit $10^{-7}M$



$$i_d = nFAD^{1/2} \frac{-1/2}{\pi} C^b / (\tau - \tau')^{1/2}$$



$$i_d = nFAD^{1/2} \frac{-1/2}{\pi} C^b / (\tau')^{1/2}$$

Figure 5.8.6

Polarograms for $10^{-8} M Cd^{2+}$ in $0.01 M HCl$. (a) Normal pulse mode. (b) Tast mode.

$$(i_d)_p / (i_d)_t = (\tau' / \tau - \tau')^{1/2} = 10$$

suppose $\tau' = 4s$
 $\tau - \tau' = 40ms$

$$(i_c)_p \approx (i_c)_t = 0.00567 C_i (E - E_2) m^{2/3} t^{-1/3}$$

7.4 Differential pulse polarography

Current is sampled twice a time t and t' . Quantity measured is a difference δi :

$$\delta i = i(t) - i(t')$$

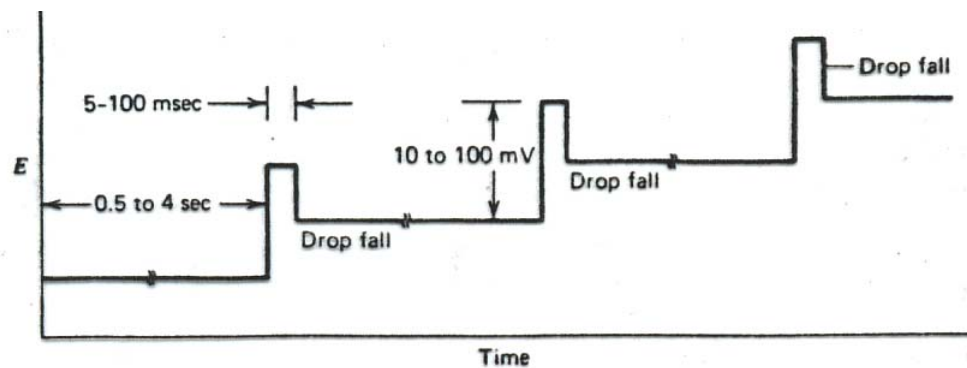
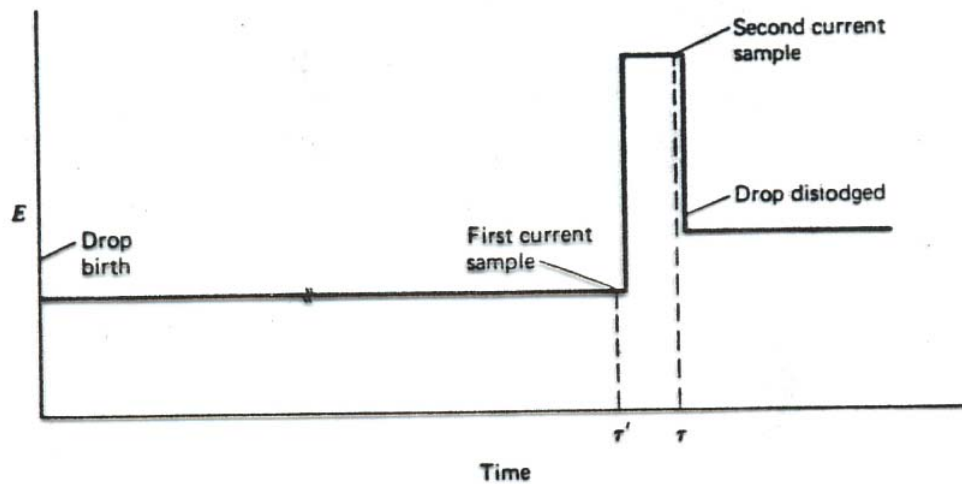


Figure 5.8.8

Potential program for several drops in a differential pulse polarographic experiment.



Differential pulse

$$\delta i = \delta i_d + \delta i_c$$

$$\delta i_c = i_c(t) - i_c(t')$$

Normal pulse

$$i = i_d(t - t') + i_c(t)$$

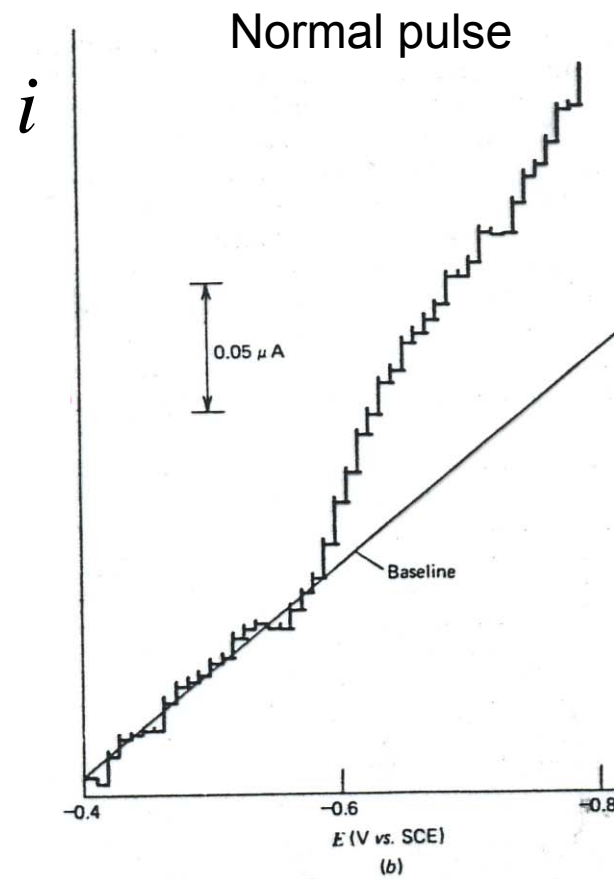
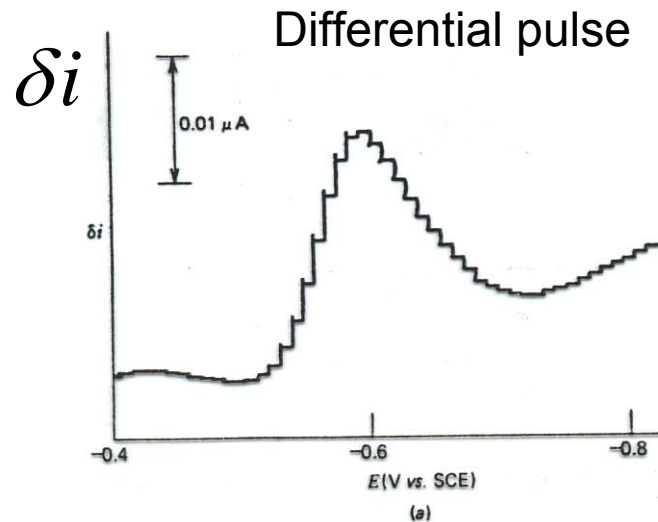
at peak potential

$$\delta i_d \propto i_d(t - t')$$

but

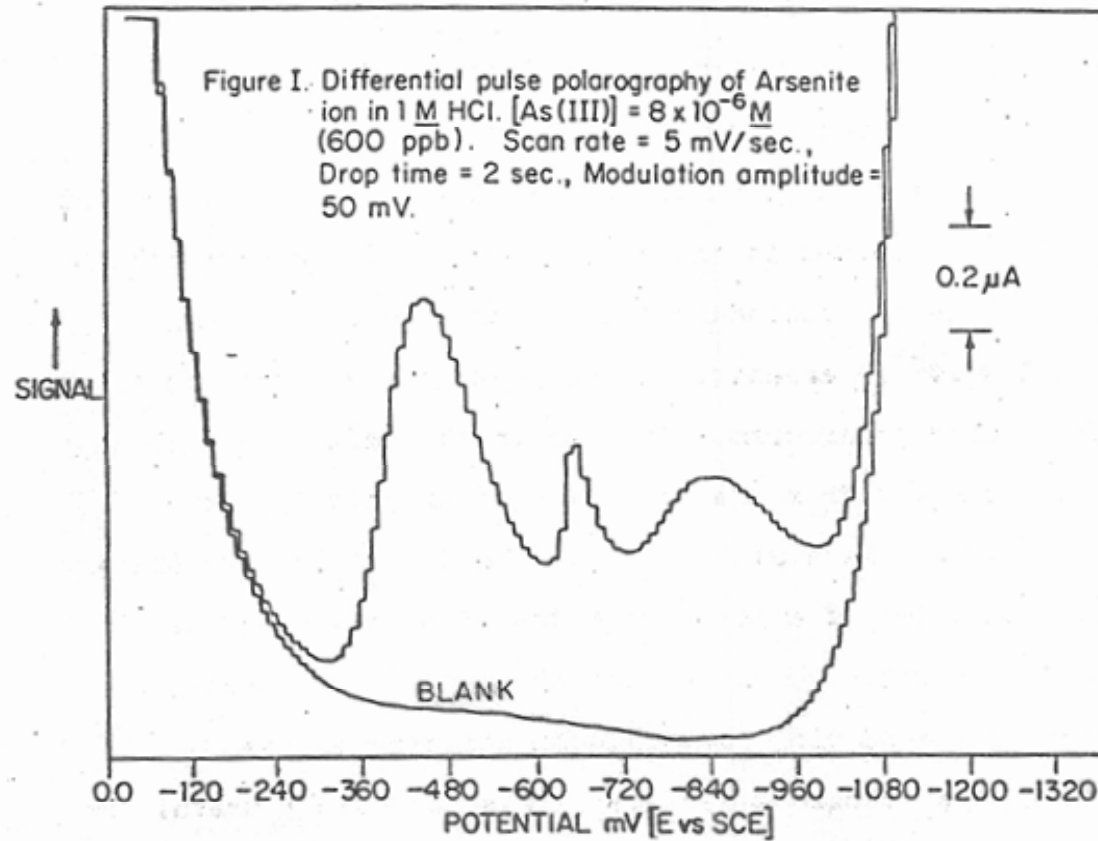
$$\delta i_c \ll i_c(t)$$

Detection limit of differential pulse polarography
 $\sim 10^{-8} \text{M}$

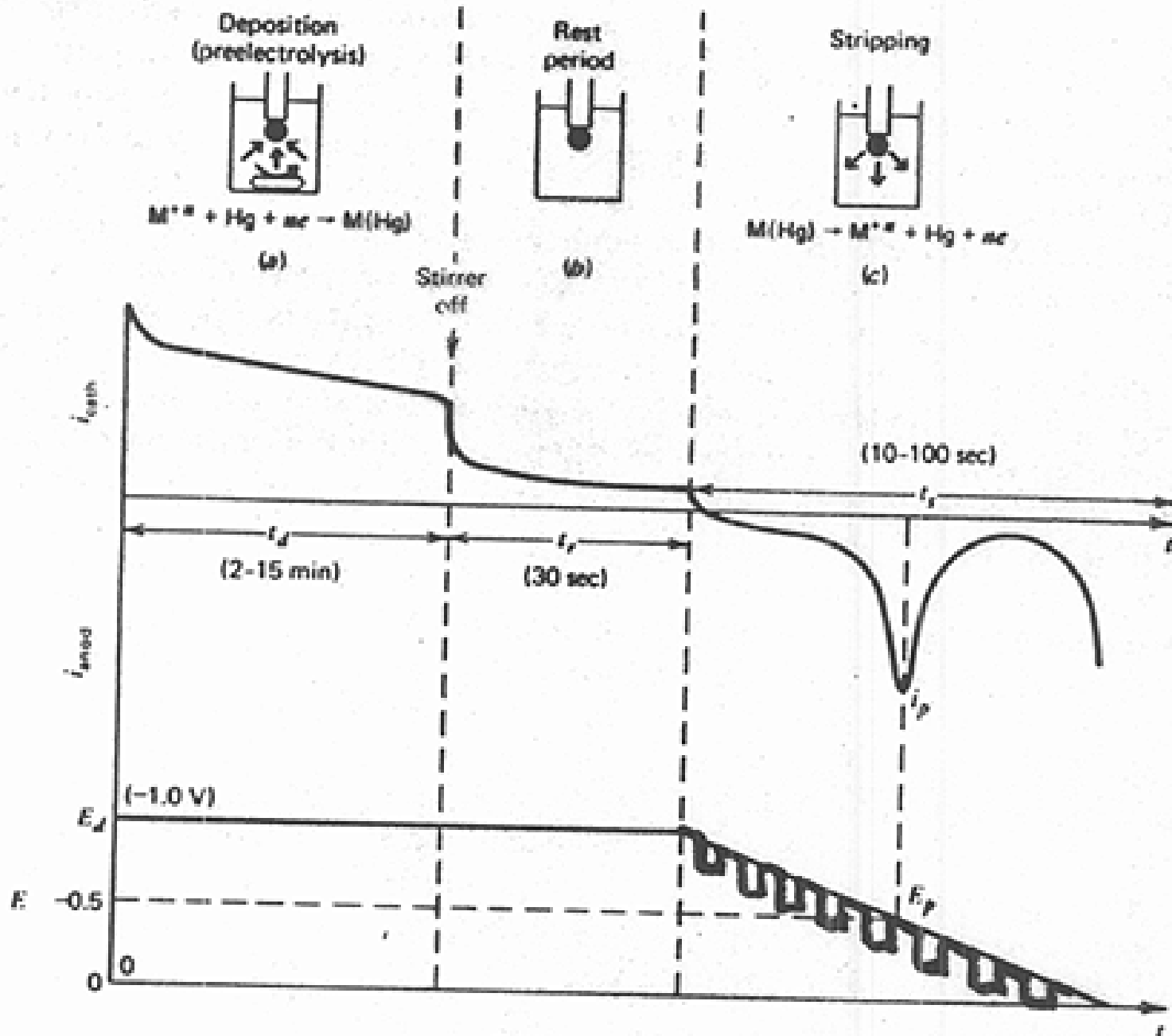


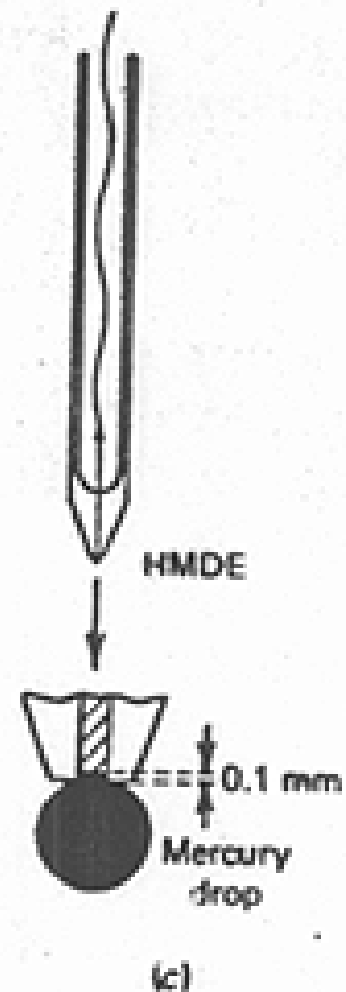
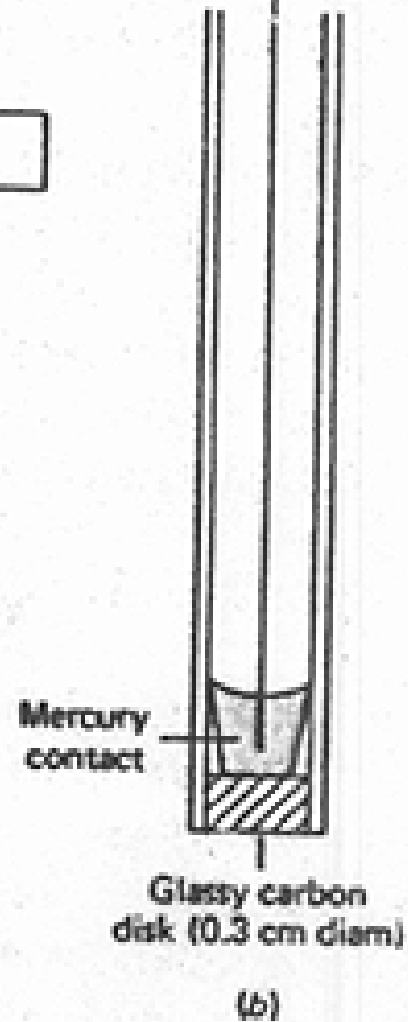
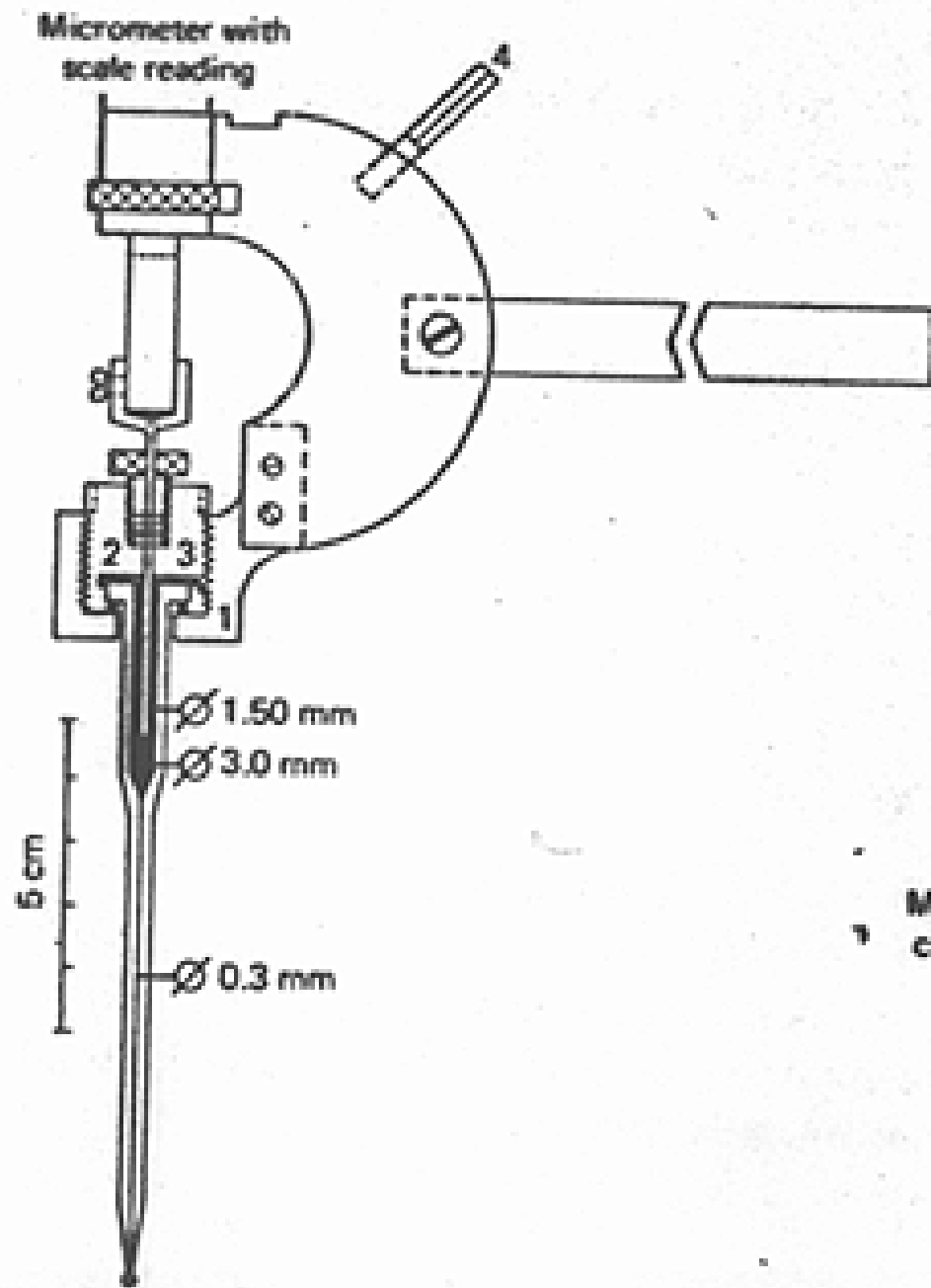
Examples of Pulse Polarographic Analysis:

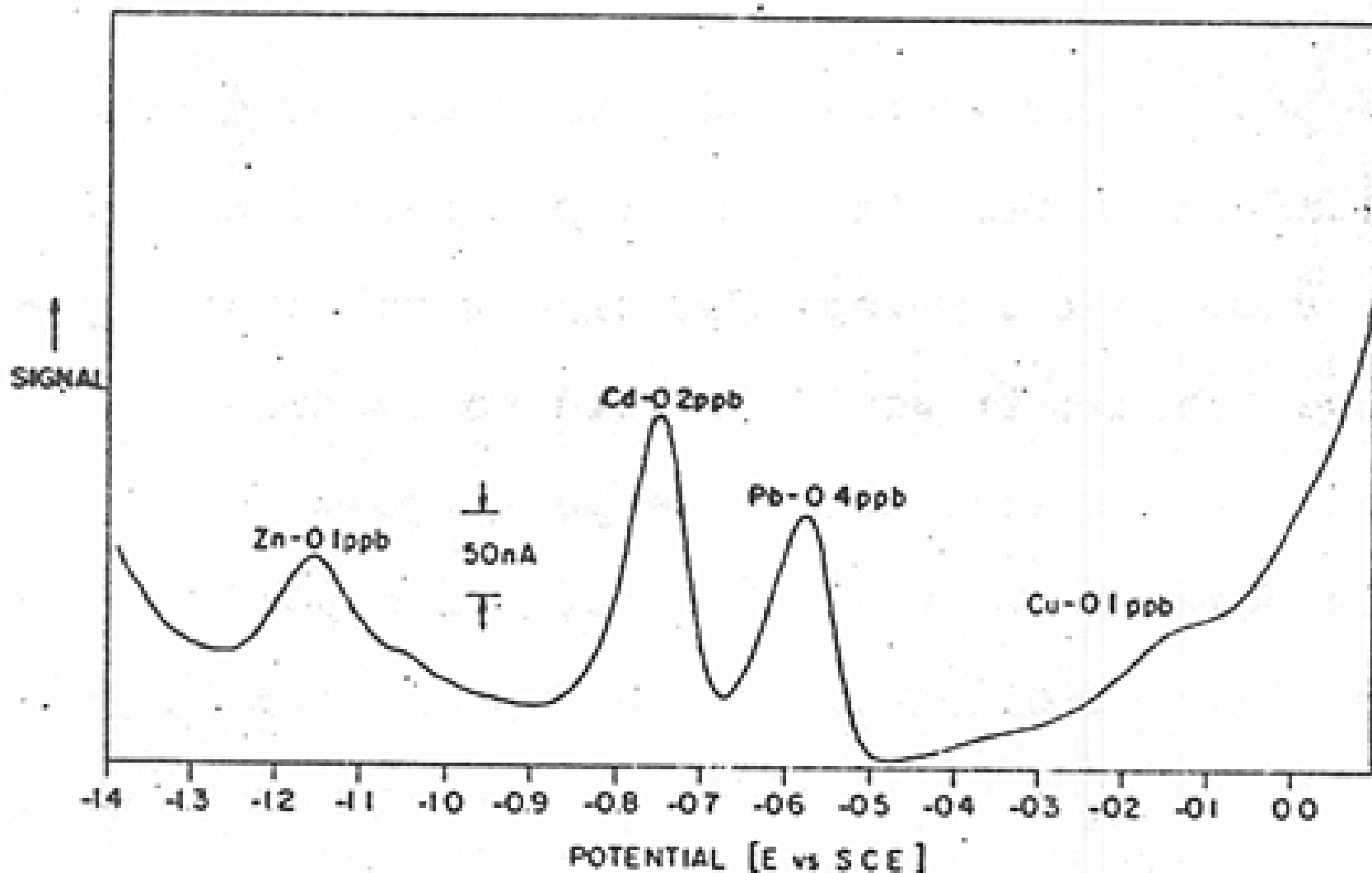
Arsenic:



7.5 Striping voltammetry

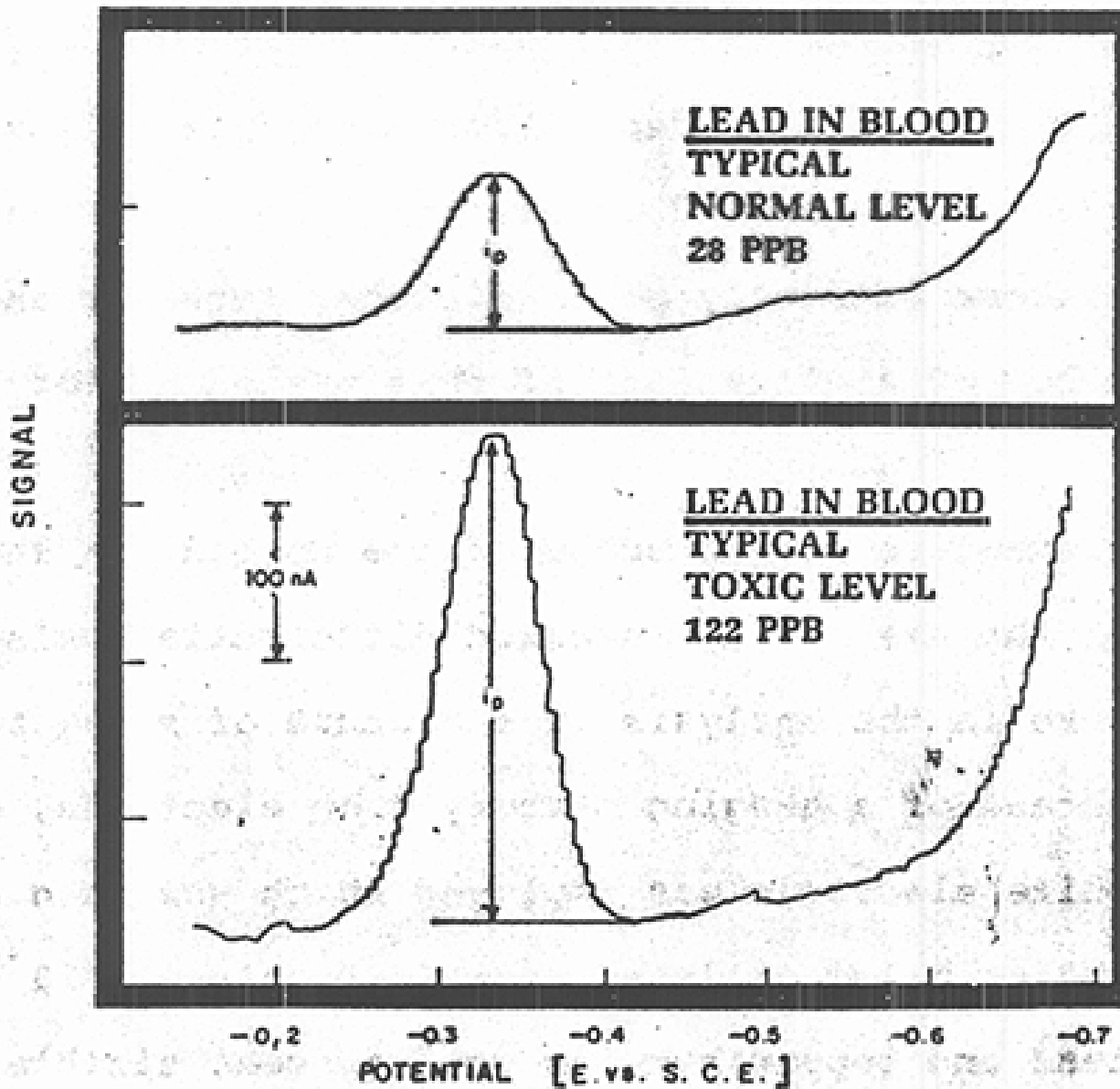






Differential pulse anodic stripping voltammetry. PAR Model 174 polarographic analyzer, Model 9319 wax-impregnated graphite electrode (mercury-plated). $2 \times 10^{-1} M$ Zn, Cd, Pb, and Cu

Determination of lead in blood in the 10-100 parts per billion range:



Electroanalytical techniques – Figures of merits

	Accuracy %	Sensitivity mol dm^{-3}	Range mol dm^{-3}	Selectivity $\Delta E_{1/2} / \text{mV}$
DC Polarography	$\pm 1-3\%$	10^{-5}	$10^{-2} - 10^{-5}$	100
Tast Polarography	$\pm 1-3\%$	10^{-6}	$10^{-2} - 10^{-6}$	100
Normal Pulse Polarography	$\pm 1-3\%$	10^{-7}	$10^{-2} - 10^{-7}$	100
Differential Pulse Polarography	$\pm 1-3\%$	10^{-8}	$10^{-2} - 10^{-8}$	50
stripping Voltammetry	$\pm 2-20\%$	10^{-10}	$10^{-2} - 10^{-10}$	50
L.S.V	$\pm 1-3\%$	10^{-5}	$10^{-2} - 10^{-5}$	100

1. Analyses of metals

about 30 metals at levels ≥ 10 ppb

about 12 metals at levels less
than 1 ppb

2. Analyses of non-metallic ions

at ultra-trace quantities by stripping
techniques

(Cl^- , Br^- , I^- , CN^- , N_3^- , S^{2-} , $\text{S}_2\text{O}_3^{2-}$ etc)

or

(CO_2^- , NO_3^- , IO_3^- , IO_4^-)

3. Analysis of organics

reducible functional groups

Imines, Oximes, Nitro, Nitroso, Aldehydes

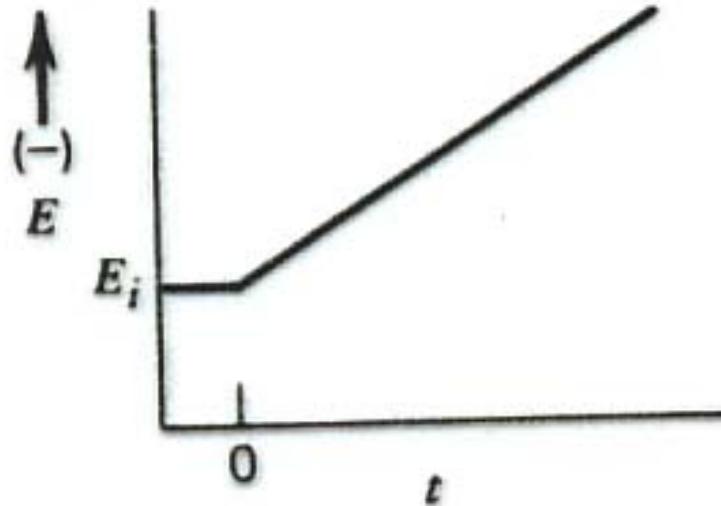
Halides, Organo-metallics etc.

8. Linear sweep voltammetry

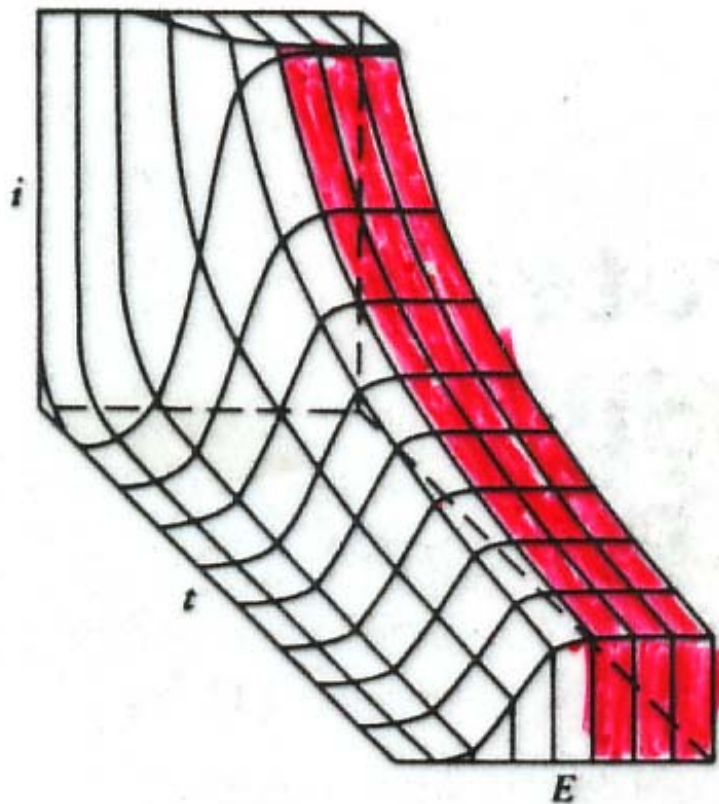
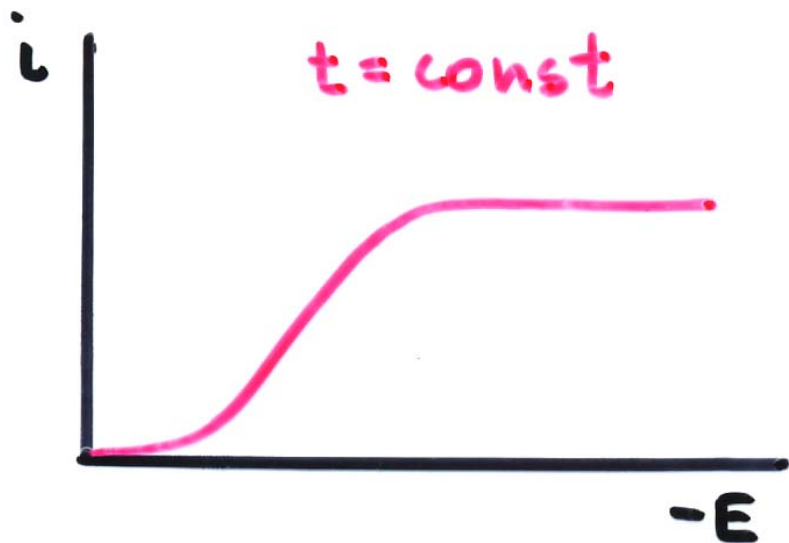
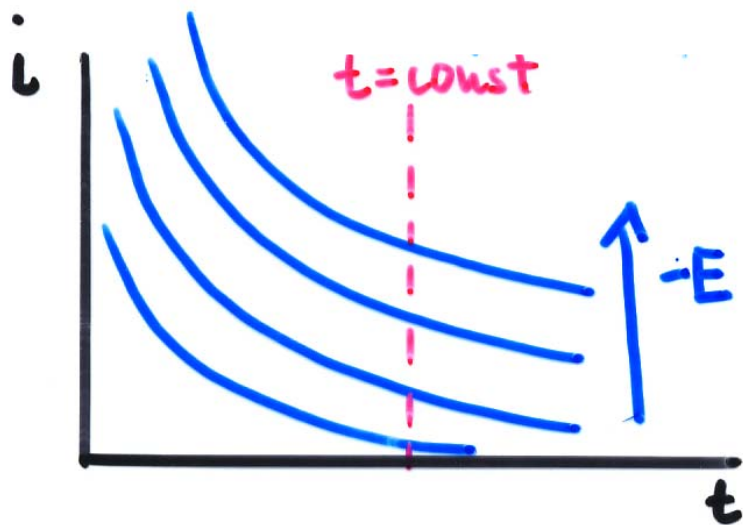
Perturbation – linear voltage sweep (voltage ramp)

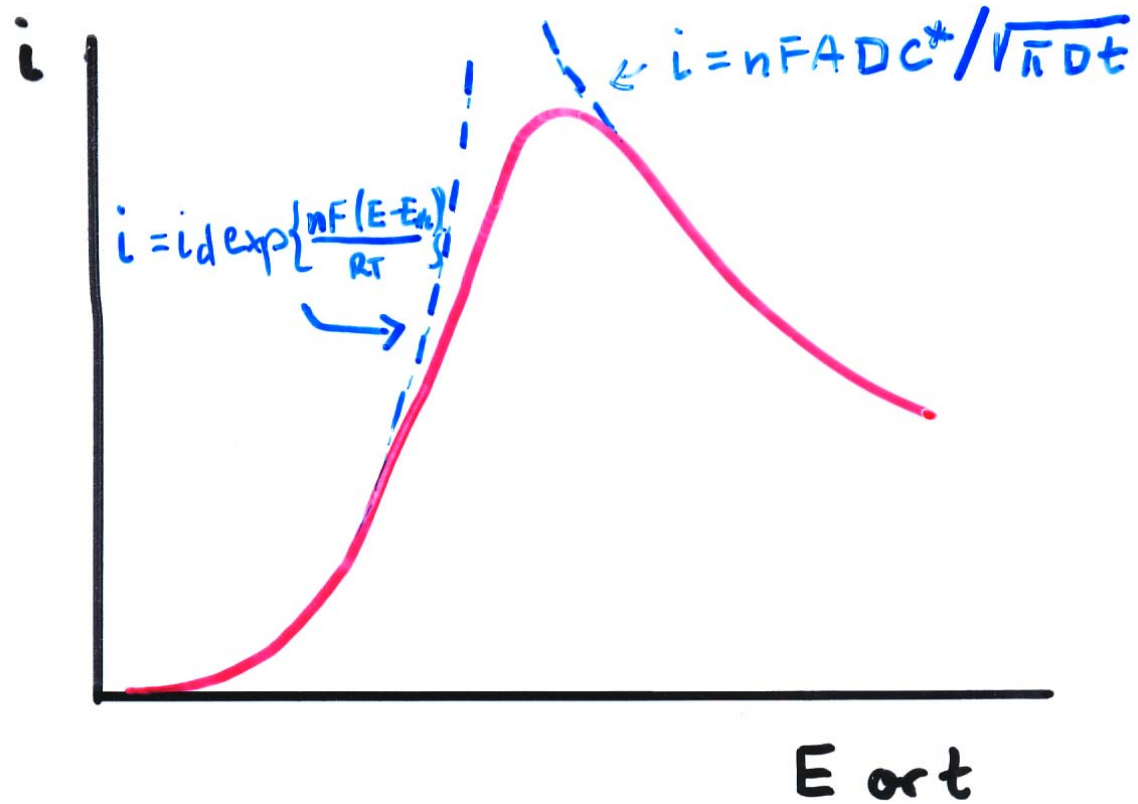
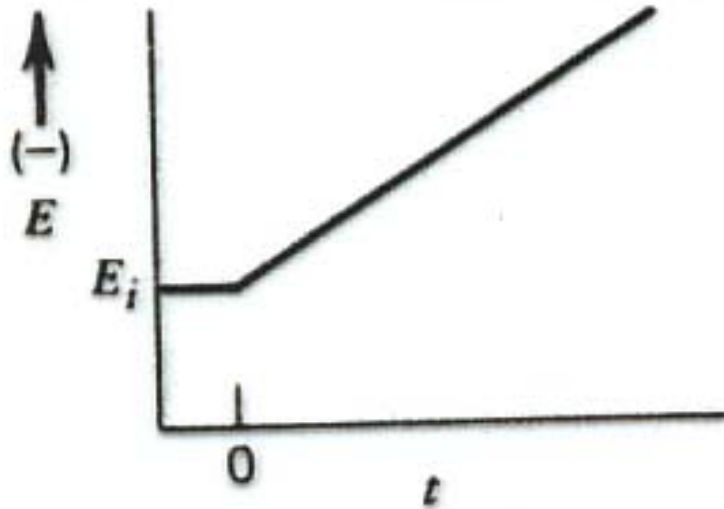
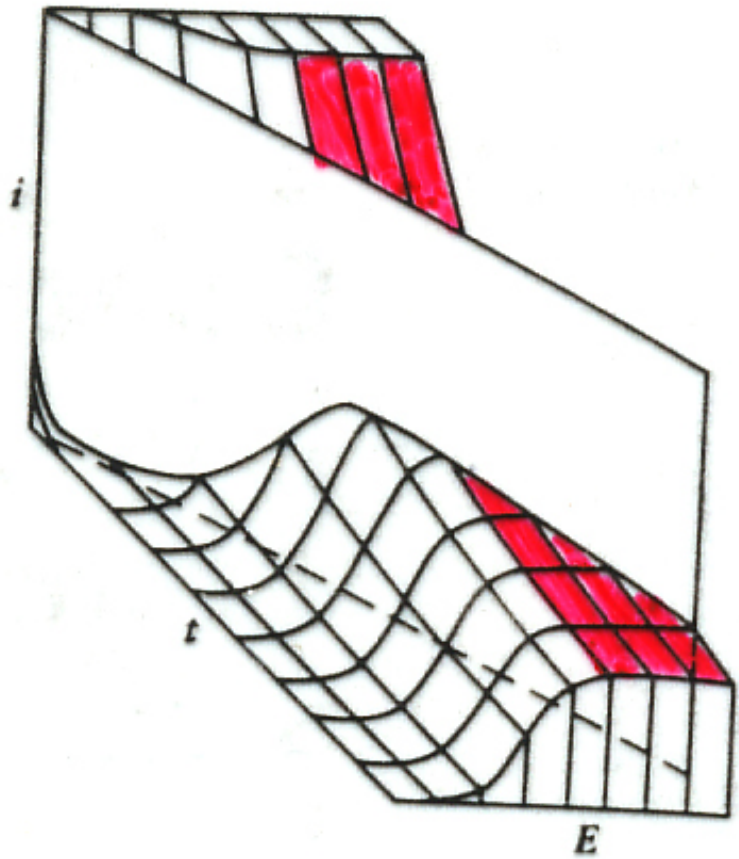
$$E = E_i - vt$$

v sweep rate in V/s



Qualitative prediction of the shape of a CV curve –
chronoamperometric experiments





There is no analytical solution to this problem – the equation has been solved numerically

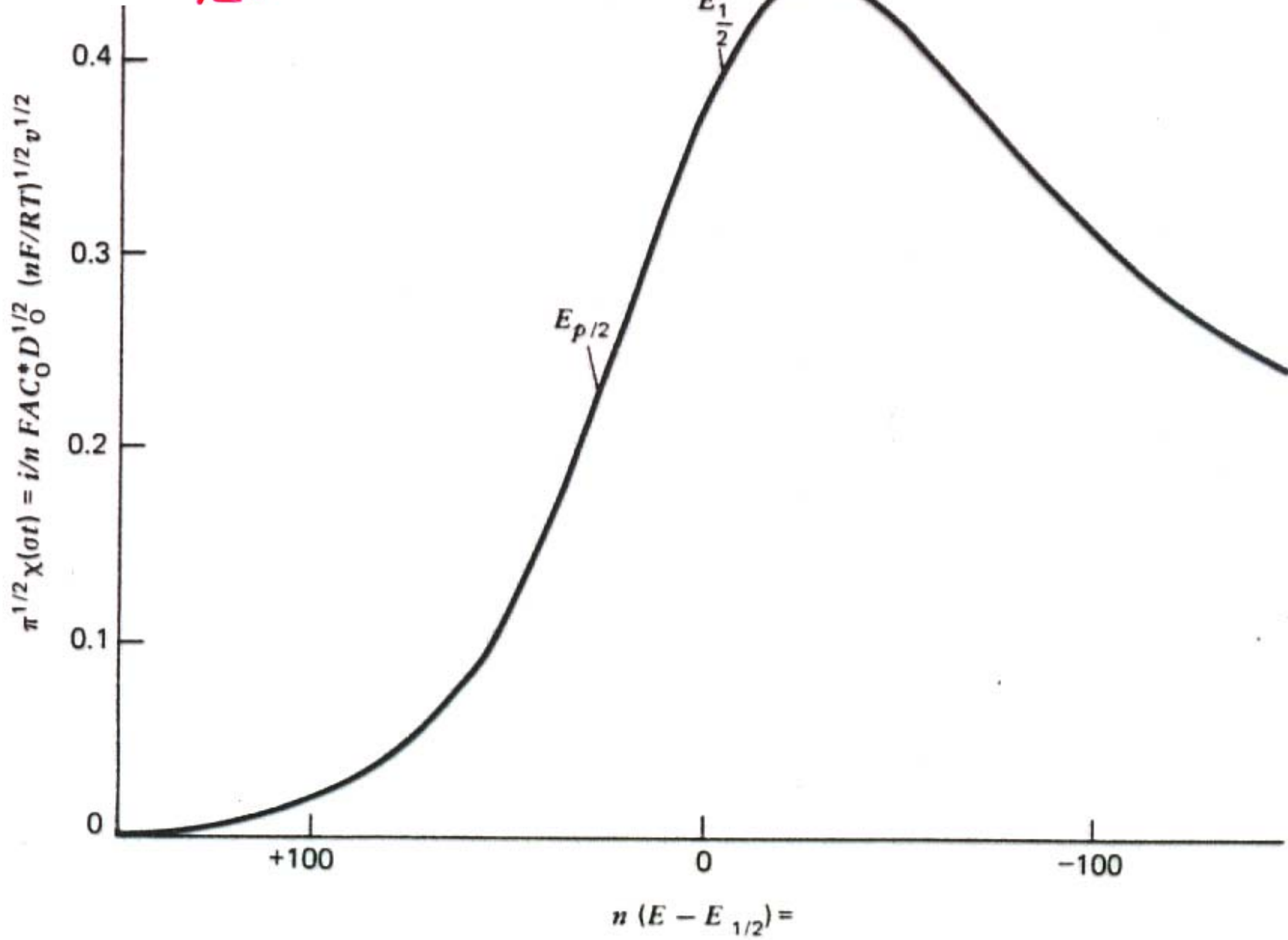
$$i = nFA C_o^* \left(\pi D_o \frac{nFv}{RT} \right)^{1/2} \chi(E - E_{1/2})$$

where $\chi(E - E_{1/2})$ at any given point is a pure number

The shape of the CV curve is determined by the shape of numerical function:

$$\chi(E - E_{1/2})$$

$\chi(E - E_{1/2})$



$$i_p = 0.4463 nFA C_o^* \left(\frac{nF}{RT} \right)^{1/2} v^{1/2} D_o^{1/2}$$

$$E_p - E_{1/2} = -28.5 \text{ mV}/n \quad \text{at } 25^\circ\text{C}$$

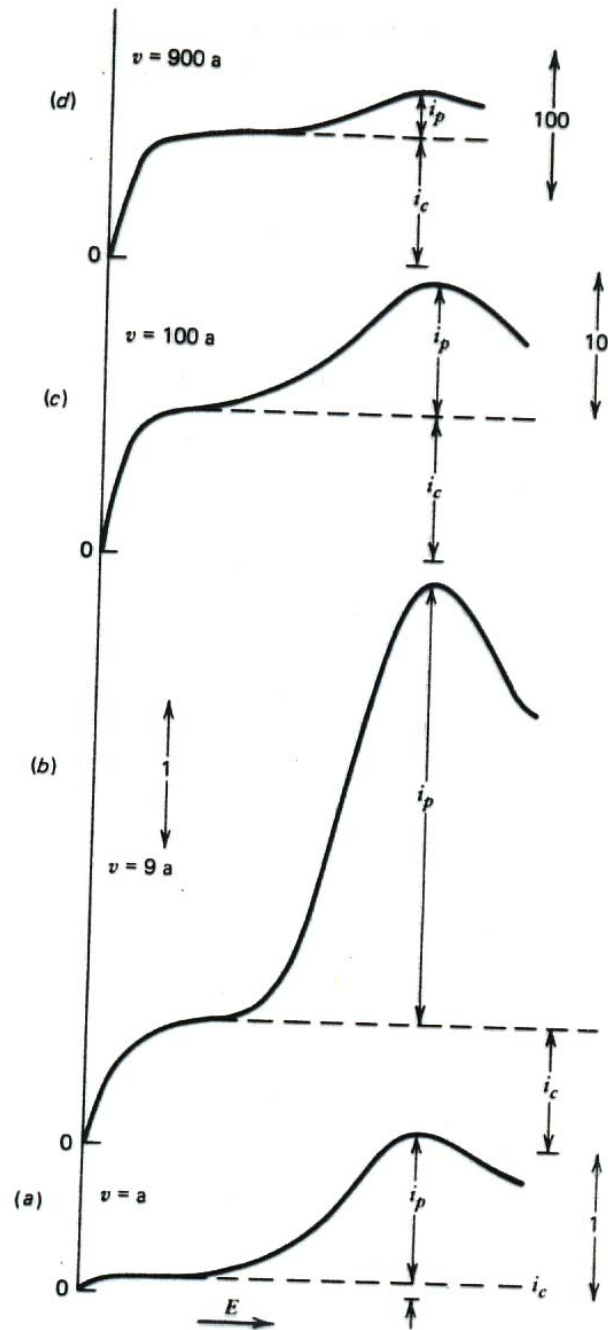
$$E_{p/2} = E_{1/2} + 28.0/n \text{ mV}$$

$$|E_p - E_{p/2}| = 56.5/n \text{ mV}$$

$$i = i_c + i_F$$

$$i_c = A \frac{dq}{dt} = A \frac{dq}{dE} \cdot \frac{dE}{dt} = ACd \cdot v$$

$$i = k_c v + k'_F v^{1/2}$$



LSV - detection limit

$$i_p \geq 2i_c$$

$$0.446 nFA \left(\frac{nFv}{RT} \right)^{1/2} D^{1/2} C^* = 2AC_d v$$

$$C^* \geq \frac{2C_d \left(\frac{nFv}{RT} \right)^{1/2}}{D^{1/2} 0.45 nF}$$

for

$$D = 4 \times 10^{-6} \text{ cm}^2 \text{ s}^{-1}$$

$$C_d = 20 \mu\text{F cm}^{-2}$$

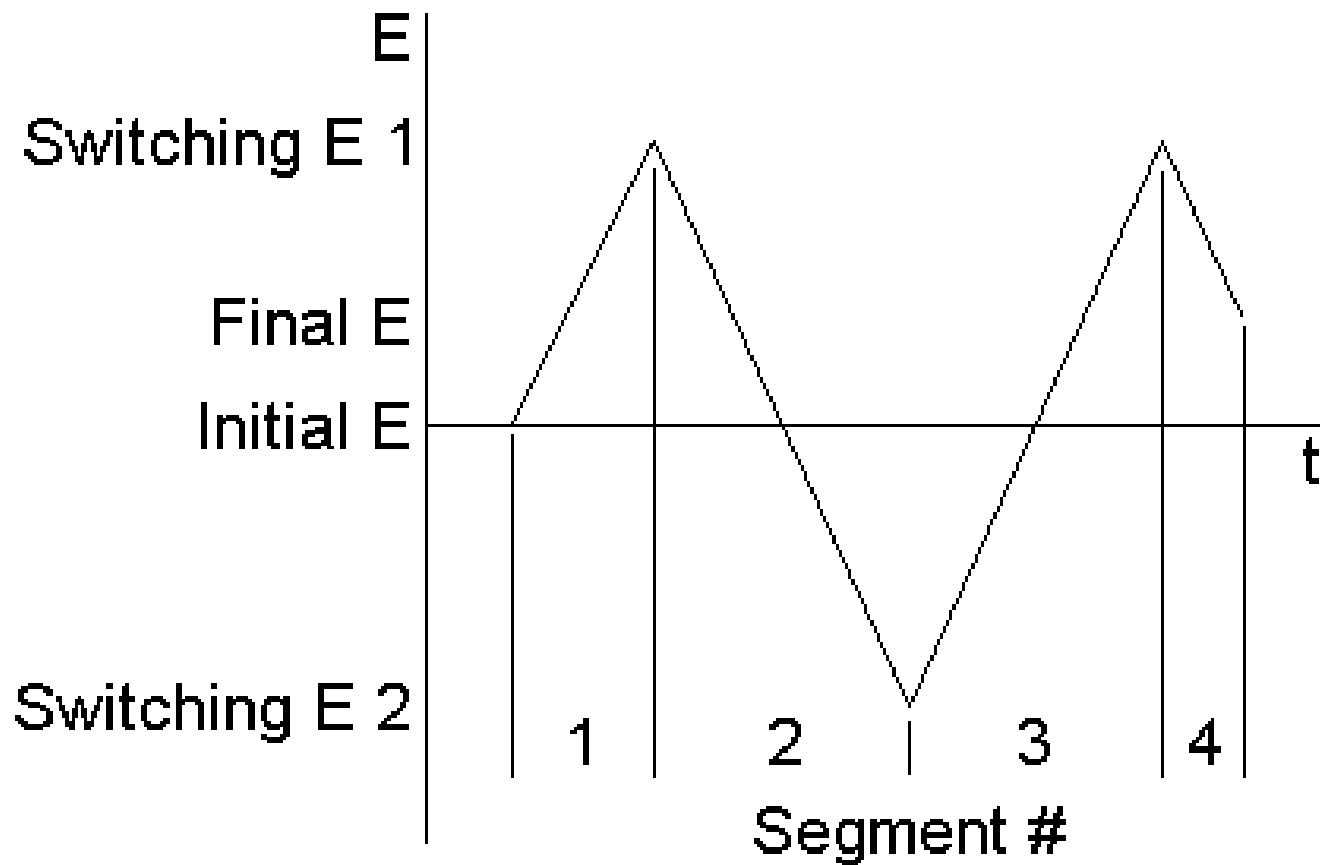
$$n = 2$$

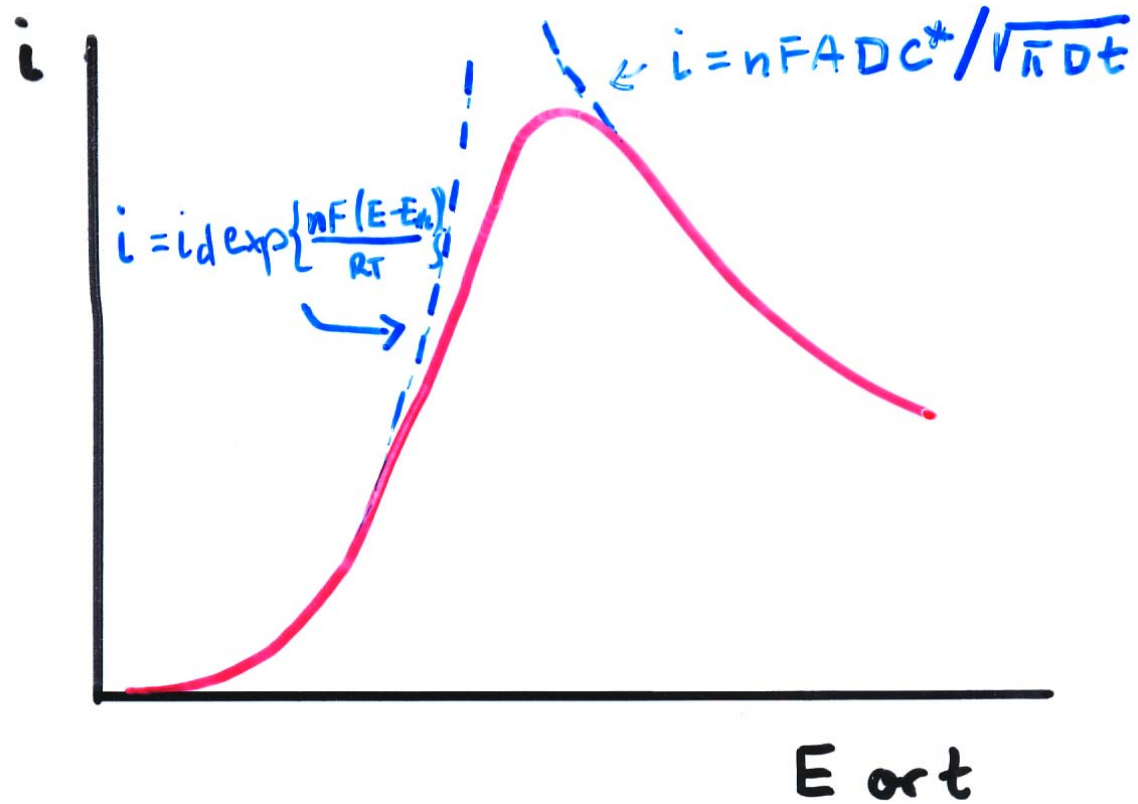
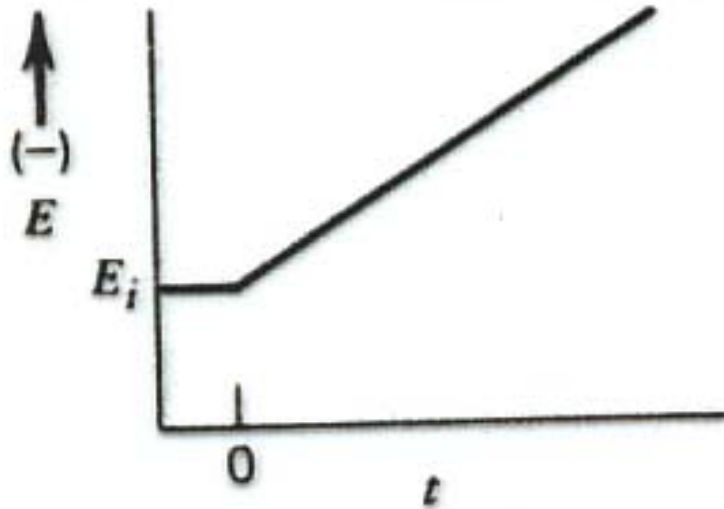
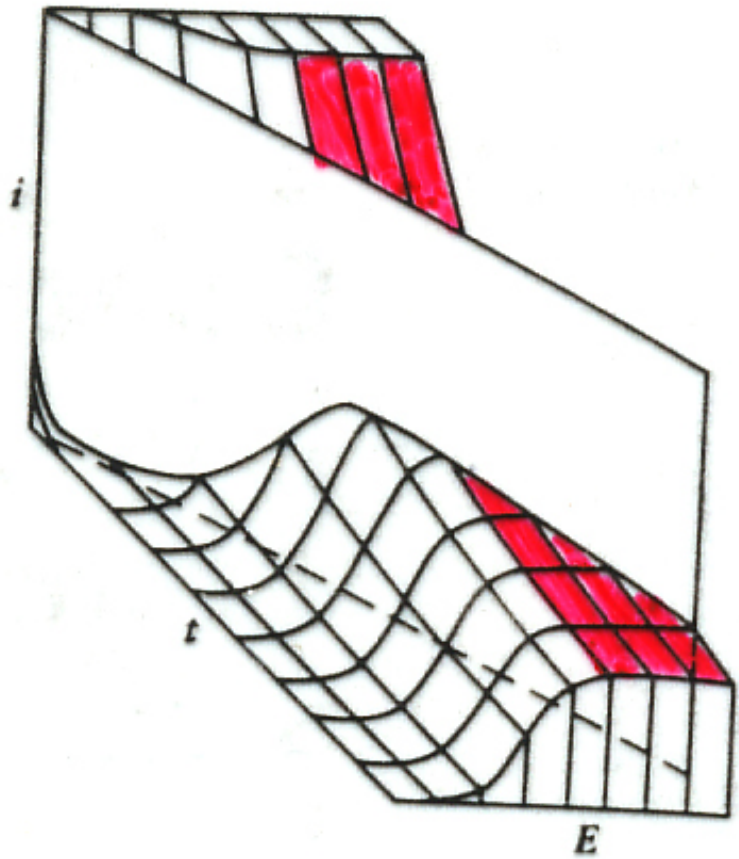
$$\left(\frac{nFv}{RT} \right)^{1/2} = 1 \text{ s}^{1/2} \quad v \approx 25 \text{ mVs}^{-1}$$

$$C^* \geq 10^{-5} \text{ mol dm}^{-3}$$

	time parameter	time window/s	reversibility lower limit of $k_0/\text{cm s}^{-1}$
DC Polarography	t_d	1 - 10	$10^{-3} - 3 \cdot 10^{-4}$
Fast Polarography	τ'	1 - 10	$10^{-3} - 3 \cdot 10^{-4}$
Normal Pulse polarography	$\tau - \tau'$	$10^{-2} - 10^{-1}$	$10^{-2} - 3 \cdot 10^{-3}$
Differential Pulse Polarography	$\tau - \tau'$	$10^{-2} - 10^{-1}$	$10^{-2} - 3 \cdot 10^{-3}$
LSV	$\frac{RT}{Fv}$	$1\text{Vs}^{-1} - 1\text{mVs}^{-1}$	$10^{-2} - 10^{-3}$

Cyclic voltammetry





CV Run for BAS5-Epsilon

